

LAT.	5°		6°		7°		8°		9°		LAT.
H.A.	Alt.	Az.	Alt.	Az.	Alt.	Az.	Alt.	Az.	Alt.	Az.	H.A.
45	42 11-19	59	42 42-18	60	43 11-16	61	43 40-15	61	44 09-15	62	315
46	41 20 19	59	41 50 17	60	42 19 16	61	42 48 15	62	43 16 13	63	314
47	40 28 17	60	40 58 16	60	41 27 15	61	41 56 14	62	42 24 14	63	313
48	39 37 17	60	40 06 16	61	40 35 15	62	41 03 13	62	41 31 13	63	312
49	38 45 17	60	39 14 15	61	39 43 14	62	40 11 13	63	40 38 12	63	311
50	37 53-16	61	38 22-15	61	38 50-13	62	39 18-12	63	39 45-11	64	310
51	37 01 16	61	37 29 14	62	37 57 12	62	38 25 12	63	38 52 11	64	309
52	36 08 14	61	36 37 14	62	37 05 13	63	37 32 11	63	37 59 10	64	308
53	35 16 14	62	35 44 13	62	36 12 12	63	36 39 11	63	37 05 9	64	307
54	34 23 13	62	34 51 12	62	35 19 11	63	35 46 10	64	36 12 9	64	306
55	33 31-13	62	33 58-11	63	34 26-11	63	34 53-10	64	35 19 -9	64	305
56	32 38 12	62	33 05 11	63	33 33 10	63	33 59 9	64	34 25 7	65	304
57	31 45 12	62	32 12 10	63	32 39 9	64	33 06 8	64	33 32 7	65	303
58	30 52 11	63	31 19 10	63	31 46 9	64	32 12 7	64	32 38 6	65	302
59	29 59 11	63	30 26 9	63	30 53 9	64	31 19 7	64	31 45 7	65	301
60	29 06-10	63	29 33 -9	63	29 59 -7	64	30 25 -6	64	30 51 -6	65	300
61	28 13 10	63	28 39 8	64	29 06 7	64	29 32 6	65	29 57 5	65	299
62	27 19 9	63	27 46 8	64	28 12 6	64	28 38 6	65	29 04 5	65	298
63	26 26 8	63	26 53 8	64	27 19 6	64	27 44 5	65	28 10 4	65	297
64	25 32 7	64	25 59 7	64	26 25 6	64	26 51 5	65	27 16 4	65	296
65	24 39 -7	64	25 05 -6	64	25 31 -5	64	25 57 -4	65	26 22 -3	65	295
66	23 46 7	64	24 12 6	64	24 38 5	65	25 03 3	65	25 28 2	65	294
67	22 52 6	64	23 18 5	64	23 44 4	65	24 10 4	65	24 35 3	65	293
68	21 58 5	64	22 24 4	64	22 50 3	65	23 16 3	65	23 41 2	65	292
69	21 05 5	64	21 31 4	64	21 57 4	65	22 22 2	65	22 47 1	65	291
70	20 11 -5	64	20 37 -4	64	21 03 -3	65	21 28 -2	65	21 53 -1	66	290
71	19 17 4	64	19 43 3	64	20 09 2	65	20 34 -1	65	20 59 0	66	289
72	18 24 4	64	18 50 3	65	19 15 2	65	19 40 0	65	20 05 +1	66	288
73	17 30 3	64	17 56 2	65	18 21 1	65	18 47 -1	65	19 12 0	65	287
74	16 36 3	64	17 02 2	65	17 28 1	65	17 53 0	65	18 18 +1	65	286
75	15 43 -3	64	16 08 -1	65	16 34 -1	65	16 59 +1	65	17 24 +2	65	285
76	14 49 2	64	15 15 1	65	15 40 0	65	16 05 1	65	16 30 2	65	284
77	13 55 -1	64	14 21 -1	65	14 46 +1	65	15 12 1	65	15 37 2	65	283
78	13 01 0	64	13 27 0	65	13 53 1	65	14 18 2	65	14 43 3	65	282
79	12 08 -1	64	12 33 +1	65	12 59 1	65	13 24 3	65	13 49 4	65	281
80	11 14 0	64	11 40 +1	65	12 05 +2	65	12 31 +3	65	12 56 +4	65	280
81	10 21 0	64	10 46 +2	65	11 12 2	65	11 37 3	65	12 02 5	65	279
82	...		...		10 18 +3	65	10 44 +3	65	11 09 5	65	278
83	...		...		...		...		10 15 +6	65	277
84	...		...		...		...		...		276
85	...		...		...		...		...		275

In South { For argument H.A. on the left, True Azimuth = $180^\circ + \text{Tabulated Azimuth}$. } See
 Latitudes { For argument H.A. on the right, True Azimuth = $180^\circ - \text{Tabulated Azimuth}$. } p. 91.

LAT.	5°		6°		7°		8°		9°		LAT.
H.A.	Alt.	Az.	Alt.	Az.	Alt.	Az.	Alt.	Az.	Alt.	Az.	H.A.
0	59 00-59	180	58 01-60	180	57 01-60	180	56 01-60	180	55 01-60	180	360
1	59 00 60	178	58 00 60	178	57 00 60	178	56 00 60	178	55 00 60	178	359
2	58 57 60	177	57 57 60	177	56 57 60	177	55 57 60	177	54 57 60	177	358
3	58 52 59	175	57 53 60	175	56 53 60	175	55 53 60	175	54 53 59	175	357
4	58 46 59	173	57 46 59	173	56 47 60	173	55 47 59	174	54 48 60	174	356
5	58 38-59	171	57 39-60	172	56 39-59	172	55 40-59	172	54 40-59	172	355
6	58 28 59	170	57 29 59	170	56 30 59	170	55 31 59	170	54 32 59	171	354
7	58 16 58	168	57 18 59	168	56 19 59	169	55 20 59	169	54 21 58	169	353
8	58 03 58	166	57 05 58	167	56 06 58	167	55 08 58	167	54 09 58	168	352
9	57 48 57	165	56 50 57	165	55 52 57	166	54 54 58	166	53 56 58	166	351
10	57 32-57	163	56 34-57	164	55 37-58	164	54 39-57	164	53 41-57	165	350
11	57 13 56	162	56 17 57	162	55 19 56	162	54 22 57	163	53 25 57	163	349
12	56 54 56	160	55 57 56	161	55 01 56	161	54 04 56	161	53 07 56	162	348
13	56 33 55	158	55 37 55	159	54 41 56	160	53 44 55	160	52 48 56	160	347
14	56 10 54	157	55 15 55	158	54 19 55	158	53 23 55	159	52 27 55	159	346
15	55 46-53	156	54 51-54	156	53 56-54	157	53 01-54	157	52 06-55	158	345
16	55 21 53	154	54 26 53	155	53 32 53	155	52 37 53	156	51 43 54	156	344
17	54 54 52	153	54 00 52	153	53 07 53	154	52 13 53	155	51 18 53	155	343
18	54 26 51	151	53 33 51	152	52 40 52	153	51 47 53	153	50 53 53	154	342
19	53 57 50	150	53 05 51	151	52 12 51	151	51 19 51	152	50 26 52	153	341
20	53 27-50	149	52 35-50	150	51 43-50	150	50 51-51	151	49 58-51	151	340
21	52 55 48	148	52 04 49	148	51 13 49	149	50 21 50	150	49 30 51	150	339
22	52 23 48	147	51 33 49	147	50 42 49	148	49 51 49	149	49 00 50	149	338
23	51 49 46	145	51 00 48	146	50 10 48	147	49 19 48	147	48 29 49	148	337
24	51 15 46	144	50 26 47	145	49 37 47	146	48 47 48	146	47 57 48	147	336
25	50 40-46	143	49 51-45	144	49 03-47	145	48 14-47	145	47 24-47	146	335
26	50 03 44	142	49 16 45	143	48 28 46	144	47 39 46	144	46 50 46	145	334
27	49 26 43	141	48 39 44	142	47 52 45	143	47 04 45	143	46 16 46	144	333
28	48 48 42	140	48 02 43	141	47 15 43	142	46 28 44	142	45 41 46	143	332
29	48 10 42	139	47 24 42	140	46 38 43	141	45 51 43	141	45 04 44	142	331
30	47 30-40	138	46 45-41	139	46 00-42	140	45 14-43	140	44 28-44	141	330
31	46 50 40	137	46 06 41	138	45 21 41	139	44 36 42	139	43 50 43	140	329
32	46 10 40	137	45 26 40	137	44 41 40	138	43 57 42	139	43 12 42	139	328
33	45 28 38	136	44 45 39	136	44 01 40	137	43 17 40	138	42 32 41	138	327
34	44 46 37	135	44 04 39	136	43 20 39	136	42 37 40	137	41 53 41	138	326
35	44 04-37	134	43 22-38	135	42 39-38	136	41 56-39	136	41 13-40	137	325
36	43 21 36	133	42 39 37	134	41 57 37	135	41 15 39	135	40 32 39	136	324
37	42 37 35	133	41 56 36	133	41 15 37	134	40 33 38	135	39 50 38	135	323
38	41 53 35	132	41 12 35	133	40 31 36	133	39 50 37	134	39 08 37	134	322
39	41 08 33	131	40 28 34	132	39 48 35	133	39 07 36	133	38 26 37	134	321
40	40 23-33	131	39 44-34	131	39 04-35	132	38 24-36	133	37 43-36	133	320
41	39 38 33	130	38 59 33	131	38 19 33	131	37 40 35	132	36 59 35	132	319
42	38 52 32	129	38 13 32	130	37 34 33	131	36 55 34	131	36 15 34	132	318
43	38 05 30	129	37 27 31	129	36 49 32	130	36 10 33	131	35 31 34	131	317
44	37 19 30	128	36 41 31	129	36 03 31	129	35 25 32	130	34 46 33	131	316
45	36 32-30	128	35 55-30	128	35 17-31	129	34 39-31	129	34 01-33	130	315

In North { For argument H.A. on the left, True Azimuth = $360^\circ - \text{Tabulated Azimuth}$. } See
latitudes { For argument H.A. on the right, True Azimuth = Tabulated Azimuth. } p. 90.

26°

DECLINATION CONTRARY NAME TO LATITUDE

26°

LAT.	5°		6°		7°		8°		9°		LAT.
H.A.	Alt.	Az.	Alt.	Az.	Alt.	Az.	Alt.	Az.	Alt.	Az.	H.A.
	°	° , d	°	° , d	°	° , d	°	° , d	°	° , d	°
45	36 32-30	128	35 55-30	128	35 17-31	129	34 39-31	129	34 01-33	130	315
46	35 44 28	127	35 08 30	128	34 31 31	128	33 53 31	129	33 15 31	129	314
47	34 56 27	127	34 20 28	127	33 44 30	128	33 07 31	128	32 29 31	129	313
48	34 08 27	126	33 33 28	127	32 57 29	127	32 20 30	128	31 43 30	128	312
49	33 20 26	126	32 45 28	126	32 09 28	127	31 33 29	127	30 56 29	128	311
50	32 31-25	125	31 57-27	126	31 21-27	126	30 46-29	127	30 10-30	127	310
51	31 43 26	125	31 08 26	125	30 33 27	126	29 58 28	126	29 22 28	127	309
52	30 53 24	124	30 19 25	125	29 45 26	125	29 10 27	126	28 35 28	126	308
53	30 04 24	124	29 30 25	124	28 56 26	125	28 22 27	125	27 47 28	126	307
54	29 14 23	124	28 41 24	124	28 07 25	124	27 33 26	125	26 59 27	125	306
55	28 24-22	123	27 51-23	124	27 18-24	124	26 44-25	124	26 10-26	125	305
56	27 34 22	123	27 02 23	123	26 29 24	124	25 55 24	124	25 22 26	124	304
57	26 44 21	122	26 12 23	123	25 39 23	123	25 06 24	124	24 33 25	124	303
58	25 54 21	122	25 22 22	123	24 49 22	123	24 17 24	123	23 43 24	124	302
59	25 03 20	122	24 31 21	122	23 59 22	123	23 27 23	123	22 54 24	123	301
60	24 12-20	121	23 41-21	122	23 09-22	122	22 37-22	123	22 05-24	123	300
61	23 21 19	121	22 50 20	121	22 19 21	122	21 47 22	122	21 15 23	123	299
62	22 30 19	121	21 59 19	121	21 28 20	122	20 57 22	122	20 25 22	122	298
63	21 39 18	121	21 08 19	121	20 37 20	121	20 06 21	122	19 35 22	122	297
64	20 47 17	120	20 17 19	121	19 46 19	121	19 15 20	121	18 44 21	121	296
65	19 56-17	120	19 26-18	120	18 55-19	121	18 25-20	121	17 54-21	121	295
66	19 04 17	120	18 34 17	120	18 04 18	120	17 34 19	121	17 03 20	121	294
67	18 12 16	119	17 42 16	120	17 13 18	120	16 43 19	120	16 12 19	121	293
68	17 20 15	119	16 51 17	119	16 21 17	120	15 51 18	120	15 21 19	120	292
69	16 28 15	119	15 59 16	119	15 29 16	119	15 00 18	120	14 30 18	120	291
70	15 36-15	119	15 07-15	119	14 38-16	119	14 08-16	119	13 39-18	120	290
71	14 43 13	119	14 15 15	119	13 46 16	119	13 17 17	119	12 48 18	119	289
72	13 51 13	118	13 23 14	119	12 54 15	119	12 25 16	119	11 56 17	119	288
73	12 59 13	118	12 30 13	118	12 02 15	119	11 33 15	119	11 05 17	119	287
74	12 06 12	118	11 38 13	118	11 10 14	118	10 42-15	118	10 13-16	119	286
75	11 14-12	118	10 46-13	118	10 18-14	118	...	...	...	...	285
76	10 21-11	118	...	...	...	...	...	...	...	...	284
77	...	...	...	...	...	...	...	...	...	...	283
78	...	...	...	...	...	...	...	...	...	...	282
79	...	...	...	...	...	...	...	...	...	...	281
80	...	...	...	...	...	...	...	...	...	...	280

In South { For argument H.A. on the left, True Azimuth = $180^\circ + \text{Tabulated Azimuth}$. } See
 Latitudes { For argument H.A. on the right, True Azimuth = $180^\circ - \text{Tabulated Azimuth}$. } p. 91.

LAT.	5°		6°		7°		8°		9°		LAT.
H.A.	Alt.	Az.	Alt.	Az.	Alt.	Az.	Alt.	Az.	Alt.	Az.	H.A.
0	68 00-60	0	69 00-60	0	70 00-60	0	71 00-60	0	72 00-60	0	360
1	67 59 60	2	68 59 60	2	69 59 60	3	70 59 60	3	71 59 60	3	359
2	67 55 59	5	68 55 60	5	69 55 60	5	70 55 60	5	71 54 59	6	358
3	67 49 59	7	68 49 60	7	69 48 59	8	70 48 60	8	71 47 59	9	357
4	67 41 59	9	68 40 59	10	69 39 59	10	70 38 59	11	71 37 59	11	356
5	67 30-59	12	68 28-58	12	69 27-58	13	70 25-58	13	71 24-58	14	355
6	67 16 57	14	68 15 58	15	69 13 58	15	70 10 57	16	71 08 57	17	354
7	67 01 57	16	67 58 56	17	68 56 57	18	69 53 57	18	70 50 56	19	353
8	66 43 56	18	67 40 56	19	68 37 56	20	69 33 55	21	70 29 55	22	352
9	66 23 55	20	67 20 56	21	68 15 54	22	69 11 55	23	70 06 54	24	351
10	66 02-55	22	66 57-54	23	67 52-54	24	68 46-53	25	69 40-52	26	350
11	65 38 54	24	66 32 53	25	67 26 52	26	68 20 52	27	69 13 51	29	349
12	65 12 52	26	66 06 52	27	66 59 51	28	67 52 51	29	68 44 50	31	348
13	64 45 51	28	65 38 51	29	66 30 50	30	67 22 50	31	68 12 48	33	347
14	64 16 50	30	65 08 49	31	65 59 48	32	66 50 48	33	67 40 47	35	346
15	63 46-49	31	64 37-49	33	65 27-48	34	66 17-47	35	67 05-45	36	345
16	63 14 48	33	64 04 47	34	64 53 46	35	65 42 46	37	66 30 45	38	344
17	62 41 47	35	63 30 46	36	64 18 45	37	65 06 44	38	65 52 43	40	343
18	62 06 45	36	62 54 44	37	63 42 44	38	64 28 42	40	65 14 42	41	342
19	61 31 45	37	62 18 44	39	63 04 42	40	63 50 42	41	64 35 41	42	341
20	60 54-44	39	61 40-42	40	62 26-42	41	63 10-40	42	63 54-39	44	340
21	60 16 42	40	61 01 41	41	61 46 40	42	62 30 39	44	63 13 38	45	339
22	59 37 41	41	60 21 40	42	61 05 39	44	61 48 38	45	62 30 36	46	338
23	58 57 40	42	59 41 39	44	60 24 38	45	61 06 37	46	61 47 35	47	337
24	58 16 39	44	58 59 38	45	59 41 36	46	60 23 36	47	61 03 34	48	336
25	57 35-38	45	58 17-37	46	58 58-35	47	59 39-34	48	60 18-33	49	335
26	56 52 36	46	57 34 36	47	58 14 34	48	58 54 33	49	59 33 32	50	334
27	56 09 35	47	56 50 34	48	57 30 33	49	58 09 32	50	58 47 31	51	333
28	55 25 34	47	56 06 34	49	56 45 32	50	57 23 31	51	58 00 29	52	332
29	54 41 33	48	55 21 33	49	55 59 31	51	56 37 30	52	57 13 28	53	331
30	53 56-32	49	54 35-31	50	55 13-30	51	55 50-29	52	56 26-28	54	330
31	53 11 32	50	53 49 30	51	54 26 29	52	55 03 28	53	55 38 27	54	329
32	52 25 31	51	53 02 29	52	53 39 28	53	54 15 27	54	54 50 26	55	328
33	51 38 29	51	52 15 28	52	52 51 27	53	53 27 26	55	54 01 25	56	327
34	50 51 28	52	51 28 28	53	52 03 26	54	52 38 25	55	53 12 24	56	326
35	50 04-28	53	50 40-27	54	51 15-26	55	51 49-24	56	52 22-23	57	325
36	49 16 27	53	49 52 26	54	50 26 24	55	51 00 23	56	51 33 22	57	324
37	48 28 26	54	49 03 25	55	49 37 24	56	50 10 22	57	50 43 22	58	323
38	47 40 26	55	48 14 24	55	48 48 23	56	49 20 21	57	49 52 20	58	322
39	46 51 25	55	47 25 24	56	47 58 22	57	48 30 21	58	49 02 20	59	321
40	46 02-24	56	46 35-22	56	47 08-21	57	47 40-20	58	48 11-19	59	320
41	45 12 23	56	45 45 21	57	46 18 21	58	46 49 19	59	47 20 18	60	319
42	44 23 23	57	44 55 21	57	45 27 20	58	45 59 19	59	46 29 17	60	318
43	43 33 22	57	44 05 20	58	44 37 19	59	45 08 18	59	45 38 17	60	317
44	42 42 20	57	43 14 19	58	43 46 19	59	44 16 17	60	44 46 16	61	316
45	41 52-20	58	42 24-19	59	42 55-18	59	43 25-17	60	43 54-15	61	315

In North { For argument H.A. on the left, True Azimuth = 360° - Tabulated Azimuth. } See
 Latitudes { For argument H.A. on the right, True Azimuth = Tabulated Azimuth. } p. 90.

