

LAT.	35°		36°		37°		38°		39°		LAT.
H.A.	Alt.	Az.	Alt.	Az.	Alt.	Az.	Alt.	Az.	Alt.	Az.	H.A.
45	49 42+26	93	49 37+28	94	49 32+29	96	49 26+30	97	49 18+32	98	315
46	48 52 27	93	48 49 28	94	48 44 29	95	48 39 30	96	48 32 31	97	314
47	48 03 27	92	48 01 27	93	47 57 29	94	47 52 30	95	47 45 32	96	313
48	47 14 26	91	47 12 28	93	47 09 29	94	47 05 30	95	46 59 32	96	312
49	46 25 26	91	46 24 27	92	46 21 29	93	46 17 31	94	46 13 31	95	311
50	45 36+26	90	45 35+28	91	45 33+29	92	45 30+30	93	45 26+32	94	310
51	44 47 26	90	44 47 27	91	44 45 29	92	44 43 30	93	44 40 31	94	309
52	43 58 26	89	43 58 28	90	43 58 28	91	43 56 30	92	43 53 31	93	308
53	43 09 26	89	43 10 27	90	43 10 28	90	43 09 30	91	43 07 31	92	307
54	42 20 26	88	42 21 28	89	42 22 28	90	42 21 30	91	42 20 31	92	306
55	41 30+27	88	41 33+27	88	41 34+29	89	41 34+30	90	41 34+31	91	305
56	40 41 27	87	40 44 28	88	40 46 29	89	40 47 30	90	40 47 31	90	304
57	39 52 27	86	39 56 27	87	39 58 29	88	40 00 30	89	40 00 32	90	303
58	39 03 27	86	39 07 28	87	39 10 29	88	39 12 30	88	39 14 31	89	302
59	38 14 27	85	38 19 28	86	38 22 29	87	38 25 30	88	38 27 31	89	301
60	37 25+27	85	37 30+28	86	37 35+29	86	37 38+30	87	37 41+31	88	300
61	36 37 26	84	36 42 28	85	36 47 29	86	36 51 30	87	36 54 31	87	299
62	35 48 27	84	35 54 28	85	35 59 29	85	36 04 30	86	36 07 32	87	298
63	34 59 27	83	35 05 29	84	35 11 30	85	35 17 30	85	35 21 31	86	297
64	34 10 27	83	34 17 28	83	34 24 29	84	34 29 31	85	34 34 32	86	296
65	33 21+28	82	33 29+28	83	33 36+30	84	33 42+31	84	33 48+32	85	295
66	32 33 27	82	32 41 28	82	32 49 29	83	32 55 31	84	33 02 31	84	294
67	31 44 28	81	31 53 29	82	32 01 30	83	32 08 31	83	32 15 32	84	293
68	30 56 27	81	31 05 29	81	31 14 29	82	31 22 30	83	31 29 32	83	292
69	30 07 28	80	30 17 29	81	30 26 30	81	30 35 31	82	30 43 32	83	291
70	29 19+28	80	29 29+29	80	29 39+30	81	29 48+31	82	29 57+32	82	290
71	28 31 28	79	28 41 30	80	28 52 30	80	29 01 32	81	29 10 33	82	289
72	27 42 29	79	27 54 29	79	28 05 30	80	28 15 31	80	28 24 33	81	288
73	26 54 29	78	27 06 30	79	27 17 31	79	27 28 32	80	27 38 33	80	287
74	26 06 29	78	26 19 29	78	26 30 31	79	26 42 31	79	26 53 32	80	286
75	25 18+29	77	25 31+30	78	25 44+30	78	25 55+32	79	26 07+33	79	285
76	24 30 29	77	24 44 30	77	24 57 31	78	25 09 32	78	25 21 33	79	284
77	23 43 29	76	23 57 30	77	24 10 31	77	24 23 32	78	24 35 34	78	283
78	22 55 29	76	23 09 31	76	23 23 32	77	23 37 32	77	23 50 33	78	282
79	22 07 30	75	22 22 31	76	22 37 31	76	22 51 32	77	23 05 33	77	281
80	21 20+30	75	21 35+31	75	21 50+32	76	22 05+33	76	22 19+34	76	280
81	20 33 30	74	20 49 31	75	21 04 32	75	21 19 33	76	21 34 34	76	279
82	19 46 30	74	20 02 31	74	20 18 32	75	20 34 33	75	20 49 34	75	278
83	18 58 31	73	19 15 32	74	19 32 32	74	19 48 33	74	20 04 34	75	277
84	18 12 30	73	18 29 31	73	18 46 32	74	19 03 33	74	19 19 34	74	276
85	17 25+31	72	17 43+31	73	18 00+33	73	18 17+34	73	18 34+35	74	275
86	16 38 31	72	16 56 32	72	17 14 33	73	17 32 34	73	17 50 34	73	274
87	15 52 31	71	16 10 33	72	16 29 33	72	16 47 34	72	17 05 35	73	273
88	15 05 32	71	15 24 33	71	15 44 33	71	16 02 35	72	16 21 35	72	272
89	14 19 32	70	14 39 32	71	14 58 34	71	15 18 34	71	15 37 35	71	271
90	13 33+32	70	13 53+33	70	14 13+34	70	14 33+35	71	14 53+35	71	270

In South { For argument H.A. on the left, True Azimuth = $180^\circ + \text{Tabulated Azimuth.}$ } See
 Latitudes { For argument H.A. on the right, True Azimuth = $180^\circ - \text{Tabulated Azimuth.}$ } p. 91.

24°

DECLINATION **SAME** NAME AS LATITUDE

24°

LAT.	35°		36°		37°		38°		39°		LAT.
H.A.	Alt.	Az.	Alt.	Az.	Alt.	Az.	Alt.	Az.	Alt.	Az.	H.A.
°	° , d °		° , d °		° , d °		° , d °		° , d °		°
90	13 33+32	70	13 53+33	70	14 13+34	70	14 33+35	71	14 53+35	71	270
91	12 47 32	69	13 08 33	70	13 28 34	70	13 49 35	70	14 09 36	70	269
92	12 01 33	69	12 23 33	69	12 44 34	69	13 05 35	70	13 25 36	70	268
93	11 16 33	68	11 38 33	69	11 59 35	69	12 21 35	69	12 42 36	69	267
94	10 30+33	68	10 53 34	68	11 15 35	68	11 37 35	68	11 59 36	69	266
95	...		10 08+34	68	10 31+35	68	10 53+36	68	11 16+36	68	265
96	...		...		...		10 10+36	67	10 33+36	68	264
97	...		...		...		...		...		263
98	...		...		...		...		...		262
99	...		...		...		...		...		261
100	...		...		...		...		...		260