27°

DECLINATION SAME NAME AS LATITUDE

27°

LAT.	5°		6°		7°		8°		9°		LAT.
H.A.	Alt.	Az.	Alt.	Az.	Alt.	Az.	Alt.	Az.	Alt.	Az.	H.A.
	°	°	°	°	°	°	°	°	°	°	°
45	41 52-20	58	42 24-19	59	42 55-18	59	43 25-17	60	43 54-15	61	315
46	41 01 19	58	41 33 18	59	42 03 17	60	42 33 15	60	43 03 15	61	314
47	40 11 19	58	40 42 18	59	41 12 16	60	41 42 16	61	42 10 13	62	313
48	39 20 18	59	39 50 16	60	40 20 15	60	40 50 15	61	41 18 13	62	312
49	38 28 17	59	38 59 16	60	39 29 15	61	39 58 14	61	40 26 13	62	311
50	37 37-17	59	38 07-15	60	38 37-15	61	39 06-14	62	39 34-12	62	310
51	36 45 15	60	37 15 14	60	37 45 14	61	38 13 12	62	38 41 11	62	309
52	35 54 16	60	36 23 14	61	36 52 13	61	37 21 12	62	37 49 11	63	308
53	35 02 15	60	35 31 13	61	36 00 12	62	36 28 11	62	36 56 10	63	307
54	34 10 14	61	34 39 13	61	35 08 12	62	35 36 11	62	36 03 9	63	306
55	33 18-14	61	33 47-12	61	34 15-11	62	34 43-10	63	35 10-9	63	305
56	32 26 13	61	32 54 11	62	33 23 11	62	33 50 9	63	34 18 9	63	304
57	31 33 12	61	32 02 11	62	32 30 10	62	32 58 9	63	33 25 8	64	303
58	30 41 12	61	31 09 10	62	31 37 9	63	32 05 9	63	32 32 8	64	302
59	29 48 11	62	30 17 10	62	30 44 8	63	31 12 8	63	31 38 6	64	301
60	28 56-11	62	29 24-9	62	29 52-9	63	30 19-8	63	30 45-6	64	300
61	28 03 10	62	28 31 9	62	28 59 8	63	29 26 7	63	29 52 6	64	299
62	27 10 9	62	27 38 8	63	28 06 8	63	28 32 6	64	28 59 5	64	298
63	26 18 9	62	26 45 7	63	27 13 7	63	27 39 5	64	28 06 5	64	297
64	25 25 9	62	25 52 7	63	26 19 6	63	26 46 5	64	27 12 4	64	296
65	24 32-8	63	24 59-6	63	25 26-5	63	25 53-5	64	26 19-3	64	295
66	23 39 7	63	24 06 6	63	24 33 5	63	25 00 4	64	25 26 3	64	294
67	22 46 7	63	23 13 6	63	23 40 5	64	24 06 3	64	24 32 2	64	293
68	21 53 6	63	22 20 5	63	22 47 5	64	23 13 3	64	23 39 2	64	292
69	21 00 6	63	21 27 5	63	21 53 3	64	22 20 3	64	22 46 2	64	291
70	20 06-5	63	20 33-4	63	21 00-3	64	21 26-2	64	21 52-1	64	290
71	19 13 4	63	19 40 4	63	20 07 3	64	20 33 2	64	20 59-1	64	289
72	18 20 4	63	18 47 3	63	19 13 2	64	19 40-1	64	20 06 0	64	288
73	17 27 4	63	17 54 3	64	18 20 2	64	18 46 0	64	19 12 +1	64	287
74	16 33 3	63	17 00 2	64	17 27-1	64	17 53 0	64	18 19 1	64	286
75	15 40-2	63	16 07-2	64	16 33 0	64	17 00 0	64	17 26 +1	64	285
76	14 47 2	63	15 14-1	64	15 40 0	64	16 06 +1	64	16 32 2	64	284
77	13 54 2	63	14 20 0	64	14 47 0	64	15 13 1	64	15 39 2	64	283
78	13 01-2	63	13 27 0	64	13 54 0	64	14 20 2	64	14 46 3	64	282
79	12 07 0	63	12 34 0	64	13 00 +2	64	13 27 2	64	13 53 3	64	281
80	11 14 0	63	11 41 +1	64	12 07 +2	64	12 34 +2	64	13 00 +3	64	280
81	10 21 0	63	10 48 +1	64	11 14 2	64	11 40 4	64	12 07 4	64	279
82	...		...		10 21 +3	64	10 47 +4	64	11 14 4	64	278
83	...		...		...		...		10 21 +5	64	277
84	...		...		...		...		...		276
85	...		...		...		...		...		275

In South { For argument H.A. on the left, True Azimuth = 180° + Tabulated Azimuth. } See
 Latitudes { For argument H.A. on the right, True Azimuth = 180° - Tabulated Azimuth. } p. 91.

LAT.	5°		6°		7°		8°		9°		LAT.
H.A.	Alt.	Az.	Alt.	Az.	Alt.	Az.	Alt.	Az.	Alt.	Az.	H.A.
0	58 01-60	180	57 01-60	180	56 01-60	180	55 01-60	180	54 01-60	180	360
1	58 00 60	178	57 00 60	178	56 00 60	178	55 00 60	178	54 00 60	178	359
2	57 57 60	177	56 57 60	177	55 57 60	177	54 57 60	177	53 57 59	177	358
3	57 53 60	175	56 53 60	175	55 53 60	175	54 53 59	175	53 54 60	175	357
4	57 47 60	173	56 47 60	173	55 47 59	174	54 48 60	174	53 48 59	174	356
5	57 39-59	172	56 39-59	172	55 40-59	172	54 41-60	172	53 41-59	172	355
6	57 29 59	170	56 30 59	170	55 31 59	171	54 32 59	171	53 33 60	171	354
7	57 18 58	168	56 19 58	169	55 20 58	169	54 21 58	169	53 23 59	170	353
8	57 05 58	167	56 07 58	167	55 08 58	167	54 10 59	168	53 11 58	168	352
9	56 51 58	165	55 53 58	166	54 55 58	166	53 56 58	166	52 58 58	167	351
10	56 35-57	164	55 37-57	164	54 39-57	164	53 42-58	165	52 44-58	165	350
11	56 17 56	162	55 20 57	163	54 23 57	163	53 25 57	163	52 28 57	164	349
12	55 58 56	161	55 01 56	161	54 05 57	162	53 08 57	162	52 11 57	162	348
13	55 38 55	159	54 42 56	160	53 45 55	160	52 49 56	161	51 52 56	161	347
14	55 16 55	158	54 20 55	158	53 24 55	159	52 28 55	159	51 32 55	160	346
15	54 53-54	156	53 57-54	157	53 02-54	157	52 07-55	158	51 11-55	158	345
16	54 28 53	155	53 33 53	156	52 39 54	156	51 44 54	157	50 49 55	157	344
17	54 02 52	154	53 08 52	154	52 14 53	155	51 20 54	155	50 25 54	156	343
18	53 35 52	152	52 42 52	153	51 48 52	154	50 54 52	154	50 00 53	155	342
19	53 07 51	151	52 14 51	152	51 21 52	152	50 28 52	153	49 34 52	153	341
20	52 37-50	150	51 45-50	151	50 53-51	151	50 00-51	152	49 07-51	152	340
21	52 07 49	149	51 15 49	149	50 24 50	150	49 31 50	151	48 39 51	151	339
22	51 35 48	148	50 44 48	148	49 53 49	149	49 02 50	149	48 10 50	150	338
23	51 03 48	146	50 12 48	147	49 22 49	148	48 31 49	148	47 40 50	149	337
24	50 29 47	145	49 39 47	146	48 50 48	147	47 59 48	147	47 09 49	148	336
25	49 54-45	144	49 06-47	145	48 16-46	146	47 27-48	146	46 37-48	147	335
26	49 19 45	143	48 31 46	144	47 42 46	145	46 53 46	145	46 04 47	146	334
27	48 43 44	142	47 55 44	143	47 07 45	144	46 19 46	144	45 30 46	145	333
28	48 06 43	141	47 19 44	142	46 32 45	143	45 44 45	143	44 55 45	144	332
29	47 28 42	140	46 42 43	141	45 55 44	142	45 08 44	142	44 20 45	143	331
30	46 50-42	139	46 04-42	140	45 18-43	141	44 31-43	141	43 44-44	142	330
31	46 10 40	139	45 25 41	139	44 40 42	140	43 54 43	140	43 07 43	141	329
32	45 30 39	138	44 46 41	138	44 01 41	139	43 15 41	140	42 30 43	140	328
33	44 50 39	137	44 06 40	138	43 21 40	138	42 37 42	139	41 51 41	139	327
34	44 09 38	136	43 25 39	137	42 41 39	137	41 57 40	138	41 12 41	139	326
35	43 27-37	135	42 44-38	136	42 01-39	137	41 17-40	137	40 33-40	138	325
36	42 45 37	135	42 02 37	135	41 20 38	136	40 36 38	136	39 53 40	137	324
37	42 02 36	134	41 20 37	134	40 38 37	135	39 55 38	136	39 12 39	136	323
38	41 18 35	133	40 37 36	134	39 55 36	134	39 13 37	135	38 31 38	136	322
39	40 35 35	132	39 54 35	133	39 13 36	134	38 31 36	134	37 49 37	135	321
40	39 50-33	132	39 10-34	132	38 29-35	133	37 48-36	134	37 07-37	134	320
41	39 05 32	131	38 26 34	132	37 46 35	132	37 05 35	133	36 24 36	133	319
42	38 20 32	131	37 41 33	131	37 01 33	132	36 21 34	132	35 41 35	133	318
43	37 35 32	130	36 56 32	131	36 17 33	131	35 37 34	132	34 57 34	132	317
44	36 49 31	129	36 10 31	130	35 32 32	130	34 53 33	131	34 13 34	132	316
45	36 02-29	129	35 25-31	129	34 46-31	130	34 08-33	130	33 28-33	131	315

In North { For argument H.A. on the left, True Azimuth = $360^\circ - \text{Tabulated Azimuth}$. } See
 Latitudes { For argument H.A. on the right, True Azimuth = Tabulated Azimuth. } p. 90.

27°

DECLINATION CONTRARY NAME TO LATITUDE

27°

LAT.	5°		6°		7°		8°		9°		LAT.
H.A.	Alt.	Az.	Alt.	Az.	Alt.	Az.	Alt.	Az.	Alt.	Az.	H.A.
	° ' d		° ' d		° ' d		° ' d		° ' d		
45	36 02-29	129	35 25-31	129	34 46-31	130	34 08-33	130	33 28-33	131	315
46	35 16 29	128	34 38 30	129	34 00 30	129	33 22 31	130	32 44 33	130	314
47	34 29 29	128	33 52 30	128	33 14 30	129	32 36 30	129	31 58 31	130	313
48	33 41 27	127	33 05 29	128	32 28 30	128	31 50 30	129	31 13 31	129	312
49	32 54 27	127	32 17 27	127	31 41 29	128	31 04 30	128	30 27 31	129	311
50	32 06-27	126	31 30-27	127	30 54-28	127	30 17-29	128	29 40-29	128	310
51	31 17 25	126	30 42 27	126	30 06 27	127	29 30 28	127	28 54 29	128	309
52	30 29 25	125	29 54 26	126	29 19 27	126	28 43 28	127	28 07 29	127	308
53	29 40 24	125	29 05 25	126	28 30 26	126	27 55 27	126	27 19 27	127	307
54	28 51 24	125	28 17 25	125	27 42 25	126	27 07 26	126	26 32 27	126	306
55	28 02-23	124	27 28-24	125	26 54-25	125	26 19-26	126	25 44-27	126	305
56	27 12 22	124	26 39 24	124	26 05 24	125	25 31 26	125	24 56 26	125	304
57	26 23 22	123	25 49 22	124	25 16 24	124	24 42 25	125	24 08 26	125	303
58	25 33 21	123	25 00 22	124	24 27 23	124	23 53 24	124	23 19 25	125	302
59	24 43 21	123	24 10 21	123	23 37 22	124	23 04 23	124	22 30 24	124	301
60	23 52-20	122	23 20-21	123	22 47-21	123	22 15-23	124	21 41-23	124	300
61	23 02 20	122	22 30 20	123	21 58 22	123	21 25 22	123	20 52 23	124	299
62	22 11 19	122	21 40 20	122	21 08 21	123	20 35 21	123	20 03 23	123	298
63	21 21 19	122	20 49 19	122	20 17 20	122	19 45 21	123	19 13 22	123	297
64	20 30 18	121	19 58 18	122	19 27 20	122	18 55 20	122	18 23 21	122	296
65	19 39-18	121	19 08-18	121	18 36-19	122	18 05-20	122	17 33-21	122	295
66	18 47 16	121	18 17 18	121	17 46 19	121	17 15 20	122	16 43 20	122	294
67	17 56 16	120	17 26 17	121	16 55 18	121	16 24 19	121	15 53 20	122	293
68	17 05 16	120	16 34 16	120	16 04 17	121	15 33 18	121	15 02 19	121	292
69	16 13 15	120	15 43 16	120	15 13 17	120	14 42 17	121	14 12 19	121	291
70	15 21-14	120	14 52-16	120	14 22-17	120	13 52-18	120	13 21-18	121	290
71	14 30 14	120	14 00 15	120	13 30 15	120	13 00 16	120	12 30 17	120	289
72	13 38 14	119	13 09 15	120	12 39 15	120	12 09 16	120	11 39 17	120	288
73	12 46 13	119	12 17 14	119	11 47 14	120	11 18 16	120	10 48-16	120	287
74	11 54 12	119	11 25 13	119	10 56 14	119	10 27-15	119	...	...	286
75	11 02-12	119	10 33-13	119	10 04-13	119	...	...	...	...	285
76	10 10-12	119	...	...	...	...	...	...	...	...	284
77	...	...	...	...	...	...	...	...	...	...	283
78	...	...	...	...	...	...	...	...	...	...	282
79	...	...	...	...	...	...	...	...	...	...	281
80	...	...	...	...	...	...	...	...	...	...	280

In South { For argument H.A. on the left, True Azimuth = $180^\circ + \text{Tabulated Azimuth}$. } See
 Latitudes { For argument H.A. on the right, True Azimuth = $180^\circ - \text{Tabulated Azimuth}$. } p. 91.

28°

DECLINATION SAME NAME AS LATITUDE

28°

LAT.	5°		6°		7°		8°		9°		LAT.
H.A.	Alt.	Az.	Alt.	Az.	Alt.	Az.	Alt.	Az.	Alt.	Az.	H.A.
0	67 00-60	0	68 00-60	0	69 00-60	0	70 00-60	0	71 00-60	0	360
1	66 59 60	2	67 59 60	2	68 59 60	2	69 59 60	3	70 59 60	3	359
2	66 56 60	5	67 55 59	5	68 55 60	5	69 55 60	5	70 55 60	5	358
3	66 50 60	7	67 49 59	7	68 49 60	7	69 48 59	8	70 48 60	8	357
4	66 42 59	9	67 41 59	9	68 40 59	10	69 39 59	10	70 38 59	11	356
5	66 31-58	11	67 30-58	12	68 29-59	12	69 27-58	13	70 26-58	13	355
6	66 19 58	13	67 17 58	14	68 15 58	14	69 13 57	15	70 11 57	16	354
7	66 04 58	15	67 02 58	16	67 59 57	17	68 56 56	17	69 54 57	18	353
8	65 47 57	17	66 44 56	18	67 41 56	19	68 38 56	20	69 34 56	21	352
9	65 28 56	19	66 24 55	20	67 21 55	21	68 16 54	22	69 12 54	23	351
10	65 07-55	21	66 03-55	22	66 58-54	23	67 53-53	24	68 48-53	25	350
11	64 44 53	23	65 39 53	24	66 34 53	25	67 28 52	26	68 22 52	27	349
12	64 20 53	25	65 14 52	26	66 08 52	27	67 01 51	28	67 54 51	29	348
13	63 54 52	27	64 47 51	28	65 40 51	29	66 32 50	30	67 24 49	31	347
14	63 26 51	29	64 19 51	30	65 11 50	31	66 02 49	32	66 53 49	33	346
15	62 57-50	30	63 48-49	31	64 39-48	32	65 30-48	33	66 20-47	35	345
16	62 26 49	32	63 17 48	33	64 07 47	34	64 56 46	35	65 45 45	36	344
17	61 54 47	33	62 44 47	34	63 33 46	35	64 22 45	37	65 09 44	38	343
18	61 21 47	35	62 10 46	36	62 58 45	37	63 46 44	38	64 32 42	39	342
19	60 46 45	36	61 34 44	37	62 22 44	38	63 08 42	40	63 54 41	41	341
20	60 10-44	37	60 58-44	38	61 44-42	40	62 30-41	41	63 15-40	42	340
21	59 34 43	39	60 20 42	40	61 06 41	41	61 51 40	42	62 35 39	43	339
22	58 56 42	40	59 41 41	41	60 26 40	42	61 10 38	43	61 54 38	45	338
23	58 17 41	41	59 02 40	42	59 46 39	43	60 29 37	44	61 12 37	46	337
24	57 37 39	42	58 21 38	43	59 05 38	44	59 47 36	46	60 29 36	47	336
25	56 57-39	43	57 40-37	44	58 23-37	45	59 05-36	47	59 45-34	48	335
26	56 16 38	44	56 58 36	45	57 40 35	46	58 21 34	48	59 01 33	49	334
27	55 34 37	45	56 16 36	46	56 57 35	47	57 37 33	48	58 16 32	50	333
28	54 51 36	46	55 32 34	47	56 13 34	48	56 52 32	49	57 31 31	50	332
29	54 08 35	47	54 48 33	48	55 28 32	49	56 07 31	50	56 45 30	51	331
30	53 24-34	48	54 04-33	49	54 43-31	50	55 21-30	51	55 58-28	52	330
31	52 39 32	49	53 19 32	50	53 57 30	51	54 35 29	52	55 11 27	53	329
32	51 54 31	49	52 33 31	50	53 11 30	51	53 48 28	52	54 24 27	53	328
33	51 09 31	50	51 47 30	51	52 24 28	52	53 01 28	53	53 36 26	54	327
34	50 23 30	51	51 00 28	52	51 37 27	53	52 13 26	54	52 48 25	55	326
35	49 36-29	51	50 13-27	52	50 49-26	53	51 25-25	54	51 59-24	55	325
36	48 49 28	52	49 26 27	53	50 02 26	54	50 37 25	55	51 11 24	56	324
37	48 02 27	53	48 38 26	54	49 13 24	54	49 48 24	55	50 21 22	56	323
38	47 14 26	53	47 50 25	54	48 25 24	55	48 59 23	56	49 32 22	57	322
39	46 26 25	54	47 01 24	55	47 36 23	55	48 09 21	56	48 42 20	57	321
40	45 38-25	54	46 13-24	55	46 47-23	56	47 20-21	57	47 52-20	58	320
41	44 49 23	55	45 24 23	56	45 57 21	56	46 30 20	57	47 02 19	58	319
42	44 00 23	55	44 34 22	56	45 07 20	57	45 40 20	58	46 12 19	59	318
43	43 11 22	56	43 45 21	56	44 18 20	57	44 50 19	58	45 21 18	59	317
44	42 22 22	56	42 55 20	57	43 27 19	58	43 59 18	58	44 30 17	59	316
45	41 32-21	56	42 05-20	57	42 37-19	58	43 08-17	59	43 39-16	60	315

In North { For argument H.A. on the left, True Azimuth = 360° - Tabulated Azimuth. } See
 Latitudes { For argument H.A. on the right, True Azimuth = Tabulated Azimuth. } p. 90

28°

DECLINATION SAME NAME AS LATITUDE

28°

LAT.	5°		6°		7°		8°		9°		LAT.
H.A.	Alt.	Az.	Alt.	Az.	Alt.	Az.	Alt.	Az.	Alt.	Az.	H.A.
	° ' ' d	° ' ' d	° ' ' d	° ' ' d	° ' ' d	° ' ' d	° ' ' d	° ' ' d	° ' ' d	° ' ' d	
45	41 32-21	56	42 05-20	57	42 37-19	58	43 08-17	59	43 39-16	60	315
46	40 42 20	57	41 15 19	58	41 46 17	58	42 18 17	59	42 48 16	60	314
47	39 52 19	57	40 24 18	58	40 56 17	59	41 26 16	59	41 57 15	60	313
48	39 02 19	58	39 34 18	58	40 05 17	59	40 35 15	60	41 05 14	60	312
49	38 11 18	58	38 43 17	59	39 14 16	59	39 44 15	60	40 13 13	61	311
50	37 20-17	58	37 52-16	59	38 22-15	60	38 52-14	60	39 22-13	61	310
51	36 30 17	59	37 01 16	59	37 31 14	60	38 01 14	61	38 30 12	61	309
52	35 38 15	59	36 09 15	59	36 39 13	60	37 09 13	61	37 38 12	61	308
53	34 47 15	59	35 18 14	60	35 48 13	60	36 17 12	61	36 46 11	62	307
54	33 56 15	59	34 26 13	60	34 56 13	61	35 25 11	61	35 54 11	62	306
55	33 04-14	60	33 35-13	60	34 04-12	61	34 33-11	61	35 01 -9	62	305
56	32 13 14	60	32 43 13	60	33 12 11	61	33 41 10	62	34 09 9	62	304
57	31 21 13	60	31 51 12	61	32 20 11	61	32 49 10	62	33 17 9	62	303
58	30 29 12	60	30 59 11	61	31 28 10	61	31 56 9	62	32 24 8	62	302
59	29 37 11	61	30 07 11	61	30 36 10	62	31 04 9	62	31 32 8	63	301
60	28 45-11	61	29 15-10	61	29 43 -9	62	30 11 -8	62	30 39 -7	63	300
61	27 53 10	61	28 22 9	61	28 51 9	62	29 19 7	62	29 46 6	63	299
62	27 01 10	61	27 30 9	61	27 58 8	62	28 26 7	62	28 54 6	63	298
63	26 09 9	61	26 38 9	62	27 06 7	62	27 34 7	63	28 01 5	63	297
64	25 16 8	61	25 45 8	62	26 13 7	62	26 41 6	63	27 08 4	63	296
65	24 24 -8	61	24 53 -8	62	25 21 -7	62	25 48 -5	63	26 16 -5	63	295
66	23 32 8	62	24 00 7	62	24 28 6	62	24 56 5	63	25 23 4	63	294
67	22 39 7	62	23 07 6	62	23 35 5	62	24 03 4	63	24 30 3	63	293
68	21 47 7	62	22 15 6	62	22 42 4	63	23 10 4	63	23 37 3	63	292
69	20 54 6	62	21 22 5	62	21 50 4	63	22 17 3	63	22 44 2	63	291
70	20 01 -5	62	20 29 -4	62	20 57 -4	63	21 24 -2	63	21 51 -1	63	290
71	19 09 5	62	19 36 3	62	20 04 3	63	20 31 2	63	20 58 1	63	289
72	18 16 5	62	18 44 4	62	19 11 2	63	19 39 2	63	20 06 -1	63	288
73	17 23 4	62	17 51 3	62	18 18 2	63	18 46 1	63	19 13 0	63	287
74	16 30 3	62	16 58 2	63	17 26 2	63	17 53 -1	63	18 20 0	63	286
75	15 38 -3	62	16 05 -2	63	16 33 -1	63	17 00 0	63	17 27 +1	63	285
76	14 45 2	62	15 13 2	63	15 40 0	63	16 07 +1	63	16 34 2	63	284
77	13 52 2	62	14 20 -1	63	14 47 0	63	15 14 1	63	15 41 2	63	283
78	12 59 1	62	13 27 0	63	13 54 +1	63	14 22 1	63	14 49 2	63	282
79	12 07 -1	62	12 34 0	63	13 02 1	63	13 29 2	63	13 56 3	63	281
80	11 14 0	62	11 42 0	63	12 09 +2	63	12 36 +3	63	13 03 +4	63	280
81	10 21 +1	62	10 49 +1	63	11 16 2	63	11 44 3	63	12 11 4	63	279
82	...		...		10 24 +2	63	10 51 +3	63	11 18 4	63	278
83	...		...		...		...		10 26 +4	63	277
84	...		...		...		...		...		276
85	...		...		...		...		...		275

In South { For argument H.A. on the left, True Azimuth = $180^\circ + \text{Tabulated Azimuth}$. } See
 Latitudes { For argument H.A. on the right, True Azimuth = $180^\circ - \text{Tabulated Azimuth}$. } p. 91.

LAT.	5°		6°		7°		8°		9°		LAT.
H.A.	Alt.	Az.	Alt.	Az.	Alt.	Az.	Alt.	Az.	Alt.	Az.	H.A.
0	57 01-60	180	56 01-60	180	55 01-60	180	54 01-60	180	53 01-60	180	360
1	57 00 60	178	56 00 60	178	55 00 60	178	54 00 60	178	53 00 60	179	359
2	56 57 60	177	55 57 60	177	54 57 59	177	53 57 59	177	52 58 60	177	358
3	56 53 60	175	55 53 60	175	54 53 59	175	53 54 60	176	52 54 60	176	357
4	56 47 59	174	55 47 59	174	54 48 60	174	53 48 59	174	52 49 60	174	356
5	56 40-60	172	55 40-59	172	54 41-60	172	53 41-59	173	52 42-60	173	355
6	56 30 59	170	55 31 59	171	54 32 59	171	53 33 59	171	52 33 59	171	354
7	56 20 59	169	55 21 59	169	54 22 59	169	53 23 59	170	52 24 59	170	353
8	56 07 58	167	55 09 59	168	54 10 58	168	53 11 58	168	52 13 59	168	352
9	55 53 57	166	54 55 58	166	53 57 58	166	52 58 58	167	52 00 58	167	351
10	55 38-57	164	54 40-57	165	53 42-57	165	52 44-57	165	51 46-58	166	350
11	55 21 57	163	54 23 56	163	53 26 57	164	52 28 57	164	51 31 58	164	349
12	55 02 56	161	54 05 56	162	53 08 56	162	52 11 56	163	51 14 57	163	348
13	54 43 56	160	53 46 56	160	52 50 56	161	51 53 56	161	50 56 56	162	347
14	54 21 54	159	53 25 55	159	52 29 55	159	51 33 55	160	50 37 56	160	346
15	53 59-54	157	53 03-54	158	52 08-55	158	51 12-55	159	50 16-55	159	345
16	53 35 53	156	52 40 54	156	51 45 54	157	50 50 54	157	49 54 54	158	344
17	53 10 53	154	52 16 53	155	51 21 53	156	50 26 53	156	49 31 53	157	343
18	52 43 51	153	51 50 52	154	50 56 53	154	50 02 53	155	49 07 53	155	342
19	52 16 51	152	51 23 52	153	50 29 51	153	49 36 52	154	48 42 53	154	341
20	51 47-50	151	50 55-51	151	50 02-51	152	49 09-51	153	48 16-52	153	340
21	51 18 50	150	50 26 50	150	49 34 51	151	48 41 51	151	47 48 51	152	339
22	50 47 49	148	49 56 49	149	49 04 50	150	48 12 50	150	47 20 51	151	338
23	50 15 48	147	49 24 48	148	48 33 48	149	47 42 49	149	46 50 49	150	337
24	49 42 47	146	48 52 47	147	48 02 48	148	47 11 48	148	46 20 49	149	336
25	49 09-46	145	48 19-46	146	47 30-48	146	46 39-47	147	45 49-48	148	335
26	48 34 45	144	47 45 45	145	46 56 46	145	46 07 47	146	45 17 48	147	334
27	47 59 45	143	47 11 45	144	46 22 46	144	45 33 46	145	44 44 47	146	333
28	47 23 44	142	46 35 44	143	45 47 45	144	44 59 46	144	44 10 46	145	332
29	46 46 43	141	45 59 44	142	45 11 44	143	44 24 45	143	43 35 45	144	331
30	46 08-42	140	45 22-43	141	44 35-43	142	43 48-44	142	43 00-45	143	330
31	45 30 41	140	44 44 42	140	43 58 43	141	43 11 43	141	42 24 44	142	329
32	44 51 41	139	44 05 41	139	43 20 42	140	42 34 43	141	41 47 43	141	328
33	44 11 40	138	43 26 40	139	42 41 41	139	41 55 41	140	41 10 43	140	327
34	43 31 39	137	42 46 39	138	42 02 40	138	41 17 41	139	40 31 41	140	326
35	42 50-38	136	42 06-39	137	41 22-39	138	40 37-40	138	39 53-41	139	325
36	42 08 37	136	41 25 38	136	40 42 39	137	39 58 40	137	39 13 40	138	324
37	41 26 36	135	40 43 37	135	40 01 38	136	39 17 38	137	38 33 39	137	323
38	40 43 35	134	40 01 36	135	39 19 37	135	38 36 38	136	37 53 39	136	322
39	40 00 34	134	39 19 36	134	38 37 36	135	37 55 38	135	37 12 38	136	321
40	39 17-34	133	38 36-35	133	37 54-35	134	37 12-36	135	36 30-37	135	320
41	38 33 33	132	37 52 34	133	37 11 35	133	36 30 36	134	35 48 36	134	319
42	37 48 32	132	37 08 33	132	36 28 34	133	35 47 35	133	35 06 36	134	318
43	37 03 31	131	36 24 33	132	35 44 33	132	35 03 34	133	34 23 35	133	317
44	36 18 31	130	35 39 32	131	35 00 33	132	34 20 34	132	33 39 34	133	316
45	35 33-31	130	34 54-31	130	34 15-32	131	33 35-32	131	32 55-33	132	315

In North { For argument H.A. on the left, True Azimuth = $360^\circ - \text{Tabulated Azimuth}$. } See
 Latitudes { For argument H.A. on the right, True Azimuth = Tabulated Azimuth. } p. 90.

28°

DECLINATION **CONTRARY** NAME TO LATITUDE

28°

LAT.	5°		6°		7°		8°		9°		LAT.
H.A.	Alt.	Az.	Alt.	Az.	Alt.	Az.	Alt.	Az.	Alt.	Az.	H.A.
°	°	d	°	d	°	d	°	d	°	d	°
45	35 33-31	130	34 54-31	130	34 15-32	131	33 35-32	131	32 55-33	132	315
46	34 47 30	129	34 08 30	130	33 30 32	130	32 51 32	131	32 11 33	131	314
47	34 00 29	129	33 22 29	129	32 44 30	130	32 06 32	130	31 27 33	131	313
48	33 14 29	128	32 36 29	129	31 58 30	129	31 20 31	130	30 42 32	130	312
49	32 27 28	128	31 50 29	128	31 12 29	129	30 34 30	129	29 56 31	130	311
50	31 39-27	127	31 03-28	128	30 26-29	128	29 48-29	129	29 11-31	129	310
51	30 52 26	127	30 15 27	127	29 39 28	128	29 02 29	128	28 25 30	129	309
52	30 04 26	127	29 28 26	127	28 52 27	127	28 15 28	128	27 38 29	128	308
53	29 16 25	126	28 40 26	127	28 04 26	127	27 28 27	127	26 52 29	128	307
54	28 27 24	126	27 52 25	126	27 17 26	127	26 41 27	127	26 05 28	127	306
55	27 39-24	125	27 04-25	126	26 29-26	126	25 53-26	127	25 17-27	127	305
56	26 50 23	125	26 15 23	125	25 41 25	126	25 05 25	126	24 30 26	126	304
57	26 01 23	125	25 27 24	125	24 52 24	125	24 17 25	126	23 42 25	126	303
58	25 12 22	124	24 38 23	125	24 04 24	125	23 29 24	125	22 54 25	126	302
59	24 22 21	124	23 49 22	124	23 15 23	125	22 41 24	125	22 06 24	125	301
60	23 32-20	124	22 59-21	124	22 26-23	124	21 52-23	125	21 18-24	125	300
61	22 42 19	123	22 10 21	124	21 36 21	124	21 03 23	124	20 29 23	124	299
62	21 52 19	123	21 20 20	123	20 47 21	124	20 14 22	124	19 40 23	124	298
63	21 02 18	123	20 30 20	123	19 57 20	123	19 24 21	124	18 51 22	124	297
64	20 12 18	122	19 40 19	123	19 07 20	123	18 35 21	123	18 02 22	123	296
65	19 21-17	122	18 50-19	122	18 17-19	123	17 45-20	123	17 12-21	123	295
66	18 31 17	122	17 59 18	122	17 27 18	122	16 55 19	123	16 23 21	123	294
67	17 40 16	121	17 09 18	122	16 37 18	122	16 05 19	122	15 33 20	122	293
68	16 49 16	121	16 18 17	121	15 47 18	122	15 15 19	122	14 43 19	122	292
69	15 58 15	121	15 27 16	121	14 56 17	121	14 25 18	122	13 53 19	122	291
70	15 07-15	121	14 36-15	121	14 05-16	121	13 34-17	121	13 03-18	122	290
71	14 16 15	121	13 45 15	121	13 15 16	121	12 44 17	121	12 13 18	121	289
72	13 24 13	120	12 54 14	121	12 24 16	121	11 53 16	121	11 22 17	121	288
73	12 33 13	120	12 03 14	120	11 33 15	121	11 02 15	121	10 32-17	121	287
74	11 42 13	120	11 12 14	120	10 42-15	120	10 12-16	120	...		286
75	10 50-12	120	10 20-13	120	...		...		...		285

In South { For argument H.A. on the left, True Azimuth = $180^\circ + \text{Tabulated Azimuth.}$ } See
 Latitudes { For argument H.A. on the right, True Azimuth = $180^\circ - \text{Tabulated Azimuth.}$ } p. 91.