24°

DECLINATION **CONTRARY** NAME TO LATITUDE

24°

LAT.	35°		36°		37°		38°		39°		LAT.
H.A.	Alt.	Az.	Alt.	Az.	Alt.	Az.	Alt.	Az.	Alt.	Az.	H.A.
°	° , d °		° , d °		° , d °		° , d °		° , d °		°
45	17 15-47	137	16 31-48	138	15 47-49	138	15 02-49	138	14 18-49	138	315
46	16 42 47	137	15 58 47	137	15 14 48	137	14 31 49	137	13 47 49	137	314
47	16 08 47	136	15 25 47	136	14 42 48	136	13 58 48	136	13 15 49	137	313
48	15 34 47	135	14 51 47	135	14 09 48	136	13 26 48	136	12 43 48	136	312
49	14 59 46	134	14 17 47	135	13 35 47	135	12 53 48	135	12 10 47	135	311
50	14 24-46	134	13 42-46	134	13 01-47	134	12 19-47	134	11 38-48	134	310
51	13 48 45	133	13 07 45	133	12 26 46	133	11 45 46	134	11 04 47	134	309
52	13 12 45	132	12 32 45	132	11 52 46	133	11 11 46	133	10 31-47	133	308
53	12 36 45	132	11 56 45	132	11 16 45	132	10 36 45	132	...		307
54	11 59 44	131	11 20 44	131	10 41 45	131	10 01-45	131	...		306
55	11 22-44	130	10 43-44	130	10 05-45	131	...		...		305
56	10 45 44	130	10 07-44	130	...		...		...		304
57	10 07-43	129	...		...		...		...		303
58	...		...		...		...		...		302
59	...		...		...		...		...		301
60	...		...		...		...		...		300

In North { For argument H.A. on the left, True Azimuth = 360° - Tabulated Azimuth. } See
 Latitudes { For argument H.A. on the right, True Azimuth = Tabulated Azimuth. } p. 90.

LAT.	35°		36°		37°		38°		39°		LAT.
H.A.	Alt.	Az.	Alt.	Az.	Alt.	Az.	Alt.	Az.	Alt.	Az.	H.A.
0	31 01-60	180	30 01-60	180	29 01-59	180	28 02-60	180	27 02-60	180	360
1	31 01 60	179	30 01 60	179	29 01 60	179	28 01 60	179	27 01 60	179	359
2	31 00 60	178	30 00 60	178	29 00 60	178	28 00 60	178	27 00 60	178	358
3	30 57 60	177	29 57 59	177	28 58 60	177	27 58 60	177	26 58 60	177	357
4	30 54 60	176	29 54 60	176	28 54 59	176	27 55 60	176	26 55 60	176	356
5	30 50-60	175	29 50-59	175	28 51-60	175	27 51-60	175	26 51-60	175	355
6	30 45 60	174	29 45 59	174	28 46 60	174	27 46 59	174	26 47 60	174	354
7	30 39 59	173	29 40 60	173	28 40 59	173	27 41 60	173	26 41 59	173	353
8	30 32 59	172	29 33 59	172	28 34 60	172	27 34 59	172	26 35 59	172	352
9	30 25 60	170	29 25 59	171	28 26 59	171	27 27 59	171	26 28 59	171	351
10	30 16-59	169	29 17-59	170	28 18-59	170	27 19-59	170	26 20-59	170	350
11	30 07 59	168	29 08 59	168	28 09 59	169	27 10 59	169	26 12 60	169	349
12	29 56 59	167	28 58 59	167	27 59 59	168	27 01 59	168	26 02 59	168	348
13	29 45 59	166	28 47 59	166	27 48 58	167	26 50 59	167	25 52 59	167	347
14	29 33 58	165	28 35 58	165	27 37 59	166	26 39 59	166	25 41 59	166	346
15	29 20-58	164	28 22-58	164	27 25-59	165	26 27-59	165	25 29-58	165	345
16	29 06 58	163	28 09 58	163	27 11 58	164	26 14 58	164	25 16 58	164	344
17	28 52 58	162	27 55 58	162	26 58 58	163	26 00 58	163	25 03 58	163	343
18	28 36 57	161	27 40 58	161	26 43 58	162	25 46 58	162	24 49 58	162	342
19	28 20 57	160	27 24 57	160	26 27 57	161	25 31 58	161	24 34 57	161	341
20	28 03-57	159	27 07-57	159	26 11-57	160	25 15-57	160	24 19-58	160	340
21	27 45 56	158	26 50 57	158	25 54 57	159	24 58 57	159	24 02 57	159	339
22	27 27 56	157	26 32 57	158	25 36 56	158	24 41 57	158	23 45 57	158	338
23	27 08 56	156	26 13 56	157	25 18 57	157	24 23 57	157	23 27 56	157	337
24	26 48 56	155	25 53 56	156	24 58 56	156	24 04 56	156	23 09 56	156	336
25	26 27-56	154	25 33-56	155	24 38-55	155	23 44-56	155	22 50-56	155	335
26	26 05 55	154	25 12 56	154	24 18 56	154	23 24 56	154	22 30 56	154	334
27	25 43 55	153	24 50 55	153	23 56 55	153	23 03 55	153	22 09 55	153	333
28	25 20 54	152	24 27 54	152	23 34 54	152	22 41 55	152	21 48 55	152	332
29	24 56 53	151	24 04 54	151	23 12 55	151	22 19 55	151	21 26 54	152	331
30	24 32-53	150	23 40-54	150	22 48-54	150	21 56-54	151	21 04-55	151	330
31	24 07 53	149	23 16 54	149	22 24 53	149	21 33 54	150	20 41 54	150	329
32	23 42 53	148	22 51 53	148	22 00 54	149	21 08 53	149	20 17 54	149	328
33	23 15 52	147	22 25 53	147	21 34 53	148	20 44 54	148	19 53 54	148	327
34	22 48 52	146	21 58 52	147	21 08 52	147	20 18 53	147	19 28 53	147	326
35	22 21-52	146	21 31-51	146	20 42-52	146	19 52-52	146	19 02-52	146	325
36	21 53 51	145	21 04 52	145	20 15 52	145	19 26 53	145	18 36 52	146	324
37	21 24 51	144	20 36 51	144	19 47 51	144	18 59 52	144	18 10 52	145	323
38	20 55 51	143	20 07 51	143	19 19 51	143	18 31 52	144	17 43 52	144	322
39	20 25 50	142	19 38 51	142	18 50 51	143	18 03 52	143	17 15 52	143	321
40	19 55-50	141	19 08-50	142	18 21-50	142	17 34-51	142	16 47-51	142	320
41	19 24 49	141	18 38 50	141	17 51 50	141	17 05 51	141	16 18 51	141	319
42	18 52 48	140	18 07 50	140	17 21 50	140	16 35 50	140	15 49 51	141	318
43	18 20 48	139	17 35 49	139	16 50 49	139	16 04 49	140	15 19 50	140	317
44	17 48 48	138	17 03 48	138	16 19 49	139	15 34 50	139	14 49 50	139	316
45	17 15-47	137	16 31-48	138	15 47-49	138	15 02-49	138	14 18-49	138	315

In South { For argument H.A. on the left, True Azimuth = $180^\circ +$ Tabulated Azimuth. } See
 Latitudes { For argument H.A. on the right, True Azimuth = $180^\circ -$ Tabulated Azimuth. } p. 91.