EXPLANATION

By agreement with the Admiralty, the *Astronomical Navigation Tables* are produced by H.M. Nautical Almanac Office to the general requirements of the Air Ministry.

These tables are designed to give, in a simple and direct manner, the solution of the astronomical spherical triangle that occurs in navigational practice. They have been planned for use with the *Air Almanac* (Air Publication 1602) and are consequently designed primarily to meet the requirements of modern air navigation: their use can however be extended to surface navigation, as in the case of the *Air Almanac*, within the limitations of the precision of the tabulated altitude and azimuth.

The general object of the *Astronomical Navigation Tables* is to facilitate the calculation of the Altitude and Azimuth of an observed heavenly body, as seen from some position close to that of the observer. This information, together with the observed altitude, allows to be plotted on the chart a position line upon which the observer must lie; two such position lines serve in general to determine the position of the observer. The tables have been arranged with special relation to the determination of the altitude and azimuth when an assumed position is adopted such that the latitude and hour angle are both integral degrees; interpolation in this case is consequently restricted to interpolation to the declination of the body observed, and provision has been made for this to be done in a simple manner. The precision of the tabulated data is consistent with that adopted for the *Air Almanac*, namely that the altitudes are given to the nearest minute of arc, and so are correct to within 0'·5; this standard of precision is sufficient for all purposes of air navigation and, in fact, is at present (1938) considerably greater than the precision obtainable in an altitude observed with a bubble sextant. Although these tables have been prepared in conjunction with the *Air Almanac*, they are equally applicable for use with any other almanac from which the Greenwich Hour Angle and Declination of the body observed can be found for the time of observation; it is intended, however, that the two publications should provide, in the most convenient form, all the material for a rapid solution of the navigator's problem, for all practical observations.

The *Astronomical Navigation Tables* consist of main tables and auxiliary tables. The main tables give the Tabulated Altitude, to the nearest minute of arc, and the Tabulated Azimuth, to the nearest degree, with the three arguments:—

Latitude —each integral degree from S.69° to N.69°.

Declination—for 22 selected stars for the epoch 1940 and each integral degree from S.28° to N.28°.

Hour Angle—each integral degree for which the altitude is greater than 10°* and less than 80°.

Thus for every combination of an integral degree of latitude, declination and hour angle in the above ranges, the tables give immediately the quantities required.

* The limit is decreased for declinations appropriate to the Sun (0°–23°) in latitudes above 55°, where the Sun may be at low altitudes for long periods of each day, and in latitudes below 30°, where the Sun rises rapidly, and the azimuth at low altitudes is required for checking compasses.

EXPLANATION

In the case of the separate tabulations for the 22 stars, the values of the declinations used in the tables are those of the stars themselves at the middle of 1940; the declinations of the stars change slowly owing to precession and to other causes, but the effect of these changes can be allowed for by means of a simple correcting term, which although smaller, is catered for in a similar way to the interpolation for the declination of other bodies. The stars have been selected for their brightness and their distribution in the sky, and are the same in both name and number as stars Nos. 1-22 in the *Air Almanac*. The tables for integral degrees of declination are applicable to observations of the Sun, Moon and planets, as well as for all stars with declinations between S.29° and N.29°; a list of 13 such stars is given in the *Air Almanac* (Nos. 23-35). It is only for stars outside these limits of declination, in particular stars Nos. 36-50 in the *Air Almanac*, that these tables are not applicable; some other method of obtaining the altitude and azimuth must then be employed. The 22 stars catered for separately may however be regarded as generally sufficient for all practical purposes of air navigation; with the 13 additional stars to be used in exceptional circumstances, reference to other methods should be unnecessary.

The interpolation of tables with three arguments is both laborious and difficult, and should be avoided wherever possible; no provision has therefore been made for interpolation other than for declination, and the navigator should not interpolate for latitude and hour angle, but should use an assumed position so that this may be avoided. The arrangement of the tables, however, allows for interpolation for latitude and hour angle without, in general, the necessity for the comparison of figures on different pages, and the tables may therefore be interpolated for these arguments for the solution of special problems.

The tabulated altitude includes the effect of atmospheric refraction, and is thus directly comparable with the corrected sextant reading; it is in fact the altitude of the body as would be measured by an observer. The refraction included is based on the mean value of the refraction at a height of 5,000 feet in normal conditions, and it is unlikely that at heights in that neighbourhood the refraction will differ by more than 0'.5 from that used. Table VI on page 222 gives the adjustment necessary at heights that differ materially from the basic height adopted; the values in this table should only be applied in extreme cases, and where great accuracy is necessary.

The tabulated azimuth is measured from the elevated pole either to the east or to the west. This can be converted to true azimuth, measured always from the north through east, either by the rules given at the foot of each page, or by the use of Table III on pages 90 and 91.

For the greater convenience of the user, the tables are issued in fourteen volumes, each of which caters for a belt of latitude, 5° in width, in both the northern and southern hemispheres. In each volume tabulations are given for five integral degrees of latitude; working from an assumed position, whose latitude is taken to be the nearest integral degree to that of the D.R. (or estimated) position of the observer, each tabular latitude suffices to cover observations from positions within 0° 30' of the integral degree used. The Explanation and auxiliary tables are reprinted in each volume.

Each volume consists of two main parts, pages 2-89 giving the tabulations for the selected 22 stars and pages 94-209 those for declinations 0°-28°. Each part is

EXPLANATION

divided into sections of four pages, covering one star or one whole degree of declination; separate indexes on the margin enable immediate reference to be made to the first opening of each section. Throughout, the arrangement of the tabulations in each section is generally the same; the five values of latitude (LAT.) are given across the page and the values of the hour angle (H.A.) down the page. For the stars, the tabulations for NORTH latitudes precede those for SOUTH latitudes, and for the integral degrees of declination, those for the SAME name as the latitude precede those for CONTRARY name. The amount of tabulation varies in each case with different stars and declinations, and in some cases there are no tabulations either in north or in south latitudes, as the star or a body of the given declination does not reach an altitude which makes it suitable for observation in those latitudes; occasionally it has been necessary to continue the tabulation from one page on to the previous page, and for one or two stars, in south latitudes, on to two pages before.

For the stars, each column refers to a given latitude, and contains for all applicable values of the hour angle, the altitude (Alt.), its variation with time (t) and the azimuth (Az.). For the degrees of declination, the variation t is replaced by the difference (d) between the altitude given and that for the following degree. The procedure of entering and interpolating the tables is not appreciably different in the two cases.

An assumed position is taken close to the D.R. position so that the latitude is an integral degree, while the longitude is chosen so that the hour angle, formed by the combination of longitude (*added if east, subtracted if west*) with the G.H.A., taken from the *Air Almanac*, is also an integral degree. The appropriate part (star or degree of declination) is chosen, and the correct section obtained by the marginal index, using the star number, or the integral degree numerically *less* than the declination of the observed body as found from the *Air Almanac*. In this section, the column is chosen corresponding to the assumed latitude, care being taken to select the correct hemisphere. In this column, the values of Alt., t , and Az. can be read off for the stars, corresponding to the particular integral hour angle; for a degree of declination, the values of Alt., d and Az. are similarly found.

The tabulated altitude must now be corrected, in the case of the 22 stars, for the effect of precession, and for other bodies, interpolated to the true declination. Table I on the inside front cover gives the correction to be applied to the altitude of the stars for all years to 2000 for values of t ; this correction must be added or subtracted according to the sign prefixed to t . For each star a limiting year is given before which this correction cannot exceed 1', and there is therefore no need to apply it until after that date. Similarly, the inside back cover and its facing page contain Table XV, with arguments d and the minutes of the declination of the body, giving the correction to be applied to the tabulated altitude taken out for an integral degree; this correction is to be applied to the tabulated altitude with the same sign as that of d .

It is unnecessary to correct the tabulated azimuth in any way, but it must of course be converted to true azimuth before being used to plot a position line.

Having thus obtained the corrected tabulated altitude and the true azimuth, the position line is drawn in the usual manner. The intercept is obtained from the difference between the corrected sextant reading and the corrected tabulated altitude, and is set off from the assumed position either *towards* the direction given

EXPLANATION

by the true azimuth or in the opposite direction (*away* from), according to the following rules:

Corr. Tab. Alt. *less* than Corr. Sext. Rdg., intercept *towards*;

Corr. Tab. Alt. *greater* than Corr. Sext. Rdg., intercept *away*.

The position line is then drawn at right angles to the intercept through the point so obtained. The expression corrected sextant reading is used conveniently for the observed altitude to emphasize that this quantity is the altitude as measured by the sextant, corrected only for sextant errors and for dome refraction if applicable. As the atmospheric refraction is catered for in the tabulated altitude, no correction for this should be applied to the sextant reading.

If the assumed position is close to the true position, a slight inaccuracy in plotting the tabulated azimuth is unimportant; when the tabulated azimuth is near 0° or 180° advantage may be taken of this to draw the position line simply as part of a parallel of latitude. A double border rule, given when the azimuth is within a few degrees of the meridian, indicates the portions of the tables where this can be done without great error; the limit of azimuth has been varied slightly in different volumes, according to the latitude, so as to reduce the error due to this simplified procedure. The accuracy of this method depends upon the error in the assumed longitude; for an error of 20 miles in the D.R. longitude, the maximum error introduced into the deduced latitude is about 2 miles, while the remaining error (due to the use of an assumed position) may reach a maximum of 2 miles in the worst case. This method should therefore only be adopted either when errors up to about 4 miles can be tolerated, or when the D.R. longitude is known to be fairly accurate; if the D.R. position is liable to much greater error than 20 miles, this method should not be used. An assumed position is taken and the tables entered in exactly the same way (whether for stars or other bodies) as for an ordinary observation, but there is now no necessity to take out the azimuth or to convert to true azimuth. The tabulated altitude is corrected by Table I or Table XV as necessary, and the intercept formed by the usual rules. The intercept is then set off from the assumed position *towards* or *away* from the direction of the object observed, this direction being taken as true north or true south; the position line is thus drawn in as a parallel of latitude. Although the procedure of entering the tables is exactly the same, this method saves a considerable amount of work in the plotting of the position line.

A list of the auxiliary tables is given in the list of contents; in general the titles of these tables are self-explanatory and their use either self-evident or explained on the page concerned.

Tables VII, VIII, IX, X, XI and XIII are arranged as critical tables, so that the result is obtained immediately without interpolation. The argument is divided into intervals, successive intervals corresponding to successive values of the result; for any values of the argument, inside one of these intervals, the corresponding result is the quantity opposite that interval and has in general a maximum error of less than half a unit in the last figure given; when successive values of the result are not consecutive integers, this error can rise to half the difference between successive values. The tabulated values of the argument correspond to half-way values of the result, and these are always chosen so that when the argument is exactly equal to one of the tabulated values, the nearest value of the result is the one corresponding to the previous interval. Thus the rule to be followed is:

When the argument is an exact tabulated value, the *upper* of the two possible values of the result should be taken.

ILLUSTRATIONS

Example 1.—On 1941 September 30, local date, about two hours after sunset, in dead reckoning position latitude $8^{\circ} 17' N.$, longitude $125^{\circ} 30' W.$, star number 22 (Vega) was observed to obtain a position line. Corrected sextant reading $48^{\circ} 42'$; G.M.T. of observation $04^h 18^m 14^s$.

From Table IV, page 92 :

Long. $120^{\circ} W.$ (approx.)		
Approx.	Hrs.	Date
L.M.T.	2000	Sept. 30
G.M.T.	0400	Oct. 1

From page 86 :

Lat. of ass. position $8^{\circ} NORTH$

Tab. Alt.	.	.	$49^{\circ} 08'$
Correction.	.	.	—
Corr. Tab. Alt.	.	.	$49^{\circ} 08'$
Corr. Sext. Rdg.	.	.	$48^{\circ} 42'$
Intercept	.	.	$26'$ away

From *Air Almanac*, 1941 Oct. 1 :

G.H.A. γ	($04^h 10^m$)	.	$72^{\circ} 00'$
Increment	($8^m 14^s$)	.	$2^{\circ} 04'$
S.H.A.	(No. 22)	.	$81^{\circ} 16'$
G.H.A. of star	.	.	$155^{\circ} 20'$
Long. of ass. position	.	.	$-125^{\circ} 20'$

Star No. 22

H.A. 30°

No correction for
date is necessary
in 1941.

Tab. Az. 37°

Assumed position :

Lat. $8^{\circ} N.$

Long. $125^{\circ} 20' W.$

From Table III,

page 90 :

True Az. $323^{\circ} T.$

Example 2.—On 1950 August 17, Greenwich date, in dead reckoning position latitude $5^{\circ} 52' S.$, longitude $26^{\circ} 29' E.$, star number 4 (Alpheratz) was observed to obtain a position line. From the *Almanac* of that date it was found that the G.H.A. of the star corresponding to the G.M.T. of observation was $355^{\circ} 14'$. Corrected sextant reading $49^{\circ} 26'$.

G.H.A. of star	.	.	$355^{\circ} 14'$
Long. of ass. position	.	.	$+26^{\circ} 46'$
			$382^{\circ} 00'$
			-360

From page 16 :

Lat. of ass. position $6^{\circ} SOUTH$

Tab. Alt.	.	.	$49^{\circ} 18'$
Correction (Table I)	.	.	-3
Corr. Tab. Alt.	.	.	$49^{\circ} 15'$
Corr. Sext. Rdg.	.	.	$49^{\circ} 26'$
Intercept	.	.	$11'$ towards

Star No. 4

H.A. 22°

ι . . . -16

Tab. Az. 150°

Year . . . 1950

Assumed position :

Lat. $6^{\circ} S.$

Long. $26^{\circ} 46' E.$

From Table III,

page 91 :

True Az. $330^{\circ} T.$

ILLUSTRATIONS

Example 3.—On 1941 October 1, local date, at approximate local noon, in dead reckoning position latitude $8^{\circ} 40' N.$, longitude $21^{\circ} 07' W.$, the Sun was observed to obtain a position line. Corrected sextant reading $78^{\circ} 05'$; G.M.T. of observation $13^h 11^m 27^s$.

From Table IV, page 92 :

Long. $15^{\circ} W.$ (approx.)		
Approx.	Hrs.	Date
L.M.T.	1200	Oct. 1
G.M.T.	1300	Oct. 1

From *Air Almanac*, 1941 Oct. 1 :

G.H.A.	($13^h 10^m$)	.	$20^{\circ} 04'$
Increment	($1^m 27^s$)	.	0 22
G.H.A. of Sun		.	20 26
Long. of ass. position		.	- 21 26
			- 1 00
			+360

From page 108 :

Lat. of ass. position $9^{\circ} N.$ Dec. $3^{\circ} 10' S.$ CONTRARY name H.A. 359°

Tab. Alt.	$77^{\circ} 58'$	<i>d</i>	-60	Tab. Az. 175°
Correction (Table XV) -	10	Minutes of dec. 10		

Corr. Tab. Alt.	$77^{\circ} 48'$	Assumed position :	From Table III,
Corr. Sext. Rdg.	$78^{\circ} 05'$	Lat. $9^{\circ} N.$	page 90 :
Intercept	$17'$ towards	Long. $21^{\circ} 26' W.$	True Az. $175^{\circ} T.$

Since there is a double border rule opposite the entry on page 108, this observation may be reduced by the method described on page 213. In this case the intercept is set off from the assumed position *towards* the Sun (i.e. southwards), and the position line drawn as a parallel of latitude. There is then no necessity to take out the tabulated azimuth.

Example 4.—On 1941 October 2, local date, about one hour before sunrise, in dead reckoning position latitude $4^{\circ} 38' S.$, longitude $147^{\circ} 58' E.$, star number 35 (Wezen) was observed to obtain a position line. Corrected sextant reading $58^{\circ} 27'$; G.M.T. of observation $18^h 58^m 19^s$.

From Table IV, page 93 :

Long. $150^{\circ} E.$ (approx.)		
Approx.	Hrs.	Date
L.M.T.	0500	Oct. 2
G.M.T.	1900	Oct. 1

From *Air Almanac*, 1941 Oct. 1 :

G.H.A. γ	($18^h 50^m$)	.	$292^{\circ} 36'$
Increment	($8^m 19^s$)	.	2 05
S.H.A.	(No. 35)	.	253 29
G.H.A. of star		.	548 10
Long. of ass. position		.	+147 50
			696 00
			-360

From page 198 :

Lat. of ass. position $5^{\circ} S.$ Dec. $26^{\circ} 18' S.$ SAME name H.A. 336°

Tab. Alt.	$58^{\circ} 54'$	<i>d</i>	-38	Tab. Az. 45°
Correction (Table XV) -	11	Minutes of dec. 18		

Corr. Tab. Alt.	$58^{\circ} 43'$	Assumed position :	From Table III,
Corr. Sext. Rdg.	$58^{\circ} 27'$	Lat. $5^{\circ} S.$	page 91 :
Intercept	$16'$ away	Long. $147^{\circ} 50' E.$	True Az. $135^{\circ} T.$

IVa.—CHANGE OF SEXTANT READING WITH TIME

Due to motion of
body observed

Due to motion of observer

True Azi- muth of body	Latitude			True Azi- muth of body
	5°	7°	9°	
090	+45	+45	+44	090
095	45	44	44	085
100	44	44	44	080
105	43	43	43	075
110	42	42	42	070
115	41	40	40	065
120	+39	+39	+38	060
125	37	37	36	055
130	34	34	34	050
135	32	32	31	045
140	29	29	29	040
145	26	26	25	035
150	+22	+22	+22	030
155	19	19	19	025
160	15	15	15	020
165	12	12	12	015
170	8	8	8	010
175	+4	+4	+4	005
180	0	0	0	000
185	-4	-4	-4	355
190	8	8	8	350
195	12	12	12	345
200	15	15	15	340
205	19	19	19	335
210	-22	-22	-22	330
215	26	26	25	325
220	29	29	29	320
225	32	32	31	315
230	34	34	34	310
235	37	37	36	305
240	-39	-39	-38	300
245	41	40	40	295
250	42	42	42	290
255	43	43	43	285
260	44	44	44	280
265	45	44	44	275
270	-45	-45	-44	270

Difference between True Az. of body and Track	Ground speed in m.p.h.									Difference between True Az. of body and Track
	100	130	160	190	220	250	280	310	340	
000	+4	+6	+7	+8	+10	+11	+12	+13	+15	360
005	4	6	7	8	10	11	12	13	15	355
010	4	6	7	8	9	11	12	13	15	350
015	4	5	7	8	9	10	12	13	14	345
020	4	5	7	8	9	10	11	13	14	340
025	4	5	6	7	9	10	11	12	13	335
030	+4	+5	+6	+7	+8	+9	+11	+12	+13	330
035	4	5	6	7	8	9	10	11	12	325
040	3	4	5	6	7	8	9	10	11	320
045	3	4	5	6	7	8	9	10	10	315
050	3	4	4	5	6	7	8	9	9	310
055	2	3	4	5	5	6	7	8	8	305
060	+2	+3	+3	+4	+5	+5	+6	+7	+7	300
065	2	2	3	3	4	5	5	6	6	295
070	1	2	2	3	3	4	4	5	5	290
075	1	1	2	2	2	3	3	3	4	285
080	+1	+1	1	1	2	2	2	2	3	280
085	0	0	+1	+1	+1	+1	+1	+1	+1	275
090	0	0	0	0	0	0	0	0	0	270
095	0	0	-1	-1	-1	-1	-1	-1	-1	265
100	-1	-1	1	1	2	2	2	2	3	260
105	1	1	2	2	2	3	3	3	4	255
110	1	2	2	3	3	4	4	5	5	250
115	2	2	3	3	4	5	5	6	6	245
120	-2	-3	-3	-4	-5	-5	-6	-7	-7	240
125	2	3	4	5	5	6	7	8	8	235
130	3	4	4	5	6	7	8	9	9	230
135	3	4	5	6	7	8	9	10	10	225
140	3	4	5	6	7	8	9	10	11	220
145	4	5	6	7	8	9	10	11	12	215
150	-4	-5	-6	-7	-8	-9	-11	-12	-13	210
155	4	5	6	7	9	10	11	12	13	205
160	4	5	7	8	9	10	11	13	14	200
165	4	5	7	8	9	10	12	13	14	195
170	4	6	7	8	9	11	12	13	15	190
175	4	6	7	8	10	11	12	13	15	185
180	-4	-6	-7	-8	-10	-11	-12	-13	-15	180

The theoretical change of sextant reading in any interval of time depends partly on the motion of the body observed across the sky and partly on the motion of the observer over the Earth's surface.

The two tables above give this change, in an interval of three minutes of time, due to each of these causes; a + sign denotes that the sextant reading is increasing, and a - sign that it is decreasing. The theoretical change of sextant reading in three minutes of time is obtained by combining the appropriate entries from each table.

IVb.—CHANGE OF SEXTANT READING WITH TIME

Interval of time	Change in 3 ^m (from Table IVa)								Interval of time
	0' 3' 6'	9' 12' 15'	18' 21' 24'	27' 30' 33'	36' 39' 42'	45' 48' 51'	54' 57' 60'		
0 00	0 0 0	0 0 0	0 0 0	0 0 0	0 0 0	0 0 0	0 0 0	0 00	
05	0 0 0	0 0 0	0 1 1	1 1 1	1 1 1	1 1 1	2 2 2	05	
10	0 0 0	0 1 1	1 1 1	2 2 2	2 2 2	2 3 3	3 3 3	10	
15	0 0 0	1 1 1	2 2 2	2 2 3	3 3 4	4 4 4	4 5 5	15	
20	0 0 1	1 1 2	2 2 3	3 3 4	4 4 5	5 5 6	6 6 7	20	
25	0 0 1	1 2 2	2 3 3	4 4 5	5 5 6	6 7 7	8 8 8	25	
0 30	0 0 1	2 2 2	3 4 4	4 5 6	6 6 7	8 8 8	9 10 10	0 30	
35	0 1 1	2 2 3	4 4 5	5 6 6	7 8 8	9 9 10	10 11 12	35	
40	0 1 1	2 3 3	4 5 5	6 7 7	8 9 9	10 11 11	12 13 13	40	
45	0 1 2	2 3 4	4 5 6	7 8 8	9 10 10	11 12 13	14 14 15	45	
50	0 1 2	2 3 4	5 6 7	8 8 9	10 11 12	12 13 14	15 16 17	50	
0 55	0 1 2	3 4 5	6 6 7	8 9 10	11 12 13	14 15 16	16 17 18	0 55	
1 00	0 1 2	3 4 5	6 7 8	9 10 11	12 13 14	15 16 17	18 19 20	1 00	
05	0 1 2	3 4 5	6 8 9	10 11 12	13 14 15	16 17 18	20 21 22	05	
10	0 1 2	4 5 6	7 8 9	10 12 13	14 15 16	18 19 20	21 22 23	10	
15	0 1 2	4 5 6	8 9 10	11 12 14	15 16 18	19 20 21	22 24 25	15	
20	0 1 3	4 5 7	8 9 11	12 13 15	16 17 19	20 21 23	24 25 27	20	
25	0 1 3	4 6 7	8 10 11	13 14 16	17 18 20	21 23 24	26 27 28	25	
1 30	0 2 3	4 6 8	9 10 12	14 15 16	18 20 21	22 24 26	27 28 30	1 30	
35	0 2 3	5 6 8	10 11 13	14 16 17	19 21 22	24 25 27	28 30 32	35	
40	0 2 3	5 7 8	10 12 13	15 17 18	20 22 23	25 27 28	30 32 33	40	
45	0 2 4	5 7 9	10 12 14	16 18 19	21 23 24	26 28 30	32 33 35	45	
50	0 2 4	6 7 9	11 13 15	16 18 20	22 24 26	28 29 31	33 35 37	50	
1 55	0 2 4	6 8 10	12 13 15	17 19 21	23 25 27	29 31 33	34 36 38	1 55	
2 00	0 2 4	6 8 10	12 14 16	18 20 22	24 26 28	30 32 34	36 38 40	2 00	
05	0 2 4	6 8 10	12 15 17	19 21 23	25 27 29	31 33 35	38 40 42	05	
10	0 2 4	6 9 11	13 15 17	20 22 24	26 28 30	32 35 37	39 41 43	10	
15	0 2 4	7 9 11	14 16 18	20 22 25	27 29 32	34 36 38	40 43 45	15	
20	0 2 5	7 9 12	14 16 19	21 23 26	28 30 33	35 37 40	42 44 47	20	
25	0 2 5	7 10 12	14 17 19	22 24 27	29 31 34	36 39 41	44 46 48	25	
2 30	0 2 5	8 10 12	15 18 20	22 25 28	30 32 35	38 40 42	45 48 50	2 30	
35	0 3 5	8 10 13	16 18 21	23 26 28	31 34 36	39 41 44	46 49 52	35	
40	0 3 5	8 11 13	16 19 21	24 27 29	32 35 37	40 43 45	48 51 53	40	
45	0 3 6	8 11 14	16 19 22	25 28 30	33 36 38	41 44 47	50 52 55	45	
50	0 3 6	8 11 14	17 20 23	26 28 31	34 37 40	42 45 48	51 54 57	50	
2 55	0 3 6	9 12 15	18 20 23	26 29 32	35 38 41	44 47 50	52 55 58	2 55	
3 00	0 3 6	9 12 15	18 21 24	27 30 33	36 39 42	45 48 51	54 57 60	3 00	

This table gives the theoretical change of sextant reading in any interval of time up to 3^m, in terms of the change in 3^m obtained from the tables on the opposite page. If the interval is greater than 3^m, it may be split into multiples of 3^m and a residue, and the corresponding entries from the table added together.

A knowledge of this change enables sights on different objects taken at slightly different times to be adjusted to a specified exact time, which may be either the exact time of one of them or a moment when a fix is required for a particular reason.

N. 5°-9°

V.—DIFFERENCE BETWEEN RHUMB LINE AND GREAT CIRCLE DISTANCES

S. 5°-9°

Latitude of Destination	Change of Longitude																		Latitude of Destination
	5°	10°	15°	20°	25°	30°	35°	40°	45°	50°	55°	60°	65°	70°	75°	80°	85°	90°	
N. 60°	0	1	3	6	9	14	20	27	35	46	58	72	88	108	130	155	184	217	S. 60°
55	0	1	3	5	8	11	16	22	29	38	48	60	75	91	111	134	160	190	55
50	0	1	2	4	6	9	13	17	23	31	39	50	62	77	94	114	137	163	50
45	0	1	1	3	4	7	10	14	19	25	32	41	51	63	78	95	115	138	45
40	0	0	1	2	3	5	8	11	14	19	25	32	41	51	64	78	95	114	40
N. 35	0	0	1	1	2	4	6	8	11	15	20	25	32	41	51	62	76	92	S. 35
30	0	0	0	1	2	3	4	6	8	11	15	19	25	31	39	49	60	72	30
25	0	0	0	1	1	2	3	4	6	8	11	14	19	23	29	37	45	55	25
20	0	0	0	0	1	1	2	3	4	6	8	10	13	17	21	26	32	39	20
15	0	0	0	0	0	1	1	2	3	4	5	7	9	11	14	17	21	26	15
N. 10	0	0	0	0	0	0	1	1	2	2	3	4	5	7	8	10	13	16	S. 10
N. 5	0	0	0	0	0	0	0	0	1	1	1	2	3	3	4	5	6	8	S. 5
0	0	0	0	0	0	0	0	0	0	0	1	1	1	1	2	2	2	3	0
S. 5	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	1	1	N. 5
10	0	0	0	0	0	0	0	0	0	0	0	0	0	1	1	1	1	1	10
S. 15	0	0	0	0	0	0	0	0	1	1	1	1	2	2	3	4	4	5	N. 15
20	0	0	0	0	0	0	1	1	1	2	3	3	4	5	7	8	10	12	20
25	0	0	0	0	1	1	1	2	3	4	5	6	8	10	12	15	19	22	25
30	0	0	0	1	1	2	2	3	5	6	8	10	13	16	20	24	30	36	30
35	0	0	1	1	2	3	4	5	7	9	12	15	19	24	30	36	44	53	35
S. 40	0	0	1	2	3	4	5	8	10	13	17	22	27	34	42	51	61	74	N. 40
45	0	1	1	2	4	5	8	11	14	18	24	30	37	46	56	68	81	97	45
50	0	1	2	3	5	7	11	14	19	25	31	39	49	60	72	87	104	124	50
55	0	1	2	4	7	10	14	19	25	32	40	50	62	76	91	109	130	154	55
S. 60	0	1	3	5	9	13	18	24	32	41	51	63	77	94	112	134	159	187	N. 60

This table gives the difference, in nautical miles, between the distance from one place to another by the Rhumb Line track and the distance by the Great Circle track. It is based on a *Latitude of Departure* of 7°, but may be used for any place of departure between latitudes 5° and 9°. Of the two argument columns headed *Latitude of Destination*, the one on the left is to be used when the place of departure lies between N. 5° and N. 9°, and the one on the right when the place of departure lies between S. 5° and S. 9°.

The table is intended to give only the approximate difference of distance between the two tracks. For intermediate values of the arguments *Latitude of Destination* and *Change of Longitude*, the figures in the table should be interpolated by inspection. If the *Latitude of Departure* differs by the maximum of 2½° from that on which the table is based, the error in the result will not exceed 2 miles up to a *Change of Longitude* of 50°, but may reach 4 miles for a change of 70°, and 8 miles for a change of 90°.

Example.—Required the difference in distance between the Rhumb Line track and the Great Circle track from Colombo (Lat. 6° 55' N., Long. 79° 55' E.) to Newcastle-on-Tyne (Lat. 55° 00' N., Long. 1° 35' W.).

Entering the argument column on the left with the *Latitude of Destination* of 55° 00' N., and interpolating by inspection for the *Change of Longitude* of 81° 30', it will be seen that the difference in distance is about 142 nautical miles.

VI.—ADJUSTMENT TO REFRACTION IN SPECIAL CONDITIONS

Height in feet	Observed Altitude									Height in metres
	4°	6°	8°	10°	15°	20°	30°	45°	60°	
0	-2	-1	-1	-1	0	0	0	0	0	0
5000	0	0	0	0	0	0	0	0	0	1500
10000	+1	+1	+1	+1	0	0	0	0	0	3000
15000	2	2	2	1	+1	+1	0	0	0	4600
20000	3	2	2	2	1	1	+1	0	0	6100
25000	4	3	2	2	1	1	1	0	0	7600
30000	4	3	3	3	2	1	1	0	0	9100
35000	5	4	3	3	2	1	1	+1	0	10700
40000	+5	+4	+3	+3	+2	+2	+1	+1	0	12200

This table gives the additional correction for refraction to be applied to the *observed* altitude beyond that already included in the altitude tabulated in the main tables. It is only intended for use by an observer at great heights, and when special accuracy is required.

VII.—TRUE AZIMUTH OF THE POLE STAR

1940-1960		1960-1980		1980-2000	
L.H.A. °	True Azi- muth	L.H.A. °	True Azi- muth	L.H.A. °	True Azi- muth
0	0	0	0	0	0
57	000	65	000	74	000
176	359	176	359	175	359
237	000	245	000	254	000
356	001	356	001	355	001
360	000	360	000	360	000

These tables give the True Azimuth of the Pole Star, over various periods of time, for an observer between latitudes N. 5° and N. 9°. The argument L.H.A.° is obtained from G.H.A.° by *subtracting west* longitude or *adding east* longitude.

VIII.—DIP OF THE SEA HORIZON

Height in feet	Dip	Height in metres	Height in feet	Dip	Height in metres	Height in feet	Dip	Height in metres	Height in feet	Dip	Height in metres	Height in feet	Dip	Height in metres
0	'	0	437	21	133	1700	41	520	3810	61	1160	6740	81	2050
2	1		481	22	146	1790	42	546	3930	62	1200	6910	82	2100
6		1	527	23	160	1880	43	573	4060	63	1230	7080	83	2160
12	3		575	24	175	1970	44	600	4190	64	1270	7250	84	2210
21	4	6	625	25	190	2060	45	628	4330	65	1320	7430	85	2260
31	5	9	677	26	206	2150	46	657	4460	66	1360	7610	86	2320
43	6	13	731	27	222	2250	47	686	4600	67	1400	7790	87	2370
58	7	17	787	28	240	2340	48	716	4740	68	1440	7970	88	2420
75	8	22	845	29	257	2440	49	746	4880	69	1480	8150	89	2480
93	9	28	906	30	276	2550	50	777	5020	70	1530	8340	90	2540
114	10	34	968	31	295	2650	51	809	5170	71	1570	8520	91	2590
137	11	41	1030	32	314	2760	52	841	5320	72	1620	8710	92	2650
162	12	49	1090	33	335	2860	53	874	5470	73	1660	8900	93	2710
189	13	57	1160	34	356	2980	54	908	5620	74	1710	9100	94	2770
218	14	66	1230	35	377	3090	55	942	5770	75	1760	9290	95	2830
250	15	76	1310	36	399	3200	56	977	5930	76	1800	9490	96	2890
283	16	86	1380	37	422	3320	57	1010	6090	77	1850	9690	97	2950
318	17	97	1460	38	446	3440	58	1040	6250	78	1900	9890	98	3010
356	18	108	1540	39	470	3560	59	1080	6410	79	1950	10100	99	3070
395	19	120	1620	40	495	3680	60	1120	6580	80	2000	10300	100	3140
437	20	133	1700		520	3810		1160	6740		2050	10500		3200

This table gives the dip of the sea horizon, in minutes of arc, with argument height of eye of the observer in feet or in metres. It is only required when the altitude is measured from the sea horizon. The dip is to be *subtracted* from the observed altitude.