LAT.	35°		36°		37°		38°		39°		LAT.
H.A.	Alt.	Az.	Alt.	Az.	Alt.	Az.	Alt.	Az.	Alt.	Az.	H.A.
0	80 00+60	180	79 00+60	180	78 00+60	180	77 00+60	180	76 00+60	180	360
1	79 58 60	175	78 58 60	175	77 58 60	176	76 59 59	176	75 59 60	176	359
2	79 51 59	170	78 52 59	171	77 53 59	171	76 54 59	172	75 54 60	173	358
3	79 40 58	165	78 42 59	166	77 44 59	167	76 45 59	168	75 47 59	169	357
4	79 25 57	160	78 29 57	162	77 32 57	163	76 34 58	164	75 36 59	165	356
5	79 07+55	155	78 12+56	157	77 16+57	159	76 20+57	160	75 23+58	162	355
6	78 44 54	151	77 51 55	153	76 57 56	155	76 03 56	157	75 07 57	158	354
7	78 19 52	147	77 28 53	149	76 36 54	152	75 43 55	153	74 49 55	155	353
8	77 51 50	143	77 02 51	146	76 12 52	148	75 20 54	150	74 28 54	152	352
9	77 20 48	140	76 34 49	142	75 45 51	145	74 56 52	147	74 05 53	149	351
10	76 47+46	136	76 03+48	139	75 17+49	142	74 29+51	144	73 40+52	146	350
11	76 13 44	134	75 30 47	136	74 46 48	139	74 00 50	141	73 13 51	143	349
12	75 36 43	131	74 56 45	134	74 14 46	136	73 30 48	138	72 44 50	141	348
13	74 58 41	128	74 20 43	131	73 40 45	134	72 57 48	136	72 14 48	138	347
14	74 19 40	126	73 43 42	129	73 04 44	131	72 24 46	134	71 42 47	136	346
15	73 39+38	124	73 04+41	126	72 28+42	129	71 49+45	131	71 09+46	133	345
16	72 57 37	122	72 25 39	124	71 50 41	127	71 13 43	129	70 34 45	131	344
17	72 15 36	120	71 44 38	122	71 11 40	125	70 36 42	127	69 59 44	129	343
18	71 32 35	118	71 03 37	120	70 31 40	123	69 58 41	125	69 22 43	127	342
19	70 48 34	116	70 20 37	119	69 50 39	121	69 18 41	123	68 45 42	126	341
20	70 04+33	115	69 38+35	117	69 09+38	119	68 39+39	122	68 06+42	124	340
21	69 19 32	113	68 54 35	116	68 27 37	118	67 58 39	120	67 27 41	122	339
22	68 33 32	112	68 10 34	114	67 44 36	116	67 17 38	118	66 47 40	121	338
23	67 48 31	110	67 25 34	113	67 01 36	115	66 35 37	117	66 07 39	119	337
24	67 01 31	109	66 41 32	111	66 18 34	114	65 53 36	116	65 26 38	118	336
25	66 15+30	108	65 55+32	110	65 33+34	112	65 10+36	114	64 44+38	116	335
26	65 28 29	107	65 09 32	109	64 49 33	111	64 26 36	113	64 02 37	115	334
27	64 41 29	106	64 23 31	108	64 04 33	110	63 43 34	112	63 20 36	114	333
28	63 53 29	105	63 37 30	107	63 19 32	109	62 59 34	111	62 37 36	112	332
29	63 06 28	104	62 51 29	106	62 33 32	108	62 14 34	109	61 53 36	111	331
30	62 18+28	103	62 04+29	105	61 48+31	107	61 30+33	108	61 10+35	110	330
31	61 30 27	102	61 17 29	104	61 01 31	106	60 45 32	107	60 26 34	109	329
32	60 42 27	101	60 29 29	103	60 15 31	105	59 59 33	106	59 42 34	108	328
33	59 54 26	100	59 42 29	102	59 29 30	104	59 14 32	105	58 57 34	107	327
34	59 05 27	100	58 55 28	101	58 42 30	103	58 28 32	104	58 12 34	106	326
35	58 17+26	99	58 07+28	100	57 55+30	102	57 42+32	103	57 27+34	105	325
36	57 28 26	98	57 19 28	99	57 08 30	101	56 56 31	103	56 42 33	104	324
37	56 39 26	97	56 31 28	98	56 21 30	100	56 10 31	102	55 57 32	103	323
38	55 51 25	96	55 43 28	98	55 34 29	99	55 24 30	101	55 12 32	102	322
39	55 02 25	96	54 55 27	97	54 47 29	99	54 37 31	100	54 26 32	101	321
40	54 13+25	95	54 07+27	96	53 59+29	98	53 50+31	99	53 40+32	101	320
41	53 24 25	94	53 19 27	96	53 12 28	97	53 04 30	98	52 54 32	100	319
42	52 35 25	94	52 30 27	95	52 24 29	96	52 17 30	98	52 08 32	99	318
43	51 46 25	93	51 42 27	94	51 37 28	96	51 30 30	97	51 22 31	98	317
44	50 57 25	93	50 54 26	94	50 49 28	95	50 43 30	96	50 36 31	97	316
45	50 08+25	92	50 05+27	93	50 01+28	94	49 56+30	95	49 50+31	97	315

In North { For argument H.A. on the left, True Azimuth = 360° - Tabulated Azimuth. } See
 Latitudes { For argument H.A. on the right, True Azimuth = Tabulated Azimuth. } p. 90.

LAT.	35°		36°		37°		38°		39°		LAT.
H.A.	Alt.	Az.	Alt.	Az.	Alt.	Az.	Alt.	Az.	Alt.	Az.	H.A.
45	50 08+25	92	50 05+27	93	50 01+28	94	49 56+30	95	49 50+31	97	315
46	49 19 25	91	49 17 26	92	49 13 29	94	49 09 30	95	49 03 31	96	314
47	48 30 25	91	48 28 27	92	48 26 28	93	48 22 29	94	48 17 31	95	313
48	47 40 26	90	47 40 26	91	47 38 28	92	47 35 29	93	47 31 30	95	312
49	46 51 25	90	46 51 27	91	46 50 28	92	46 48 29	93	46 44 31	94	311
50	46 02+25	89	46 03+26	90	46 02+28	91	46 00+30	92	45 58+30	93	310
51	45 13 25	88	45 14 27	89	45 14 28	90	45 13 29	91	45 11 31	92	309
52	44 24 25	88	44 26 26	89	44 26 28	90	44 26 29	91	44 24 31	92	308
53	43 35 25	87	43 37 27	88	43 38 28	89	43 39 29	90	43 38 30	91	307
54	42 46 25	87	42 49 26	88	42 50 28	89	42 51 30	90	42 51 31	91	306
55	41 57+25	86	42 00+27	87	42 03+28	88	42 04+29	89	42 05+30	90	305
56	41 08 25	86	41 12 27	87	41 15 28	88	41 17 29	88	41 18 31	89	304
57	40 19 25	85	40 23 27	86	40 27 28	87	40 30 29	88	40 32 30	89	303
58	39 30 26	85	39 35 27	86	39 39 28	86	39 42 30	87	39 45 30	88	302
59	38 41 26	84	38 47 27	85	38 51 29	86	38 55 30	87	38 58 31	87	301
60	37 52+26	84	37 58+27	84	38 04+28	85	38 08+30	86	38 12+30	87	300
61	37 03 26	83	37 10 27	84	37 16 28	85	37 21 30	85	37 25 31	86	299
62	36 15 26	83	36 22 27	83	36 28 29	84	36 34 30	85	36 39 31	86	298
63	35 26 26	82	35 34 27	83	35 41 28	84	35 47 30	84	35 52 31	85	297
64	34 37 27	82	34 45 28	82	34 53 29	83	35 00 30	84	35 06 31	84	296
65	33 49+26	81	33 57+28	82	34 06+28	83	34 13+30	83	34 20+31	84	295
66	33 00 27	81	33 09 28	81	33 18 29	82	33 26 30	83	33 33 31	83	294
67	32 12 27	80	32 22 28	81	32 31 29	82	32 39 30	82	32 47 31	83	293
68	31 23 27	80	31 34 28	80	31 43 30	81	31 52 31	82	32 01 31	82	292
69	30 35 27	79	30 46 28	80	30 56 30	80	31 06 30	81	31 15 31	82	291
70	29 47+27	79	29 58+29	79	30 09+30	80	30 19+31	81	30 29+31	81	290
71	28 59 27	78	29 11 28	79	29 22 30	79	29 33 30	80	29 43 31	81	289
72	28 11 28	78	28 23 29	78	28 35 30	79	28 46 31	79	28 57 32	80	288
73	27 23 28	77	27 36 29	78	27 48 30	78	28 00 31	79	28 11 32	79	287
74	26 35 28	77	26 48 29	77	27 01 30	78	27 13 32	78	27 25 32	79	286
75	25 47+29	76	26 01+29	77	26 14+31	77	26 27+32	78	26 40+32	78	285
76	24 59 29	76	25 14 29	76	25 28 30	77	25 41 32	77	25 54 32	78	284
77	24 12 29	75	24 27 30	76	24 41 31	76	24 55 32	77	25 09 32	77	283
78	23 24 29	75	23 40 30	75	23 55 31	76	24 09 32	76	24 23 33	77	282
79	22 37 29	74	22 53 30	75	23 08 31	75	23 23 32	76	23 38 33	76	281
80	21 50+29	74	22 06+31	74	22 22+31	75	22 38+32	75	22 53+33	76	280
81	21 03 29	74	21 20 30	74	21 36 32	74	21 52 33	75	22 08 33	75	279
82	20 16 30	73	20 33 31	73	20 50 32	74	21 07 32	74	21 23 33	74	278
83	19 29 30	73	19 47 31	73	20 04 32	73	20 21 33	74	20 38 34	74	277
84	18 42 31	72	19 00 32	72	19 18 33	73	19 36 33	73	19 53 34	73	276
85	17 56+30	72	18 14+32	72	18 33+32	72	18 51+33	73	19 09+34	73	275
86	17 09 31	71	17 28 32	71	17 47 33	72	18 06 34	72	18 24 35	72	274
87	16 23 31	71	16 43 32	71	17 02 33	71	17 21 34	71	17 40 35	72	273
88	15 37 31	70	15 57 32	70	16 17 33	71	16 37 34	71	16 56 35	71	272
89	14 51 31	70	15 11 33	70	15 32 33	70	15 52 34	70	16 12 35	71	271
90	14 05+32	69	14 26+33	69	14 47+34	70	15 08+34	70	15 28+36	70	270