IX.—DISTANCE TO THE SEA HORIZON IN NAUTICAL MILES

Height in feet	Dist.	Height in metres	Height in feet	Dist.	Height in metres	Height in feet	Dist.	Height in metres	Height in feet	Dist.	Height in metres	Height in feet	Dist.	Height in metres	Height in feet	Dist.	Height in metres
0	1	0	287	20	87	1120	39	341	2500	58	762	4420	77	1340	6890	96	2100
1	2	1	317	21	96	1170	40	359	2580	59	788	4540	78	1380	7040	97	2140
4	3	2	349	22	106	1240	41	378	2670	60	815	4650	79	1420	7180	98	2190
9	4	4	382	23	116	1300	42	396	2760	61	843	4770	80	1450	7330	99	2230
15	5	6	417	24	127	1360	43	416	2850	62	871	4900	81	1490	7480	100	2280
22	6	9	453	25	138	1430	44	436	2950	63	900	5020	82	1530	7630	101	2320
31	7	12	491	26	149	1490	45	456	3040	64	929	5140	83	1560	7780	102	2370
42	8	16	531	27	161	1560	46	477	3140	65	958	5270	84	1600	7940	103	2420
54	9	20	571	28	174	1630	47	498	3240	66	988	5390	85	1640	8100	104	2460
68	10	25	614	29	187	1700	48	520	3340	67	1010	5520	86	1680	8250	105	2510
83	11	30	658	30	200	1770	49	542	3440	68	1050	5650	87	1720	8410	106	2560
100	12	36	703	31	214	1850	50	564	3540	69	1080	5780	88	1760	8570	107	2610
118	13	42	750	32	228	1920	51	587	3650	70	1110	5920	89	1800	8730	108	2660
137	14	48	798	33	243	2000	52	611	3750	71	1140	6050	90	1840	8900	109	2710
158	15	55	848	34	258	2080	53	635	3860	72	1170	6190	91	1880	9060	110	2760
181	16	62	900	35	274	2160	54	659	3970	73	1210	6330	92	1920	9230	111	2810
205	17	70	953	36	290	2240	55	684	4080	74	1240	6460	93	1970	9400	112	2860
231	18	78	1000	37	307	2320	56	709	4190	75	1270	6610	94	2010	9560	113	2910
258	19	87	1060	38	324	2410	57	735	4310	76	1310	6750	95	2050	9740	114	2960
287			1120		341	2500		762	4420		1340	6890		2100	9910		3020

IX.—DISTANCE TO THE SEA HORIZON IN STATUTE MILES

Height in feet	Dist.	Height in metres	Height in feet	Dist.	Height in metres	Height in feet	Dist.	Height in metres	Height in feet	Dist.	Height in metres	Height in feet	Dist.	Height in metres	Height in feet	Dist.	Height in metres
0	1	0	288	23	87	1120	45	344	2520	67	768	4460	89	1360	6960	111	2120
1	2	1	314	24	95	1180	46	359	2590	68	791	4560	90	1390	7080	112	2160
3	3	2	342	25	104	1230	47	375	2670	69	815	4670	91	1420	7210	113	2190
6	4	3	370	26	113	1280	48	392	2750	70	839	4770	92	1450	7340	114	2230
11	5	5	400	27	122	1340	49	408	2830	71	863	4870	93	1480	7470	115	2270
17	6	7	431	28	131	1390	50	425	2910	72	888	4980	94	1510	7600	116	2310
24	7	9	463	29	141	1450	51	443	2990	73	913	5090	95	1550	7730	117	2350
32	8	12	496	30	151	1510	52	460	3080	74	938	5200	96	1580	7870	118	2390
41	9	15	530	31	161	1570	53	479	3160	75	964	5310	97	1610	8000	119	2440
51	10	19	565	32	172	1630	54	497	3250	76	990	5420	98	1650	8140	120	2480
62	11	22	602	33	183	1690	55	516	3330	77	1010	5530	99	1680	8280	121	2520
75	12	27	639	34	195	1750	56	535	3420	78	1040	5640	100	1720	8410	122	2560
89	13	31	678	35	206	1820	57	554	3510	79	1070	5750	101	1750	8550	123	2600
103	14	36	718	36	219	1880	58	574	3600	80	1090	5870	102	1790	8690	124	2650
119	15	41	759	37	231	1950	59	594	3690	81	1120	5990	103	1820	8830	125	2690
137	16	47	801	38	244	2010	60	615	3780	82	1150	6100	104	1860	8980	126	2730
155	17	53	845	39	257	2080	61	636	3880	83	1180	6220	105	1890	9120	127	2780
174	18	59	889	40	271	2150	62	657	3970	84	1210	6340	106	1930	9270	128	2820
195	19	66	935	41	285	2220	63	678	4070	85	1240	6460	107	1970	9410	129	2870
216	20	73	982	42	299	2290	64	700	4160	86	1270	6580	108	2000	9560	130	2910
239	21	80	1030	43	313	2370	65	723	4260	87	1300	6710	109	2040	9710	131	2960
263	22	87	1070	44	328	2440	66	745	4360	88	1330	6830	110	2080	9860	132	3000
288			1120		344	2520		768	4460		1360	6960		2120	10000		3050

These tables give the distance to the sea horizon, in nautical miles and in statute miles, with argument height of eye of the observer in feet or in metres.

At the moment when an object of known height is just appearing or disappearing over the sea horizon, its distance may be found by adding the distance corresponding to its height to the distance corresponding to the height of eye of the observer.

X.—TABLE OF RANGES IN NAUTICAL MILES

The tables below and on the opposite page give the distance, to the nearest 5 nautical miles, of an object, whose height is known and is *greater* than the height of the observer. The arguments of the table are the observed *angle of elevation* to the object, and the *difference in height* between the object and the observer, expressed in feet or in metres.

Example.—An observer, whose height is 1,500 feet, finds that the angle of elevation to the summit of a mountain, whose height is known to be 7,000 feet, is $0^{\circ} 48'$. Required the distance away of the mountain.

The difference in height between the mountain and the observer is $7,000 - 1,500 = 5,500$ feet. Entering on the opposite page the column headed $0^{\circ} 50'$ (the nearest tabulated value to $0^{\circ} 48'$), and choosing the left-hand of the two argument columns since the height is measured in feet, it is seen that 5,500 lies in the interval between 5,130 and 5,910, so that the distance of the mountain, to the nearest 5 miles, is 45 nautical miles.

The tables on pages 226 to 228 give the distance of an object, whose height is known, and is *less* than the height of the observer. The arguments of the table are the observed *angle of depression* to the object, and the *difference in height* between the observer and the object, expressed in feet or in metres. The distance is given to the nearest mile up to 10 nautical miles, and to the nearest 5 miles from 10 to 60 nautical miles.

Example.—An observer, whose height is 1,500 metres, finds that the angle of depression to a ship is $5^{\circ} 37'$. Required the distance away of the ship.

Entering on page 228 the column headed $5^{\circ} 30'$, and choosing the right-hand of the two argument columns, it is seen that 1,500 is an exact tabulated value, so that the distance away of the ship is 8 nautical miles.

On page 226, figures in *italics* represent the difference in height, *when the object observed is beyond the sea horizon*. If it is uncertain whether the object is beyond the horizon or not, and the two parts of the table give widely different results, there should be no doubt which is the correct one, while in doubtful cases the error will not be serious.

These tables are intended to give only the approximate range. They should prove a more reliable guide for large angles of elevation and depression than for small ones.

Height of object *greater* than height of observer

Angle of elevation																	
$4^{\circ} 00'$			$3^{\circ} 40'$			$3^{\circ} 20'$			$3^{\circ} 00'$			$2^{\circ} 40'$			$2^{\circ} 20'$		
Height in feet	Range	Height in metres	Height in feet	Range	Height in metres	Height in feet	Range	Height in metres	Height in feet	Range	Height in metres	Height in feet	Range	Height in metres	Height in feet	Range	Height in metres
0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
1060	0	325	978	0	298	890	0	271	801	0	244	712	0	217	624	0	190
3230	5	985	2960	5	904	2690	5	822	2430	5	741	2160	5	660	1900	5	579
5430	10	1650	4990	10	1520	4540	10	1380	4100	10	1250	3650	10	1110	3210	10	980
7670	15	2330	7050	15	2140	6430	15	1960	5810	15	1770	5190	15	1580	4570	15	1390
9950	20	3030	9150	20	2790	8350	20	2540	7550	20	2300	6750	20	2050	5960	20	1810
12200	25	3740	11200	25	3440	10300	25	3140	9340	25	2840	8360	25	2540	7390	25	2250
14600	30	4450	13400	30	4100	12300	30	3750	11100	30	3400	10000	30	3050	8850	30	2690
17000	35	5180	15600	35	4780	14300	35	4370	13000	35	3960	11600	35	3560	10300	35	3150
19400	40	5920	17900	40	5460	16400	40	5000	14900	40	4540	13400	40	4080	11900	40	3620
21900	45	6680	20200	45	6160	18500	45	5650	16800	45	5130	15100	45	4620	13400	45	4110
24400	50	7440	22500	50	6870	20600	50	6300	18800	50	5730	16900	50	5170	15100	50	4600
26900	55	8210	24900	55	7590	22800	55	6970	20800	55	6350	18800	55	5730	16700	55	5100
29500	60	9000	27300	60	8320	25100	60	7650	22800	60	6970	20600	60	6300	18400	60	5620

X.—TABLE OF RANGES IN NAUTICAL MILES
Height of object *greater* than height of observer

Angle of elevation																	
2° 00'			1° 50'			1° 40'			1° 30'			1° 20'			1° 10'		
Height in feet	Range	Height in metres	Height in feet	Range	Height in metres	Height in feet	Range	Height in metres	Height in feet	Range	Height in metres	Height in feet	Range	Height in metres	Height in feet	Range	Height in metres
0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
535	5	163	491	5	149	447	5	136	402	5	122	358	5	109	314	5	95
1630	10	498	1500	10	458	1370	10	417	1230	10	377	1100	10	336	971	10	296
2770	15	845	2550	15	777	2330	15	710	2100	15	643	1880	15	575	1660	15	508
3940	20	1200	3630	20	1100	3320	20	1010	3020	20	920	2710	20	826	2400	20	731
5160	25	1570	4760	25	1450	4360	25	1330	3960	25	1200	3570	25	1080	3170	25	966
6410	30	1950	5920	30	1800	5440	30	1650	4950	30	1510	4460	30	1360	3980	30	1210
7700	35	2340	7130	35	2170	6550	35	1990	5970	35	1820	5400	35	1640	4820	35	1470
9030	40	2750	8360	40	2550	7700	40	2340	7040	40	2140	6370	40	1940	5710	40	1740
10400	45	3160	9640	45	2940	8890	45	2710	8140	45	2480	7390	45	2250	6630	45	2020
11800	50	3590	10900	50	3340	10100	50	3080	9280	50	2820	8440	50	2570	7590	50	2310
13200	55	4030	12300	55	3750	11300	55	3470	10400	55	3180	9520	55	2900	8590	55	2620
14700	60	4480	13700	60	4170	12600	60	3860	11600	60	3550	10600	60	3240	9630	60	2930
16200		4950	15100		4610	14000		4270	12900		3930	11800		3600	10700		3260

Angle of elevation																	
1° 00'			0° 55'			0° 50'			0° 45'			0° 40'			0° 35'		
Height in feet	Range	Height in metres	Height in feet	Range	Height in metres	Height in feet	Range	Height in metres	Height in feet	Range	Height in metres	Height in feet	Range	Height in metres	Height in feet	Range	Height in metres
0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
270	5	82	247	5	75	225	5	68	203	5	62	181	5	55	159	5	48
839	10	255	772	10	235	706	10	215	640	10	195	573	10	174	507	10	154
1440	15	440	1330	15	406	1220	15	373	1110	15	339	1000	15	305	893	15	272
2090	20	637	1930	20	590	1780	20	542	1620	20	495	1470	20	448	1310	20	401
2770	25	845	2570	25	784	2370	25	724	2170	25	663	1970	25	602	1770	25	542
3490	30	1060	3250	30	991	3000	30	916	2760	30	842	2520	30	768	2270	30	694
4250	35	1290	3960	35	1200	3670	35	1120	3390	35	1030	3100	35	945	2810	35	858
5050	40	1530	4710	40	1430	4380	40	1330	4050	40	1230	3720	40	1130	3390	40	1030
5880	45	1790	5500	45	1670	5130	45	1560	4750	45	1450	4380	45	1340	4000	45	1220
6750	50	2060	6330	50	1930	5910	50	1800	5490	50	1670	5070	50	1540	4650	50	1410
7670	55	2330	7200	55	2190	6740	55	2050	6270	55	1910	5810	55	1770	5340	55	1620
8610	60	2620	8100	60	2470	7600	60	2310	7090	60	2160	6580	60	2000	6070	60	1850
9600		2920	9050		2750	8500		2590	7940		2420	7390		2250	6840		2080

Angle of elevation																	
0° 30'			0° 25'			0° 20'			0° 15'			0° 10'			0° 05'		
Height in feet	Range	Height in metres	Height in feet	Range	Height in metres	Height in feet	Range	Height in metres	Height in feet	Range	Height in metres	Height in feet	Range	Height in metres	Height in feet	Range	Height in metres
0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
137	5	41	115	5	35	93	5	28	71	5	21	48	5	14	26	5	8
440	10	134	374	10	114	308	10	93	241	10	73	175	10	53	109	10	33
782	15	238	671	15	204	561	15	171	450	15	137	339	15	103	229	15	69
1160	20	354	1000	20	306	852	20	259	697	20	212	542	20	165	387	20	118
1570	25	481	1380	25	420	1180	25	360	982	25	299	783	25	238	584	25	178
2030	30	620	1790	30	546	1540	30	471	1300	30	397	1060	30	323	818	30	249
2520	35	770	2240	35	683	1950	35	595	1660	35	507	1370	35	420	1090	35	332
3060	40	932	2720	40	831	2360	40	730	2060	40	629	1730	40	528	1400	40	427
3620	45	1100	3250	45	991	2870	45	877	2500	45	762	2120	45	648	1750	45	533
4230	50	1290	3810	50	1160	3390	50	1030	2970	50	907	2550	50	779	2130	50	651
4880	55	1480	4410	55	1340	3950	55	1200	3480	55	1060	3020	55	922	2560	55	780
5560	60	1690	5050	60	1540	4540	60	1380	4040	60	1230	3530	60	1070	3020	60	921
6280		1910	5730		1740	5180		1570	4620		1410	4070		1240	3520		1070

X.—TABLE OF RANGES IN NAUTICAL MILES

Height of object *less* than height of observer

Angle of depression																	
0° 05'			0° 10'			0° 15'			0° 20'			0° 25'			0° 30'		
Height in feet	Range	Height in metres	Height in feet	Range	Height in metres	Height in feet	Range	Height in metres	Height in feet	Range	Height in metres	Height in feet	Range	Height in metres	Height in feet	Range	Height in metres
0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
4	0	1	9	0	2	13	0	4	17	0	5	21	0	6	26	0	8
11	1	3	24	1	7	38	1	11	51	1	15	64	1	19	77	1	23
17	2	5	39	2	12	61	2	18	83	2	25	106	2	32	127	2	39
21	3	6	52	3	15	83	3	25	114	3	34	145	3	44	176	3	53
24	4	7	64	4	19	103	4	31	143	4	43	183	4	55	223	4	68
25	5	8	74	5	22	122	5	37	171	5	52	220	5	67	268	5	81
26	6	8	82	6	25	140	6	42	197	6	60	255	6	77	312	6	95
27	7	8	89	7	27	156	7	47	222	7	67	288	7	88	355	7	108
27	8	7	95	8	29	170	8	52	245	8	74	320	8	97	396	8	120
26	9	5	99	9	30	183	9	55	267	9	81	351	9	107	435	9	132
0	10	0	103	10	32	212	10	64	323	10	98	434	10	132	544	10	166
			17	15	24	231	15	70	386	15	117	541	15	164	695	15	212
			77	20	4	213	20	65	411	20	125	609	20	185	808	20	246
			0	25	0	155	25	48	398	25	122	640	25	195	884	25	269
						59	30	18	346	30	106	634	30	194	921	30	280
						0	35	0	258	35	79	590	35	180	921	35	281
									130	40	40	506	40	155	882	40	269
									0	45	0	385	45	118	805	45	246
												226	50	69	690	50	211
												28	55	9	537	55	164
												0	60	0	346	60	106

Angle of depression																	
0° 35'			0° 40'			0° 45'			0° 50'			0° 55'			1° 00'		
Height in feet	Range	Height in metres	Height in feet	Range	Height in metres	Height in feet	Range	Height in metres	Height in feet	Range	Height in metres	Height in feet	Range	Height in metres	Height in feet	Range	Height in metres
0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
30	0	9	35	0	10	39	0	12	44	0	13	48	0	14	52	0	16
91	1	27	104	1	31	117	1	35	130	1	39	144	1	43	157	1	47
150	2	45	172	2	52	194	2	59	216	2	65	238	2	72	260	2	79
207	3	63	238	3	72	269	3	82	300	3	91	331	3	100	362	3	110
263	4	80	302	4	92	342	4	104	382	4	116	422	4	128	462	4	140
317	5	96	366	5	111	414	5	126	463	5	141	512	5	156	560	5	170
370	6	112	427	6	130	485	6	147	542	6	165	600	6	182	657	6	200
421	7	128	488	7	148	554	7	168	620	7	189	687	7	209	753	7	229
471	8	143	546	8	166	621	8	189	696	8	212	772	8	235	847	8	258
519	9	158	603	9	183	687	9	209	771	9	235	855	9	260	939	9	286
655	10	199	765	10	233	876	10	267	986	10	300	1090	10	334	1200	10	368
850	15	259	1000	15	306	1160	15	353	1310	15	400	1470	15	448	1620	15	495
1000	20	307	1200	20	367	1400	20	428	1600	20	489	1800	20	549	2000	20	610
1120	25	343	1370	25	417	1610	25	491	1850	25	566	2100	25	640	2340	25	714
1200	30	368	1490	30	456	1780	30	543	2070	30	631	2350	30	719	2640	30	806
1250	35	381	1580	35	482	1910	35	583	2240	35	685	2570	35	786	2910	35	887
1260	40	384	1630	40	497	2000	40	612	2380	40	727	2760	40	841	3130	40	956
1230	45	374	1650	45	502	2060	45	629	2480	45	757	2900	45	885	3320	45	1010
1160	50	352	1620	50	494	2080	50	634	2540	50	776	3010	50	918	3470	50	1050
1050	55	319	1560	55	474	2070	55	629	2570	55	783	3080	55	938	3580	55	1090
899	60	274	1460	60	443	2010	60	611	2560	60	780	3110	60	947	3660	60	1110

For explanation, see page 224.

X.—TABLE OF RANGES IN NAUTICAL MILES

Height of object *less* than height of observer

Angle of depression																	
1° 10'			1° 20'			1° 30'			1° 40'			1° 50'			2° 00'		
Height in feet	Range	Height in metres	Height in feet	Range	Height in metres	Height in feet	Range	Height in metres	Height in feet	Range	Height in metres	Height in feet	Range	Height in metres	Height in feet	Range	Height in metres
0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
61	1	18	70	1	21	79	1	24	88	1	26	97	1	29	106	1	32
183	2	56	210	2	64	237	2	72	263	2	80	290	2	88	316	2	96
305	3	92	349	3	106	393	3	119	437	3	133	481	3	146	526	3	160
424	4	129	486	4	148	548	4	167	610	4	185	672	4	204	734	4	223
541	5	165	621	5	189	701	5	213	780	5	238	860	5	262	940	5	286
658	6	200	755	6	230	852	6	259	950	6	289	1040	6	319	1140	6	349
772	7	235	887	7	270	1000	7	305	1110	7	340	1230	7	375	1340	7	410
886	8	270	1010	8	310	1150	8	351	1280	8	391	1410	8	432	1550	8	472
997	9	304	1140	9	350	1290	9	395	1440	9	441	1590	9	487	1750	9	533
1100	10	337	1270	10	388	1440	10	440	1610	10	491	1780	10	542	1940	10	594
1430	15	435	1650	15	503	1870	15	570	2090	15	638	2310	15	705	2530	15	772
1930	20	589	2240	20	684	2550	20	778	2860	20	872	3170	20	967	3480	20	1060
2400	25	732	2790	25	853	3190	25	974	3590	25	1090	3990	25	1210	4390	25	1330
2830	30	862	3310	30	1010	3800	30	1150	4290	30	1300	4770	30	1450	5260	30	1600
3220	35	982	3790	35	1150	4370	35	1330	4940	35	1500	5520	35	1680	6090	35	1850
3570	40	1080	4230	40	1290	4900	40	1490	5560	40	1690	6230	40	1890	6890	40	2100
3880	45	1180	4640	45	1410	5390	45	1640	6140	45	1870	6890	45	2100	7650	45	2330
4160	50	1270	5000	50	1520	5840	50	1780	6680	50	2030	7530	50	2290	8370	50	2550
4400	55	1340	5330	55	1620	6260	55	1900	7190	55	2190	8120	55	2470	9050	55	2750
4600	60	1400	5620	60	1710	6640	60	2020	7660	60	2330	8670	60	2640	9690	60	2950
4760		1450	5870		1790	6980		2120	8080		2460	9190		2800	10300		3140

Angle of depression																	
2° 20'			2° 40'			3° 00'			3° 20'			3° 40'			4° 00'		
Height in feet	Range	Height in metres	Height in feet	Range	Height in metres	Height in feet	Range	Height in metres	Height in feet	Range	Height in metres	Height in feet	Range	Height in metres	Height in feet	Range	Height in metres
0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
123	1	37	141	1	43	159	1	48	176	1	53	194	1	59	212	1	64
369	2	112	422	2	128	476	2	145	529	2	161	582	2	177	636	2	193
614	3	187	703	3	214	792	3	241	880	3	268	969	3	295	1050	3	322
858	4	261	982	4	299	1100	4	337	1230	4	375	1350	4	412	1470	4	450
1090	5	335	1250	5	383	1410	5	432	1570	5	481	1730	5	529	1890	5	578
1340	6	408	1530	6	467	1730	6	527	1920	6	586	2120	6	646	2310	6	706
1570	7	481	1800	7	551	2040	7	621	2270	7	692	2500	7	762	2730	7	832
1810	8	553	2080	8	634	2340	8	715	2610	8	796	2880	8	877	3140	8	959
2050	9	625	2350	9	717	2650	9	809	2950	9	901	3250	9	993	3560	9	1080
2280	10	696	2620	10	799	2950	10	902	3290	10	1000	3630	10	1100	3970	10	1210
2970	15	908	3420	15	1040	3860	15	1170	4300	15	1310	4750	15	1440	5190	15	1580
4100	20	1250	4720	20	1430	5340	20	1620	5960	20	1810	6580	20	2000	7200	20	2190
5190	25	1580	5980	25	1820	6780	25	2060	7580	25	2310	8380	25	2550	9180	25	2790
6230	30	1900	7210	30	2190	8180	30	2490	9160	30	2790	10100	30	3090	11100	30	3380
7250	35	2210	8400	35	2560	9550	35	2910	10700	35	3260	11800	35	3610	13000	35	3960
8220	40	2500	9550	40	2910	10800	40	3310	12200	40	3720	13500	40	4120	14800	40	4530
9150	45	2790	10600	45	3250	12100	45	3710	13600	45	4170	15100	45	4620	16700	45	5090
10000	50	3060	11700	50	3590	13400	50	4090	15100	50	4600	16700	50	5120	18400	50	5630
10900	55	3320	12700	55	3890	14600	55	4460	16400	55	5020	18300	55	5590	20200	55	6160
11700	60	3570	13700	60	4190	15800	60	4810	17800	60	5440	19900	60	6060	21900	60	6680
12500		3810	14700		4490	16900		5160	19100		5840	21300		6510	23600		7190

For explanation, see page 224.

X.—TABLE OF RANGES IN NAUTICAL MILES

Height of object *less* than height of observer

Angle of depression																	
4° 30'			5° 00'			5° 30'			6° 00'			6° 30'			7° 00'		
Height in feet	Range in metres	Height in metres	Height in feet	Range in metres	Height in metres	Height in feet	Range in metres	Height in metres	Height in feet	Range in metres	Height in metres	Height in feet	Range in metres	Height in metres	Height in feet	Range in metres	Height in metres
0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
238	0	72	265	0	81	292	0	89	319	0	97	346	0	105	373	0	113
716	1	218	706	1	242	876	1	267	956	1	291	1030	1	316	1110	1	340
1190	2	363	1320	2	404	1450	2	444	1590	2	485	1720	2	526	1860	2	567
1660	3	507	1850	3	564	2040	3	621	2220	3	679	2410	3	736	2600	3	793
2130	4	651	2370	4	725	2610	4	798	2860	4	872	3100	4	945	3340	4	1010
2600	5	795	2900	5	885	3190	5	974	3490	5	1060	3780	5	1150	4080	5	1240
3070	6	938	3420	6	1040	3770	6	1150	4120	6	1250	4470	6	1360	4820	6	1460
3540	7	1080	3940	7	1200	4340	7	1320	4750	7	1440	5150	7	1570	5550	7	1690
4010	8	1220	4460	8	1360	4920	8	1500	5370	8	1630	5830	8	1770	6290	8	1910
4470	9	1360	4980	9	1510	5490	9	1670	6000	9	1830	6510	9	1980	7020	9	2140
5860	10	1780	6530	10	1990	7200	10	2190	7870	10	2390	8540	10	2600	9210	10	2800
8140	15	2480	9070	15	2760	10000	15	3050	10900	15	3330	11800	15	3620	12800	15	3910
10300	20	3160	11500	20	3530	12700	20	3890	14000	20	4260	15200	20	4630	16400	20	5000
12500	25	3830	14000	25	4280	15500	25	4730	16900	25	5180	18400	25	5630	19900	25	6080
14700	30	4490	16400	30	5020	18200	30	5550	19900	30	6080	21700	30	6620	23400	30	7150
16800	35	5140	18800	35	5750	20800	35	6360	22800	35	6980	24900	35	7590	26900	35	8210
18900	40	5780	21200	40	6470	23500	40	7160	25800	40	7860	28000	40	8550	30300	40	9250
21000	45	6400	23500	45	7180	26000	45	7950	28600	45	8730	31100	45	9510	33700	45	10200
23000	50	7020	25800	50	7870	28600	50	8730	31400	50	9590	34200	50	10400	37100	50	11300
25000	55	7620	28000	55	8550	31100	55	9490	34200	55	10400	37300	55	11300	40400	55	12300
26900	60	8210	30200	60	9230	33600	60	10200	36900	60	11200	40300	60	12200	43600	60	13300

Angle of depression																	
7° 30'			8° 00'			8° 30'			9° 00'			9° 30'			10° 00'		
Height in feet	Range in metres	Height in metres	Height in feet	Range in metres	Height in metres	Height in feet	Range in metres	Height in metres	Height in feet	Range in metres	Height in metres	Height in feet	Range in metres	Height in metres	Height in feet	Range in metres	Height in metres
0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
399	1	121	427	1	130	454	1	138	481	1	146	508	1	154	535	1	163
1190	2	365	1270	2	390	1360	2	415	1440	2	439	1520	2	464	1600	2	489
1990	3	608	2130	3	649	2260	3	691	2400	3	732	2540	3	774	2670	3	815
2790	4	851	2980	4	909	3170	4	966	3360	4	1020	3550	4	1080	3740	4	1140
3580	5	1090	3830	5	1160	4070	5	1240	4310	5	1310	4560	5	1390	4810	5	1460
4380	6	1330	4670	6	1420	4970	6	1510	5270	6	1600	5570	6	1690	5870	6	1790
5170	7	1570	5520	7	1680	5870	7	1790	6220	7	1890	6580	7	2000	6930	7	2110
5960	8	1810	6360	8	1940	6770	8	2060	7180	8	2180	7580	8	2310	8000	8	2430
6750	9	2050	7210	9	2190	7670	9	2330	8130	9	2470	8590	9	2610	9060	9	2760
7530	10	2290	8050	10	2450	8560	10	2610	9080	10	2760	9600	10	2920	10100	10	3080
9880	15	3010	10500	15	3220	11200	15	3420	11900	15	3630	12600	15	3840	13200	15	4050
13700	20	4200	14700	20	4480	15600	20	4770	16600	20	5060	17500	20	5350	18500	20	5640
17600	25	5370	18800	25	5740	20000	25	6110	21200	25	6480	22500	25	6860	23700	25	7230
21400	30	6530	22900	30	6980	24400	30	7440	25900	30	7890	27400	30	8350	28900	30	8810
25200	35	7680	26900	35	8220	28700	35	8760	30500	35	9290	32200	35	9830	34000	35	10300
28900	40	8820	30900	40	9440	33000	40	10000	35000	40	10600	37000	40	11300	39100	40	11900
32600	45	9950	34900	45	10600	37200	45	11300	39500	45	12000	41800	45	12700	44200	45	13400
36300	50	11000	38800	50	11800	41400	50	12600	44000	50	13400	46600	50	14200	49200	50	15000
39900	55	12100	42700	55	13000	45600	55	13900	48400	55	14700	51300	55	15600	54200	55	16500
43500	60	13200	46600	60	14200	49700	60	15100	52800	60	16100	56000	60	17000	59100	60	18000
47000		14300	50400		15300	53800		16400	57200		17400	60600		18400	64000		19500

For explanation, see page 224.

XI.—TEMPERATURE CONVERSION **FAHRENHEIT AND CENTIGRADE**

°F	°C	°F	°C	°F	°C	°F	°C	°F	°C	°F	°C	°F	°C
-52	-46	-14	-25	+23	-4	+61	+17	+99	+38	+137	+59	+175	+80
50	45	13	24	25	3	63	18	101	39	139	60	176	81
49	44	11	23	27	2	65	19	103	40	140	61	178	82
47	43	9	22	29	-1	67	20	104	41	142	62	180	83
45	42	7	21	31	0	68	21	106	42	144	63	182	84
43	41	5	20	32	+1	70	22	108	43	146	64	184	85
41	40	4	19	34	2	72	23	110	44	148	65	185	86
40	39	-2	18	36	3	74	24	112	45	149	66	187	87
38	38	0	17	38	4	76	25	113	46	151	67	189	88
36	37	+2	16	40	5	77	26	115	47	153	68	191	89
34	36	4	15	41	6	79	27	117	48	155	69	193	90
32	35	5	14	43	7	81	28	119	49	157	70	194	91
31	34	7	13	45	8	83	29	121	50	158	71	196	92
29	33	9	12	47	9	85	30	122	51	160	72	198	93
27	32	11	11	49	10	86	31	124	52	162	73	200	94
25	31	13	10	50	11	88	32	126	53	164	74	202	95
23	30	14	9	52	12	90	33	128	54	166	75	203	96
22	29	16	8	54	13	92	34	130	55	167	76	205	97
20	28	18	7	56	14	94	35	131	56	169	77	207	98
18	27	20	6	58	15	95	36	133	57	171	78	209	99
16	26	22	5	59	+16	97	37	135	58	173	79	211	100
-14	-26	+23	-5	+61	+17	+99	+38	+137	+59	+175	+80	+212	+100

XII.—CONVERSION FACTORS

Conversion	Ratio	Factor	Reciprocal
DISTANCE			
Statute Miles to Nautical Miles ...	66 to 76	0.8684	1.1515
Statute Miles „ Kilometres ...	66 „ 41	1.6093	0.6214
Nautical Miles „ Kilometres ...	76 „ 41	1.8531	0.5396
Feet „ Metres ...	25 „ 82	0.3048	3.2808
Yards „ Metres ...	32 „ 35	0.9144	1.0936
Fathoms „ Feet ...	6 „ 1	6.0	0.1667
SPEED			
Miles per hour to Knots ...	66 to 76	0.8684	1.1515
Miles per hour „ Metres per second ...	38 „ 85	0.4470	2.2369
Knots „ Metres per second ...	35 „ 68	0.5148	1.9426
Miles per hour „ Feet per second ...	22 „ 15	1.4667	0.6818
LIQUID MEASURE			
Gallons to Litres ...	50 to 11	4.5460	0.2200
WEIGHT			
Pounds to Kilograms ...	44 to 97	0.4536	2.2046
PRESSURE			
Inches of Mercury to Millibars ...	2100 to 62	33.87	0.02953