In South { For argument H.A. on the left, True Azimuth = $180^\circ + \text{Tabulated Azimuth}$. } See
 Latitudes { For argument H.A. on the right, True Azimuth = $180^\circ - \text{Tabulated Azimuth}$. } p. 91.

25°

DECLINATION **SAME** NAME AS LATITUDE

25°

LAT.	35°		36°		37°		38°		39°		LAT.
H.A.	Alt.	Az.	Alt.	Az.	Alt.	Az.	Alt.	Az.	Alt.	Az.	H.A.
°	°	d	°	d	°	d	°	d	°	d	°
90	14 05+32	69	14 26+33	69	14 47+34	70	15 08+34	70	15 28+36	70	270
91	13 19 32	69	13 41 33	69	14 02 34	69	14 24 34	69	14 45 35	70	269
92	12 34 32	68	12 56 33	68	13 18 34	69	13 40 35	69	14 01 36	69	268
93	11 49 32	68	12 11 34	68	12 34 34	68	12 56 35	68	13 18 36	68	267
94	11 03 33	67	11 27 33	67	11 50 34	67	12 12 36	68	12 35 36	68	266
95	10 19+33	67	10 42+34	67	11 06+35	67	11 29+36	67	11 52+37	67	265
96	...		...		10 22+35	66	10 46 36	67	11 09 37	67	264
97	...		...		...		10 03+36	66	10 27+37	66	263
98	...		...		...		...		...		262
99	...		...		...		...		...		261
100	...		...		...		...		...		260

25°

DECLINATION **CONTRARY** NAME TO LATITUDE

25°

LAT.	35°		36°		37°		38°		39°		LAT.
H.A.	Alt.	Az.	Alt.	Az.	Alt.	Az.	Alt.	Az.	Alt.	Az.	H.A.
°	°	d	°	d	°	d	°	d	°	d	°
45	16 28-48	138	15 43-48	138	14 58-48	138	14 13-48	139	13 29-50	139	315
46	15 55 48	137	15 11 48	138	14 26 48	138	13 42 48	138	12 58 49	138	314
47	15 21 47	137	14 38 48	137	13 54 48	137	13 10 48	137	12 26 48	137	313
48	14 47 46	136	14 04 47	136	13 21 47	136	12 38 48	136	11 55 48	137	312
49	14 13 46	135	13 30 46	135	12 48 47	135	12 05 47	136	11 23 48	136	311
50	13 38-46	134	12 56-46	135	12 14-46	135	11 32-47	135	10 50-47	135	310
51	13 03 45	134	12 22 46	134	11 40 46	134	10 59 47	134	10 17-47	134	309
52	12 27 44	133	11 47 46	133	11 06 46	133	10 25-46	133	...		308
53	11 51 44	132	11 11 45	132	10 31-45	133	...		...		307
54	11 15 44	132	10 36-45	132	...		...		...		306
55	10 38-43	131	...		...		...		...		305
56	10 01-43	130	...		...		...		...		304
57	...		...		...		...		...		303
58	...		...		...		...		...		302
59	...		...		...		...		...		301
60	...		...		...		...		...		300

In North { For argument H.A. on the left, True Azimuth = $360^\circ - \text{Tabulated Azimuth}$. } See
 Latitudes { For argument H.A. on the right, True Azimuth = Tabulated Azimuth. } p. 90.

LAT.	35°		36°		37°		38°		39°		LAT.
H.A.	Alt.	Az.	Alt.	Az.	Alt.	Az.	Alt.	Az.	Alt.	Az.	H.A.
0	30 01-60	180	29 01-59	180	28 02-60	180	27 02-60	180	26 02-60	180	360
1	30 01 60	179	29 01 60	179	28 01 60	179	27 01 60	179	26 01 60	179	359
2	30 00 60	178	29 00 60	178	28 00 60	178	27 00 60	178	26 00 60	178	358
3	29 57 59	177	28 58 60	177	27 58 60	177	26 58 60	177	25 58 60	177	357
4	29 54 60	176	28 54 59	176	27 55 60	176	26 55 60	176	25 55 60	176	356
5	29 50-60	175	28 51-60	175	27 51-60	175	26 51-60	175	25 51-59	175	355
6	29 45 59	174	28 46 60	174	27 46 60	174	26 47 60	174	25 47 60	174	354
7	29 40 60	173	28 40 60	173	27 41 60	173	26 41 59	173	25 42 60	173	353
8	29 33 60	172	28 34 60	172	27 34 59	172	26 35 60	172	25 36 60	172	352
9	29 25 59	171	28 26 59	171	27 27 59	171	26 28 60	171	25 29 60	171	351
10	29 17-59	170	28 18-59	170	27 19-59	170	26 20-59	170	25 21-59	170	350
11	29 08 59	169	28 09 59	169	27 10 59	169	26 11 59	169	25 12 59	169	349
12	28 57 58	168	27 59 59	168	27 00 59	168	26 02 59	168	25 03 59	168	348
13	28 46 58	167	27 48 59	167	26 50 59	167	25 51 58	167	24 53 59	167	347
14	28 35 59	166	27 37 59	166	26 38 58	166	25 40 58	166	24 42 58	166	346
15	28 22-58	165	27 24-58	165	26 26-58	165	25 28-58	165	24 31-59	165	345
16	28 08 58	164	27 11 58	164	26 13 58	164	25 16 58	164	24 18 58	164	344
17	27 54 58	163	26 57 58	163	26 00 58	163	25 02 58	163	24 05 58	163	343
18	27 39 57	162	26 42 57	162	25 45 57	162	24 48 58	162	23 51 58	162	342
19	27 23 57	161	26 27 58	161	25 30 57	161	24 33 57	161	23 37 58	161	341
20	27 06-57	160	26 10-57	160	25 14-57	160	24 18-58	160	23 21-57	160	340
21	26 49 57	159	25 53 57	159	24 57 57	159	24 01 57	159	23 05 57	159	339
22	26 31 57	158	25 35 56	158	24 40 57	158	23 44 57	158	22 48 57	158	338
23	26 12 56	157	25 17 57	157	24 21 56	157	23 26 56	157	22 31 57	157	337
24	25 52 56	156	24 57 56	156	24 02 56	156	23 08 57	156	22 13 57	157	336
25	25 31-55	155	24 37-55	155	23 43-56	155	22 48-56	155	21 54-56	156	335
26	25 10 55	154	24 16 55	154	23 22 55	154	22 28 55	155	21 34 56	155	334
27	24 48 54	153	23 55 55	153	23 01 55	153	22 08 56	154	21 14 55	154	333
28	24 26 55	152	23 33 55	152	22 40 55	153	21 46 55	153	20 53 55	153	332
29	24 03 54	151	23 10 54	151	22 17 54	152	21 24 54	152	20 32 55	152	331
30	23 39-54	150	22 46-53	151	21 54-54	151	21 02-54	151	20 09-54	151	330
31	23 14 53	149	22 22 53	150	21 31 54	150	20 39 54	150	19 47 54	150	329
32	22 49 53	149	21 58 54	149	21 06 53	149	20 15 54	149	19 23 54	149	328
33	22 23 53	148	21 32 53	148	20 41 53	148	19 50 53	148	18 59 53	149	327
34	21 56 52	147	21 06 52	147	20 16 53	147	19 25 53	148	18 35 53	148	326
35	21 29-52	146	20 40-53	146	19 50-53	146	19 00-53	147	18 10-53	147	325
36	21 02 52	145	20 12 51	145	19 23 52	146	18 33 52	146	17 44 53	146	324
37	20 33 51	144	19 45 52	145	18 56 52	145	18 07 52	145	17 18 53	145	323
38	20 04 50	144	19 16 51	144	18 28 51	144	17 39 51	144	16 51 52	144	322
39	19 35 50	143	18 47 50	143	17 59 50	143	17 11 51	143	16 23 51	144	321
40	19 05-50	142	18 18-50	142	17 31-51	142	16 43-51	143	15 56-52	143	320
41	18 35 50	141	17 48 50	141	17 01 50	142	16 14 50	142	15 27 51	142	319
42	18 04 49	140	17 17 49	141	16 31 50	141	15 45 50	141	14 58 50	141	318
43	17 32 49	140	16 46 49	140	16 01 50	140	15 15 50	140	14 29 50	140	317
44	17 00 48	139	16 15 49	139	15 30 49	139	14 44 49	139	13 59 50	140	316
45	16 28-48	138	15 43-48	138	14 58-48	138	14 13-48	139	13 29-50	139	315

In South { For argument H.A. on the left, True Azimuth = $180^\circ +$ Tabulated Azimuth. } See
 Latitudes { For argument H.A. on the right, True Azimuth = $180^\circ -$ Tabulated Azimuth. } p. 91.

26°

DECLINATION SAME NAME AS LATITUDE

26°

LAT.	35°		36°		37°		38°		39°		LAT.
H.A.	Alt.	Az.	Alt.	Az.	Alt.	Az.	Alt.	Az.	Alt.	Az.	H.A.
0	...	...	80 00+60	180	79 00+60	180	78 00+60	180	77 00+60	180	360
1	...	...	79 58 60	175	78 58 60	175	77 58 60	176	76 59 59	176	359
2	...	...	79 51 60	170	78 52 60	171	77 53 60	171	76 54 59	172	358
3	...	...	79 41 58	165	78 43 58	166	77 44 59	167	76 46 59	168	357
4	...	...	79 26 57	160	78 29 58	162	77 32 58	163	76 35 58	164	356
5	...	...	79 08+55	155	78 13+56	157	77 17+57	159	76 21+57	161	355
6	79 38+52	149	78 46 53	151	77 53 54	153	76 59 55	155	76 04 56	157	354
7	79 11 50	144	78 21 52	147	77 30 53	150	76 38 54	152	75 44 55	154	353
8	78 41 47	140	77 53 50	143	77 04 52	146	76 14 53	148	75 22 54	150	352
9	78 08 46	137	77 23 48	140	76 36 50	143	75 48 51	145	74 58 53	147	351
10	77 33+44	134	76 51+46	137	76 06+49	139	75 20+50	142	74 32+51	144	350
11	76 57 42	131	76 17 44	134	75 34 47	137	74 50 48	139	74 04 50	141	349
12	76 19 40	128	75 41 43	131	75 00 46	134	74 18 47	136	73 34 48	139	348
13	75 39 39	125	75 03 42	128	74 25 44	131	73 45 45	134	73 02 48	136	347
14	74 59 37	123	74 25 40	126	73 48 43	129	73 10 44	131	72 29 46	134	346
15	74 17+36	121	73 45+39	124	73 10+42	127	72 34+43	129	71 55+45	131	345
16	73 34 35	119	73 04 38	122	72 31 40	124	71 56 42	127	71 19 44	129	344
17	72 51 34	117	72 22 37	120	71 51 39	122	71 18 41	125	70 43 43	127	343
18	72 07 33	115	71 40 35	118	71 11 37	121	70 39 40	123	70 05 42	125	342
19	71 22 32	114	70 57 34	116	70 29 37	119	69 59 39	121	69 27 41	124	341
20	70 37+31	112	70 13+34	115	69 47+36	117	69 18+38	120	68 48+40	122	340
21	69 51 31	111	69 29 32	113	69 04 35	116	68 37 37	118	68 08 39	120	339
22	69 05 30	109	68 44 32	112	68 20 35	114	67 55 36	116	67 27 38	119	338
23	68 19 29	108	67 59 31	111	67 37 33	113	67 12 36	115	66 46 37	117	337
24	67 32 28	107	67 13 31	109	66 52 33	112	66 29 35	114	66 04 37	116	336
25	66 45+28	106	66 27+30	108	66 07+33	110	65 46+34	112	65 22+36	114	335
26	65 57 28	105	65 41 29	107	65 22 32	109	65 02 33	111	64 39 36	113	334
27	65 10 27	104	64 54 29	106	64 37 31	108	64 17 34	110	63 56 35	112	333
28	64 22 26	103	64 07 29	105	63 51 31	107	63 33 32	109	63 13 34	111	332
29	63 34 26	102	63 20 29	104	63 05 30	106	62 48 32	108	62 29 34	109	331
30	62 46+26	101	62 33+28	103	62 19+30	105	62 03+32	107	61 45+33	108	330
31	61 57 26	100	61 46 28	102	61 32 30	104	61 17 32	106	61 00 34	107	329
32	61 09 25	99	60 58 28	101	60 46 29	103	60 32 31	105	60 16 33	106	328
33	60 20 26	99	60 11 27	100	59 59 29	102	59 46 31	104	59 31 32	105	327
34	59 32 25	98	59 23 27	99	59 12 29	101	59 00 30	103	58 46 32	104	326
35	58 43+25	97	58 35+27	99	58 25+29	100	58 14+30	102	58 01+31	103	325
36	57 54 25	96	57 47 26	98	57 38 28	99	57 27 30	101	57 15 32	102	324
37	57 05 25	96	56 59 26	97	56 51 28	99	56 41 29	100	56 29 32	102	323
38	56 16 25	95	56 11 26	96	56 03 28	98	55 54 30	99	55 44 31	101	322
39	55 27 25	94	55 22 26	96	55 16 27	97	55 08 29	98	54 58 31	100	321
40	54 38+25	94	54 34+26	95	54 28+28	96	54 21+29	98	54 12+31	99	320
41	53 49 25	93	53 46 25	94	53 40 28	96	53 34 29	97	53 26 30	98	319
42	53 00 24	92	52 57 26	94	52 53 27	95	52 47 29	96	52 40 30	98	318
43	52 11 24	92	52 09 25	93	52 05 27	94	52 00 29	96	51 53 31	97	317
44	51 22 24	91	51 20 26	92	51 17 27	94	51 13 28	95	51 07 30	96	316
45	50 33+24	90	50 32+25	92	50 29+28	93	50 26+28	94	50 21+30	95	315