XIII.—CONVERSION OF TIME TO ARC

For Intervals of 10 ^m						Interpolation Table											
h	m	h	m	h	m	h	m	h	m	h	m	h	m	h	m	h	m
00	00	00	00	08	00	120	00	16	00	240	00	00	00	03	17	00	50
10	2 30	10	122 30	10	242 30	02	0 01	22	0 51	42	1 41	06	37	01	40	06	37
20	5 00	20	125 00	20	245 00	05	0 02	25	0 52	45	1 42	07	01	01	46	07	01
30	7 30	30	127 30	30	247 30	10	0 03	30	0 53	50	1 43	06	58	01	45	06	58
40	10 00	40	130 00	40	250 00	13	0 04	33	0 54	53	1 44	07	01	01	46	07	01
50	12 30	50	132 30	50	252 30	18	0 05	38	0 55	58	1 45	07	01	01	46	07	01
01	15 00	09	135 00	17	255 00	21	0 06	41	0 56	06	1 45	07	01	01	46	07	01
10	17 30	10	137 30	10	257 30	26	0 07	46	0 57	06	1 47	07	01	01	46	07	01
20	20 00	20	140 00	20	260 00	29	0 08	49	0 58	09	1 48	07	01	01	46	07	01
30	22 30	30	142 30	30	262 30	34	0 09	54	0 59	14	1 49	07	01	01	46	07	01
40	25 00	40	145 00	40	265 00	37	0 10	57	1 00	17	1 50	07	01	01	46	07	01
50	27 30	50	147 30	50	267 30	42	0 11	02	1 01	22	1 51	07	01	01	46	07	01
02	30 00	10	150 00	18	270 00	45	0 12	05	1 02	25	1 52	07	01	01	46	07	01
10	32 30	10	152 30	10	272 30	50	0 13	10	1 03	30	1 53	07	01	01	46	07	01
20	35 00	20	155 00	20	275 00	53	0 14	13	1 04	33	1 54	07	01	01	46	07	01
30	37 30	30	157 30	30	277 30	58	0 15	18	1 05	38	1 55	07	01	01	46	07	01
40	40 00	40	160 00	40	280 00	01	0 16	21	1 06	41	1 56	07	01	01	46	07	01
50	42 30	50	162 30	50	282 30	06	0 17	26	1 07	46	1 57	07	01	01	46	07	01
03	45 00	11	165 00	19	285 00	09	0 18	29	1 08	49	1 58	07	01	01	46	07	01
10	47 30	10	167 30	10	287 30	14	0 19	34	1 09	54	1 59	07	01	01	46	07	01
20	50 00	20	170 00	20	290 00	17	0 20	37	1 10	57	2 00	07	01	01	46	07	01
30	52 30	30	172 30	30	292 30	22	0 21	42	1 11	02	2 01	07	01	01	46	07	01
40	55 00	40	175 00	40	295 00	25	0 22	45	1 12	05	2 02	07	01	01	46	07	01
50	57 30	50	177 30	50	297 30	30	0 23	50	1 13	10	2 03	07	01	01	46	07	01
04	60 00	12	180 00	20	300 00	33	0 24	53	1 14	13	2 04	07	01	01	46	07	01
10	62 30	10	182 30	10	302 30	38	0 25	58	1 15	18	2 05	07	01	01	46	07	01
20	65 00	20	185 00	20	305 00	41	0 26	01	1 16	21	2 06	07	01	01	46	07	01
30	67 30	30	187 30	30	307 30	46	0 27	06	1 17	26	2 07	07	01	01	46	07	01
40	70 00	40	190 00	40	310 00	49	0 28	09	1 18	29	2 08	07	01	01	46	07	01
50	72 30	50	192 30	50	312 30	54	0 29	14	1 19	34	2 09	07	01	01	46	07	01
05	75 00	13	195 00	21	315 00	57	0 30	17	1 20	37	2 10	07	01	01	46	07	01
10	77 30	10	197 30	10	317 30	02	0 31	22	1 21	42	2 11	07	01	01	46	07	01
20	80 00	20	200 00	20	320 00	05	0 32	25	1 22	45	2 12	07	01	01	46	07	01
30	82 30	30	202 30	30	322 30	10	0 33	30	1 23	50	2 13	07	01	01	46	07	01
40	85 00	40	205 00	40	325 00	13	0 34	33	1 24	53	2 14	07	01	01	46	07	01
50	87 30	50	207 30	50	327 30	18	0 35	38	1 25	58	2 15	07	01	01	46	07	01
06	90 00	14	210 00	22	330 00	21	0 36	41	1 26	01	2 16	07	01	01	46	07	01
10	92 30	10	212 30	10	332 30	26	0 37	46	1 27	06	2 17	07	01	01	46	07	01
20	95 00	20	215 00	20	335 00	29	0 38	49	1 28	09	2 18	07	01	01	46	07	01
30	97 30	30	217 30	30	337 30	34	0 39	54	1 29	14	2 19	07	01	01	46	07	01
40	100 00	40	220 00	40	340 00	37	0 40	57	1 30	17	2 20	07	01	01	46	07	01
50	102 30	50	222 30	50	342 30	42	0 41	02	1 31	22	2 21	07	01	01	46	07	01
07	105 00	15	225 00	23	345 00	45	0 42	05	1 32	25	2 22	07	01	01	46	07	01
10	107 30	10	227 30	10	347 30	50	0 43	10	1 33	30	2 23	07	01	01	46	07	01
20	110 00	20	230 00	20	350 00	53	0 44	13	1 34	33	2 24	07	01	01	46	07	01
30	112 30	30	232 30	30	352 30	58	0 45	18	1 35	38	2 25	07	01	01	46	07	01
40	115 00	40	235 00	40	355 00	01	0 46	21	1 36	41	2 26	07	01	01	46	07	01
50	117 30	50	237 30	50	357 30	06	0 47	26	1 37	46	2 27	07	01	01	46	07	01
						09	0 48	29	1 38	49	2 28	07	01	01	46	07	01
						14	0 49	34	1 39	54	2 29	07	01	01	46	07	01
						17	0 50	37	1 40	57	2 30	07	01	01	46	07	01
						03	22	06	42	10	00	07	01	01	46	07	01

When the argument is an exact tabulated value, the upper of the two possible values of the result should be taken.

XIV.—CONVERSION OF ARC TO TIME

DEGREES												MINUTES	
°	'	°	'	°	'	°	'	°	'	°	'	°	'
0	00	60	4 00	120	8 00	180	12 00	240	16 00	300	20 00	0	00
1	04	61	4 04	121	8 04	181	12 04	241	16 04	301	20 04	1	04
2	08	62	4 08	122	8 08	182	12 08	242	16 08	302	20 08	2	08
3	12	63	4 12	123	8 12	183	12 12	243	16 12	303	20 12	3	12
4	16	64	4 16	124	8 16	184	12 16	244	16 16	304	20 16	4	16
5	20	65	4 20	125	8 20	185	12 20	245	16 20	305	20 20	5	20
6	24	66	4 24	126	8 24	186	12 24	246	16 24	306	20 24	6	24
7	28	67	4 28	127	8 28	187	12 28	247	16 28	307	20 28	7	28
8	32	68	4 32	128	8 32	188	12 32	248	16 32	308	20 32	8	32
9	36	69	4 36	129	8 36	189	12 36	249	16 36	309	20 36	9	36
10	40	70	4 40	130	8 40	190	12 40	250	16 40	310	20 40	10	40
11	44	71	4 44	131	8 44	191	12 44	251	16 44	311	20 44	11	44
12	48	72	4 48	132	8 48	192	12 48	252	16 48	312	20 48	12	48
13	52	73	4 52	133	8 52	193	12 52	253	16 52	313	20 52	13	52
14	56	74	4 56	134	8 56	194	12 56	254	16 56	314	20 56	14	56
15	00	75	5 00	135	9 00	195	13 00	255	17 00	315	21 00	15	00
16	04	76	5 04	136	9 04	196	13 04	256	17 04	316	21 04	16	04
17	08	77	5 08	137	9 08	197	13 08	257	17 08	317	21 08	17	08
18	12	78	5 12	138	9 12	198	13 12	258	17 12	318	21 12	18	12
19	16	79	5 16	139	9 16	199	13 16	259	17 16	319	21 16	19	16
20	20	80	5 20	140	9 20	200	13 20	260	17 20	320	21 20	20	20
21	24	81	5 24	141	9 24	201	13 24	261	17 24	321	21 24	21	24
22	28	82	5 28	142	9 28	202	13 28	262	17 28	322	21 28	22	28
23	32	83	5 32	143	9 32	203	13 32	263	17 32	323	21 32	23	32
24	36	84	5 36	144	9 36	204	13 36	264	17 36	324	21 36	24	36
25	40	85	5 40	145	9 40	205	13 40	265	17 40	325	21 40	25	40
26	44	86	5 44	146	9 44	206	13 44	266	17 44	326	21 44	26	44
27	48	87	5 48	147	9 48	207	13 48	267	17 48	327	21 48	27	48
28	52	88	5 52	148	9 52	208	13 52	268	17 52	328	21 52	28	52
29	56	89	5 56	149	9 56	209	13 56	269	17 56	329	21 56	29	56
30	00	90	6 00	150	10 00	210	14 00	270	18 00	330	22 00	30	00
31	04	91	6 04	151	10 04	211	14 04	271	18 04	331	22 04	31	04
32	08	92	6 08	152	10 08	212	14 08	272	18 08	332	22 08	32	08
33	12	93	6 12	153	10 12	213	14 12	273	18 12	333	22 12	33	12
34	16	94	6 16	154	10 16	214	14 16	274	18 16	334	22 16	34	16
35	20	95	6 20	155	10 20	215	14 20	275	18 20	335	22 20	35	20
36	24	96	6 24	156	10 24	216	14 24	276	18 24	336	22 24	36	24
37	28	97	6 28	157	10 28	217	14 28	277	18 28	337	22 28	37	28
38	32	98	6 32	158	10 32	218	14 32	278	18 32	338	22 32	38	32
39	36	99	6 36	159	10 36	219	14 36	279	18 36	339	22 36	39	36
40	40	100	6 40	160	10 40	220	14 40	280	18 40	340	22 40	40	40
41	44	101	6 44	161	10 44	221	14 44	281	18 44	341	22 44	41	44
42	48	102	6 48	162	10 48	222	14 48	282	18 48	342	22 48	42	48
43	52	103	6 52	163	10 52	223	14 52	283	18 52	343	22 52	43	52
44	56	104	6 56	164	10 56	224	14 56	284	18 56	344	22 56	44	56
45	00	105	7 00	165	11 00	225	15 00	285	19 00	345	23 00	45	00
46	04	106	7 04	166	11 04	226	15 04	286	19 04	346	23 04	46	04
47	08	107	7 08	167	11 08	227	15 08	287	19 08	347	23 08	47	08
48	12	108	7 12	168	11 12	228	15 12	288	19 12	348	23 12	48	12
49	16	109	7 16	169	11 16	229	15 16	289	19 16	349	23 16	49	16
50	20	110	7 20	170	11 20	230	15 20	290	19 20	350	23 20	50	20
51	24	111	7 24	171	11 24	231	15 24	291	19 24	351	23 24	51	24
52	28	112	7 28	172	11 28	232	15 28	292	19 28	352	23 28	52	28
53	32	113	7 32	173	11 32	233	15 32	293	19 32	353	23 32	53	32
54	36	114	7 36	174	11 36	234	15 36	294	19 36	354	23 36	54	36
55	40	115	7 40	175	11 40	235	15 40	295	19 40	355	23 40	55	40
56	44	116	7 44	176	11 44	236	15 44	296	19 44	356	23 44	56	44
57	48	117	7 48	177	11 48	237	15 48	297	19 48	357	23 48	57	48
58	52	118	7 52	178	11 52	238	15 52	298	19 52	358	23 52	58	52
59	56	119	7 56	179	11 56	239	15 56	299	19 56	359	23 56	59	56

XV.—CORRECTION TO TABULATED ALTITUDE FOR MINUTES OF DECLINATION

d	1	2	3	4	5	6	7	8	9	10	11	12	13	14	15	16	17	18	19	20	21	22	23	24	25	26	27	28	29	30	d
00	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	00
01	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	01
02	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	02
03	0	0	0	0	0	0	0	0	0	0	1	1	1	1	1	1	1	1	1	1	1	1	1	1	1	1	1	1	1	1	03
04	0	0	0	0	0	0	0	1	1	1	1	1	1	1	1	1	1	1	1	1	1	1	2	2	2	2	2	2	2	2	04
05	0	0	0	0	0	0	1	1	1	1	1	1	1	1	1	1	2	2	2	2	2	2	2	2	2	2	2	2	2	2	05
06	0	0	0	0	0	1	1	1	1	1	1	1	1	1	2	2	2	2	2	2	2	2	2	2	2	2	3	3	3	3	06
07	0	0	0	0	0	1	1	1	1	1	1	1	2	2	2	2	2	2	2	2	2	2	3	3	3	3	3	3	3	3	07
08	0	0	0	0	1	1	1	1	1	1	2	2	2	2	2	2	2	2	3	3	3	3	3	3	3	3	3	4	4	4	08
09	0	0	0	0	1	1	1	1	1	2	2	2	2	2	2	2	3	3	3	3	3	3	3	4	4	4	4	4	4	4	09
10	0	0	0	1	1	1	1	1	2	2	2	2	2	2	2	3	3	3	3	3	3	4	4	4	4	4	4	4	5	5	10
11	0	0	1	1	1	1	1	1	2	2	2	2	2	3	3	3	3	3	3	4	4	4	4	4	4	5	5	5	5	5	11
12	0	0	1	1	1	1	1	2	2	2	2	2	3	3	3	3	3	3	4	4	4	4	4	4	5	5	5	5	6	6	12
13	0	0	1	1	1	1	2	2	2	2	2	3	3	3	3	3	4	4	4	4	4	4	5	5	5	5	5	6	6	6	13
14	0	0	1	1	1	1	2	2	2	2	3	3	3	3	4	4	4	4	4	5	5	5	5	5	6	6	6	6	7	7	14
15	0	0	1	1	1	2	2	2	2	2	3	3	3	4	4	4	4	4	5	5	5	6	6	6	6	6	6	7	7	8	15
16	0	1	1	1	1	2	2	2	2	3	3	3	3	4	4	4	5	5	5	5	6	6	6	6	6	7	7	7	8	8	16
17	0	1	1	1	1	2	2	2	3	3	3	3	4	4	4	5	5	5	5	6	6	6	7	7	7	7	8	8	8	8	17
18	0	1	1	1	2	2	2	2	3	3	3	4	4	4	4	5	5	5	6	6	6	7	7	7	8	8	8	8	9	9	18
19	0	1	1	1	2	2	2	3	3	3	3	4	4	4	5	5	5	6	6	6	7	7	7	8	8	8	9	9	9	10	19
20	0	1	1	1	2	2	2	3	3	3	4	4	4	5	5	5	6	6	6	7	7	7	8	8	8	9	9	9	10	10	20
21	0	1	1	1	2	2	2	3	3	4	4	4	5	5	5	6	6	6	7	7	7	8	8	8	9	9	9	10	10	10	21
22	0	1	1	1	2	2	3	3	3	4	4	4	5	5	6	6	6	7	7	8	8	8	9	9	9	10	10	11	11	11	22
23	0	1	1	2	2	2	3	3	3	4	4	5	5	5	6	6	7	7	8	8	8	9	9	9	10	10	10	11	11	12	23
24	0	1	1	2	2	2	3	3	4	4	4	5	5	6	6	6	7	7	8	8	8	9	9	10	10	10	11	11	12	12	24
25	0	1	1	2	2	2	3	3	4	4	5	5	5	6	6	7	7	8	8	8	9	9	10	10	10	11	11	12	12	12	25
26	0	1	1	2	2	3	3	3	4	4	5	5	6	6	6	7	7	8	8	9	9	10	10	10	11	11	12	12	13	13	26
27	0	1	1	2	2	3	3	4	4	4	5	5	6	6	7	7	8	8	9	9	9	10	10	11	11	12	12	13	13	14	27
28	0	1	1	2	2	3	3	4	4	5	5	6	6	7	7	8	8	9	9	10	10	10	11	11	12	12	13	13	14	14	28
29	0	1	1	2	2	3	3	4	4	5	5	6	6	7	7	8	8	9	9	10	10	11	11	12	12	13	13	14	14	14	29
30	0	1	2	2	2	3	4	4	4	5	6	6	6	7	7	8	8	8	9	10	10	10	11	12	12	12	13	14	14	15	30
31	1	1	2	2	3	3	4	4	5	5	6	6	7	7	8	8	9	9	10	10	11	11	12	12	13	13	14	15	15	16	31
32	1	1	2	2	3	3	4	4	5	5	6	6	7	7	8	9	9	10	10	11	11	12	12	13	13	14	15	16	16	17	32
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36	1	1	2	2	3	4	4	5	5	6	7	7	8	8	9	10	10	11	11	12	12	13	13	14	14	15	16	17	17	18	36
37	1	1	2	2	3	4	4	5	6	6	7	7	8	9	9	10	10	11	12	12	13	13	14	14	15	16	17	17	18	18	37
38	1	1	2	3	3	4	4	5	6	7	7	8	8	9	10	10	11	11	12	12	13	13	14	15	15	16	17	18	18	19	38
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40	1	1	2	3	3	4	5	5	6	7	7	8	9	9	10	11	11	12	13	13	14	14	15	15	16	17	18	19	19	20	40
41	1	1	2	3	3	4	5	5	6	7	8	8	9	10	10	11	12	12	13	14	14	15	16	16	17	18	18	19	20	20	41
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43	1	1	2	3	4	4	5	6	6	7	8	9	9	10	11	11	12	13	14	14	15	16	16	17	18	19	19	20	21	22	43
44	1	1	2	3	4	4	5	6	7	7	8	9	10	10	11	12	12	13	14	15	15	16	17	18	18	19	20	21	21	22	44
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46	1	2	2	3	4	5	5	6	7	8	8	9	10	11	12	12	13	14	15	15	16	17	18	18	19	20	21	22	23	23	46
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57	1	2	3	4	5	6	7	8	9	10	10	11	12	13	14	15	16	17	18	19	20	21	22	23	24	25	26	27	28	28	57

XV.—CORRECTION TO TABULATED ALTITUDE FOR MINUTES OF DECLINATION

d	31	32	33	34	35	36	37	38	39	40	41	42	43	44	45	46	47	48	49	50	51	52	53	54	55	56	57	58	59	60	d	
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02	1	1	1	1	1	1	1	1	1	1	1	1	1	1	2	2	2	2	2	2	2	2	2	2	2	2	2	2	2	2	02	
03	2	2	2	2	2	2	2	2	2	2	2	2	2	2	2	2	2	2	2	2	3	3	3	3	3	3	3	3	3	3	03	
04	2	2	2	2	2	2	2	3	3	3	3	3	3	3	3	3	3	3	3	3	3	3	4	4	4	4	4	4	4	4	04	
05	3	3	3	3	3	3	3	3	3	3	3	3	4	4	4	4	4	4	4	4	4	4	4	4	4	5	5	5	5	5	05	
06	3	3	3	3	4	4	4	4	4	4	4	4	4	4	4	5	5	5	5	5	5	5	5	5	5	6	6	6	6	6	06	
07	4	4	4	4	4	4	4	4	4	4	5	5	5	5	5	5	5	6	6	6	6	6	6	6	6	6	7	7	7	7	7	07
08	4	4	4	5	5	5	5	5	5	5	5	5	6	6	6	6	6	6	6	7	7	7	7	7	7	7	7	8	8	8	08	
09	5	5	5	5	5	5	6	6	6	6	6	6	6	7	7	7	7	7	7	8	8	8	8	8	8	8	8	9	9	9	9	09
10	5	5	6	6	6	6	6	6	6	7	7	7	7	7	8	8	8	8	8	8	8	9	9	9	9	9	9	10	10	10	10	10
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17	9	9	9	10	10	10	10	11	11	11	12	12	12	12	13	13	13	14	14	14	14	15	15	15	16	16	16	16	17	17	17	17
18	9	10	10	10	10	11	11	11	12</																							