In North { For argument H.A. on the left, True Azimuth = $360^\circ - \text{Tabulated Azimuth}$. } See
 Latitudes { For argument H.A. on the right, True Azimuth = Tabulated Azimuth. } p. 90.

26°

DECLINATION SAME NAME AS LATITUDE

26°

LAT.	35°		36°		37°		38°		39°		LAT.
H.A.	Alt.	Az.	Alt.	Az.	Alt.	Az.	Alt.	Az.	Alt.	Az.	H.A.
45	50 33+24	90	50 32+25	92	50 29+28	93	50 26+28	94	50 21+30	95	315
46	49 44 24	90	49 43 26	91	49 42 27	92	49 39 28	93	49 34 30	95	314
47	48 55 24	89	48 55 25	90	48 54 27	92	48 51 29	93	48 48 30	94	313
48	48 06 24	89	48 06 26	90	48 06 27	91	48 04 29	92	48 01 30	93	312
49	47 16 25	88	47 18 25	89	47 18 27	90	47 17 28	91	47 15 30	93	311
50	46 27+25	88	46 29+26	89	46 30+27	90	46 30+28	91	46 28+30	92	310
51	45 38 25	87	45 41 25	88	45 42 27	89	45 42 29	90	45 42 29	91	309
52	44 49 25	87	44 52 26	88	44 54 27	89	44 55 29	90	44 55 30	91	308
53	44 00 25	86	44 04 26	87	44 06 27	88	44 08 28	89	44 08 30	90	307
54	43 11 25	86	43 15 26	87	43 18 28	87	43 21 28	88	43 22 30	89	306
55	42 22+25	85	42 27+26	86	42 31+27	87	42 33+29	88	42 35+30	89	305
56	41 33 25	85	41 39 26	85	41 43 27	86	41 46 29	87	41 49 29	88	304
57	40 44 25	84	40 50 26	85	40 55 27	86	40 59 29	87	41 02 30	88	303
58	39 56 25	84	40 02 26	84	40 07 28	85	40 12 29	86	40 15 30	87	302
59	39 07 25	83	39 14 26	84	39 20 27	85	39 25 29	86	39 29 30	86	301
60	38 18+25	83	38 25+27	83	38 32+28	84	38 38+29	85	38 42+31	86	300
61	37 29 26	82	37 37 27	83	37 44 28	84	37 51 29	84	37 56 30	85	299
62	36 41 25	82	36 49 27	82	36 57 28	83	37 04 29	84	37 10 30	85	298
63	35 52 26	81	36 01 27	82	36 09 28	83	36 17 29	83	36 23 31	84	297
64	35 04 26	81	35 13 27	81	35 22 28	82	35 30 29	83	35 37 30	83	296
65	34 15+26	80	34 25+27	81	34 34+29	82	34 43+29	82	34 51+30	83	295
66	33 27 26	80	33 37 28	80	33 47 29	81	33 56 30	82	34 04 31	82	294
67	32 39 26	79	32 50 27	80	33 00 28	80	33 09 30	81	33 18 31	82	293
68	31 50 27	79	32 02 28	79	32 13 28	80	32 23 30	81	32 32 31	81	292
69	31 02 27	78	31 14 28	79	31 26 28	79	31 36 30	80	31 46 31	81	291
70	30 14+27	78	30 27+28	78	30 39+29	79	30 50+30	80	31 00+31	80	290
71	29 26 28	77	29 39 28	78	29 52 29	78	30 03 31	79	30 14 32	80	289
72	28 39 27	77	28 52 28	77	29 05 29	78	29 17 30	78	29 29 31	79	288
73	27 51 27	76	28 05 28	77	28 18 30	77	28 31 30	78	28 43 32	78	287
74	27 03 28	76	27 17 29	76	27 31 30	77	27 45 30	77	27 57 32	78	286
75	26 16+28	75	26 30+29	76	26 45+30	76	26 59+31	77	27 12+32	77	285
76	25 28 28	75	25 43 30	75	25 58 30	76	26 13 31	76	26 26 33	77	284
77	24 41 28	74	24 57 29	75	25 12 30	75	25 27 31	76	25 41 33	76	283
78	23 53 29	74	24 10 29	74	24 26 30	75	24 41 32	75	24 56 33	76	282
79	23 06 29	74	23 23 30	74	23 39 31	74	23 55 32	75	24 11 33	75	281
80	22 19+30	73	22 37+30	73	22 53+32	74	23 10+32	74	23 26+33	75	280
81	21 32 30	73	21 50 31	73	22 08 31	73	22 25 32	74	22 41 33	74	279
82	20 46 29	72	21 04 31	72	21 22 31	73	21 39 33	73	21 56 34	74	278
83	19 59 30	72	20 18 31	72	20 36 32	72	20 54 33	73	21 12 33	73	277
84	19 13 30	71	19 32 31	71	19 51 32	72	20 09 33	72	20 27 34	73	276
85	18 26+31	71	18 46+31	71	19 05+33	71	19 24+33	72	19 43+34	72	275
86	17 40 31	70	18 00 32	70	18 20 33	71	18 40 33	71	18 59 34	71	274
87	16 54 31	70	17 15 31	70	17 35 33	70	17 55 34	71	18 15 34	71	273
88	16 08 31	69	16 29 32	69	16 50 33	70	17 11 33	70	17 31 35	70	272
89	15 22 32	69	15 44 32	69	16 05 34	69	16 26 34	70	16 47 35	70	271
90	14 37+32	68	14 59+33	68	15 21+33	69	15 42+35	69	16 04+35	69	270

In South { For argument H.A. on the left, True Azimuth = 180° + Tabulated Azimuth. } See Latitudes { For argument H.A. on the right, True Azimuth = 180° - Tabulated Azimuth. } p. 91.

26°

DECLINATION **SAME** NAME AS LATITUDE

26°

LAT.	35°		36°		37°		38°		39°		LAT.
H.A.	Alt.	Az.	Alt.	Az.	Alt.	Az.	Alt.	Az.	Alt.	Az.	H.A.
°	° , d	°	° , d	°	° , d	°	° , d	°	° , d	°	°
90	14 37+32	68	14 59+33	68	15 21+33	69	15 42+35	69	16 04+35	69	270
91	13 51 33	68	14 14 33	68	14 36 34	68	14 58 35	68	15 20 36	69	269
92	13 06 33	67	13 29 33	67	13 52 34	68	14 15 34	68	14 37 36	68	268
93	12 21 33	67	12 45 33	67	13 08 34	67	13 31 35	67	13 54 36	68	267
94	11 36 33	66	12 00 34	66	12 24 35	67	12 48 35	67	13 11 36	67	266
95	10 52+33	66	11 16+34	66	11 41+34	66	12 05+35	66	12 29+36	66	265
96	10 07+34	65	10 32+35	65	10 57 35	66	11 22 36	66	11 46 37	66	264
97	...		...		10 14+35	65	10 39+36	65	11 04 37	65	263
98	...		...		...		...		10 22+37	65	262
99	...		...		...		...		...		261
100	...		...		...		...		...		260

26°

DECLINATION **CONTRARY** NAME TO LATITUDE

26°

LAT.	35°		36°		37°		38°		39°		LAT.
H.A.	Alt.	Az.	Alt.	Az.	Alt.	Az.	Alt.	Az.	Alt.	Az.	H.A.
°	° , d	°	° , d	°	° , d	°	° , d	°	° , d	°	°
45	15 40-48	139	14 55-48	139	14 10-49	139	13 25-49	139	12 39-49	139	315
46	15 07 47	138	14 23 48	138	13 38 48	138	12 54 49	138	12 09 49	139	314
47	14 34 47	137	13 50 47	137	13 06 48	138	12 22 48	138	11 38 49	138	313
48	14 01 47	137	13 17 47	137	12 34 48	137	11 50 48	137	11 07 49	137	312
49	13 27 46	136	12 44 47	136	12 01 47	136	11 18 47	136	10 35 48	136	311
50	12 52-45	135	12 10-46	135	11 28-47	135	10 45-47	136	10 03-48	136	310
51	12 18 46	134	11 36 46	135	10 54 46	135	10 12-46	135	...		309
52	11 43 45	134	11 01 45	134	10 20-46	134	...		...		308
53	11 07 44	133	10 26-45	133	...		...		...		307
54	10 31-44	132	...		...		...		...		306
55	...		...		...		...		...		305

In North { For argument H.A. on the left, True Azimuth = $360^\circ - \text{Tabulated Azimuth}$. } See
 Latitudes { For argument H.A. on the right, True Azimuth = Tabulated Azimuth. } p. 90.

26° DECLINATION CONTRARY NAME TO LATITUDE 26°

LAT.	35°		36°		37°		38°		39°		LAT.
H.A.	Alt.	Az.	Alt.	Az.	Alt.	Az.	Alt.	Az.	Alt.	Az.	H.A.
0	29 01-59	180	28 02-60	180	27 02-60	180	26 02-60	180	25 02-60	180	360
1	29 01 60	179	28 01 60	179	27 01 60	179	26 01 60	179	25 01 60	179	359
2	29 00 60	178	28 00 60	178	27 00 60	178	26 00 60	178	25 00 60	178	358
3	28 58 60	177	27 58 60	177	26 58 60	177	25 58 60	177	24 58 60	177	357
4	28 54 59	176	27 55 60	176	26 55 60	176	25 55 60	176	24 55 60	176	356
5	28 50-59	175	27 51-60	175	26 51-60	175	25 51-59	175	24 52-60	175	355
6	28 46 60	174	27 46 60	174	26 46 59	174	25 47 60	174	24 47 59	174	354
7	28 40 60	173	27 40 59	173	26 41 60	173	25 42 60	173	24 42 60	173	353
8	28 33 59	172	27 34 59	172	26 35 60	172	25 35 59	172	24 36 59	172	352
9	28 26 59	171	27 27 60	171	26 28 60	171	25 28 59	171	24 29 59	171	351
10	28 18-59	170	27 19-59	170	26 20-60	170	25 21-60	170	24 22-60	170	350
11	28 09 59	169	27 10 59	169	26 11 59	169	25 12 59	169	24 13 59	169	349
12	27 59 59	168	27 00 59	168	26 01 58	168	25 03 59	168	24 04 59	168	348
13	27 48 59	167	26 49 58	167	25 51 59	167	24 53 59	167	23 54 59	167	347
14	27 36 58	166	26 38 58	166	25 40 59	166	24 42 59	166	23 44 59	166	346
15	27 24-58	165	26 26-58	165	25 28-58	165	24 30-58	165	23 32-58	165	345
16	27 10 58	164	26 13 58	164	25 15 58	164	24 18 59	164	23 20 58	164	344
17	26 56 57	163	25 59 58	163	25 02 58	163	24 04 58	163	23 07 58	163	343
18	26 42 58	162	25 45 58	162	24 48 58	162	23 50 57	162	22 53 58	162	342
19	26 26 57	161	25 29 57	161	24 33 58	161	23 36 58	161	22 39 58	162	341
20	26 09-57	160	25 13-57	160	24 17-57	160	23 20-57	160	22 24-58	161	340
21	25 52 56	159	24 56 57	159	24 00 57	159	23 04 57	160	22 08 57	160	339
22	25 34 56	158	24 39 57	158	23 43 57	158	22 47 57	159	21 51 56	159	338
23	25 16 56	157	24 20 56	157	23 25 56	158	22 30 57	158	21 34 56	158	337
24	24 56 56	156	24 01 56	156	23 06 56	157	22 11 56	157	21 16 56	157	336
25	24 36-55	155	23 42-56	156	22 47-56	156	21 52-56	156	20 58-56	156	335
26	24 15 55	154	23 21 55	155	22 27 55	155	21 33 56	155	20 38 55	155	334
27	23 54 55	154	23 00 55	154	22 06 55	154	21 12 55	154	20 19 55	154	333
28	23 31 54	153	22 38 54	153	21 45 55	153	20 51 55	153	19 58 55	153	332
29	23 09 55	152	22 16 55	152	21 23 55	152	20 30 55	152	19 37 55	152	331
30	22 45-54	151	21 53-54	151	21 00-54	151	20 08-55	151	19 15-55	152	330
31	22 21 54	150	21 29 54	150	20 37 54	150	19 45 54	151	18 53 55	151	329
32	21 56 53	149	21 04 53	149	20 13 54	150	19 21 54	150	18 29 54	150	328
33	21 30 52	148	20 39 53	148	19 48 53	149	18 57 53	149	18 06 54	149	327
34	21 04 52	147	20 14 53	148	19 23 53	148	18 32 53	148	17 42 54	148	326
35	20 37-51	147	19 47-52	147	18 57-52	147	18 07-53	147	17 17-53	147	325
36	20 10 51	146	19 21 52	146	18 31 52	146	17 41 52	146	16 51 52	146	324
37	19 42 51	145	18 53 51	145	18 04 52	145	17 15 52	146	16 25 52	146	323
38	19 14 51	144	18 25 51	144	17 37 52	145	16 48 52	145	15 59 52	145	322
39	18 45 50	143	17 57 51	144	17 09 51	144	16 20 51	144	15 32 52	144	321
40	18 15-50	143	17 28-51	143	16 40-51	143	15 52-51	143	15 04-51	143	320
41	17 45 49	142	16 58 50	142	16 11 50	142	15 24 51	142	14 36 51	142	319
42	17 15 49	141	16 28 49	141	15 41 49	141	14 55 51	142	14 08 51	142	318
43	16 43 48	140	15 57 49	140	15 11 49	141	14 25 50	141	13 39 50	141	317
44	16 12 48	139	15 26 48	140	14 41 49	140	13 55 49	140	13 09 50	140	316
45	15 40-48	139	14 55-48	139	14 10-49	139	13 25-49	139	12 39-49	139	315

In South { For argument H.A. on the left, True Azimuth = $180^\circ +$ Tabulated Azimuth. } See
 Latitudes { For argument H.A. on the right, True Azimuth = $180^\circ -$ Tabulated Azimuth. } p. 91.

LAT.	35°		36°		37°		38°		39°		LAT.
H.A.	Alt.	Az.	Alt.	Az.	Alt.	Az.	Alt.	Az.	Alt.	Az.	H.A.
0	° , d	°	° , d	°	° , d	°	° , d	°	° , d	°	360
1	...		...		80 00+60 180		79 00+60 180		78 00+60 180		359
2	...		...		79 58 60 175		78 58 60 175		77 58 60 176		358
3	...		...		79 52 59 170		78 53 59 171		77 53 60 171		357
4	...		...		79 41 58 165		78 43 59 166		77 45 58 167		356
5	...		...		79 27 57 160		78 30 57 162		77 33 58 163		355
6	...		...		79 09+55 156		78 14+56 158		77 18+57 159		354
7	...		79 39+53 149		78 47 54 151		77 54 55 154		77 00 56 156		353
8	79 28+46 137		79 13 50 145		78 23 52 147		77 32 53 150		76 39 55 152		352
9	78 54 43 134		78 43 48 141		77 56 50 144		77 07 51 146		76 16 53 149		351
10	78 17+42 130		78 11 46 137		77 26 49 140		76 39 50 143		75 51 51 145		350
11	77 39 40 127		77 37+44 134		76 55+46 137		76 10+48 140		75 23+50 142		349
12	76 59 38 125		77 01 43 131		76 21 45 134		75 38 47 137		74 54 48 139		348
13	76 18 37 122		76 24 41 128		75 46 43 131		75 05 45 134		74 22 48 137		347
14	75 36 35 120		75 45 39 126		75 09 42 129		74 30 44 131		73 50 46 134		346
15	74 53+34 118		75 05 38 123		74 31 40 126		73 54 43 129		73 15 45 132		345
16	74 09 33 116		74 24+36 121		73 52+39 124		73 17+41 127		72 40+43 129		344
17	73 25 31 114		73 42 35 119		73 11 38 122		72 38 41 125		72 03 43 127		343
18	72 40 30 113		72 59 34 117		72 30 37 120		71 59 39 123		71 26 41 125		342
19	71 54 30 111		72 15 34 115		71 48 36 118		71 19 38 121		70 47 40 123		341
20	71 08+29 110		71 31 33 114		71 06 35 116		70 38 37 119		70 08 39 121		340
21	70 22 28 108		70 47+31 112		70 23+34 115		69 56+36 117		69 28+38 120		339
22	69 35 27 107		70 01 31 111		69 39 33 113		69 14 35 116		68 47 37 118		338
23	68 48 26 106		69 16 30 110		68 55 32 112		68 31 35 114		68 05 37 117		337
24	68 00 27 105		68 30 29 108		68 10 32 111		67 48 34 113		67 23 36 115		336
25	67 13+25 104		67 44 29 107		67 25 31 109		67 04 33 112		66 41 35 114		335
26	66 25 25 103		66 57+29 106		66 40+30 108		66 20+33 110		65 58+35 112		334
27	65 37 25 102		66 10 28 105		65 54 30 107		65 35 33 109		65 15 34 111		333
28	64 48 25 101		65 23 28 104		65 08 30 106		64 51 31 108		64 31 34 110		332
29	64 00 25 100		64 36 27 103		64 22 29 105		64 05 32 107		63 47 33 109		331
30	63 12+24 99		63 49 26 102		63 35 29 104		63 20 31 106		63 03 32 108		330
31	62 23 24 98		63 01+27 101		62 49+28 103		62 35+30 105		62 18+33 107		329
32	61 34 24 97		62 14 26 100		62 02 28 102		61 49 30 104		61 34 31 106		328
33	60 46 23 97		61 26 26 99		61 15 28 101		61 03 29 103		60 49 31 105		327
34	59 57 23 96		60 38 25 98		60 28 28 100		60 17 29 102		60 03 31 104		326
35	59 08+23 95		59 50 25 98		59 41 27 99		59 30 29 101		59 18 31 103		325
36	58 19 23 95		59 02+25 97		58 54+27 99		58 44+29 100		58 32+31 102		324
37	57 30 23 94		58 13 25 96		58 06 27 98		57 57 29 99		57 47 30 101		323
38	56 41 23 93		57 25 25 95		57 19 26 97		57 10 29 99		57 01 30 100		322
39	55 52 23 93		56 37 25 95		56 31 27 96		56 24 28 98		56 15 30 99		321
40	55 03+23 92		55 48 25 94		55 43 27 96		55 37 28 97		55 29 30 98		320
41	54 14 23 91		55 00+25 93		54 56+26 95		54 50+28 96		54 43+29 98		319
42	53 24 23 91		54 11 25 93		54 08 26 94		54 03 28 95		53 56 30 97		318
43	52 35 23 90		53 23 25 92		53 20 26 93		53 16 28 95		53 10 29 96		317
44	51 46 23 90		52 34 25 91		52 32 26 93		52 29 27 94		52 24 29 95		316
45	50 57+23 89		51 46 25 91		51 44 27 92		51 41 28 93		51 37 29 95		315
46	50 07+23 88		50 57+25 90		50 57+26 92		50 54+28 93		50 51+29 94		314

In North { For argument H.A. on the left, True Azimuth = $360^\circ - \text{Tabulated Azimuth}$. } See
 Latitudes { For argument H.A. on the right, True Azimuth = Tabulated Azimuth. } p. 90.

27°

DECLINATION SAME NAME AS LATITUDE

27°

LAT.	35°		36°		37°		38°		39°		LAT.
H.A.	Alt.	Az.	Alt.	Az.	Alt.	Az.	Alt.	Az.	Alt.	Az.	H.A.
45	50 57+23	89	50 57+25	90	50 57+26	92	50 54+28	93	50 51+29	94	315
46	50 08 23	88	50 09 25	90	50 09 26	91	50 07 28	92	50 04 29	93	314
47	49 19 23	88	49 20 25	89	49 21 26	90	49 20 27	91	49 18 29	93	313
48	48 30 23	87	48 32 25	89	48 33 26	90	48 33 27	91	48 31 29	92	312
49	47 41 23	87	47 43 25	88	47 45 26	89	47 45 28	90	47 45 28	91	311
50	46 52+23	86	46 55+25	87	46 57+26	88	46 58+28	90	46 58+29	91	310
51	46 03 23	86	46 06 25	87	46 09 26	88	46 11 27	89	46 11 29	90	309
52	45 14 23	85	45 18 25	86	45 21 27	87	45 24 27	88	45 25 29	89	308
53	44 25 23	85	44 30 25	86	44 33 27	87	44 36 28	88	44 38 29	89	307
54	43 36 24	84	43 41 25	85	43 46 26	86	43 49 28	87	43 52 29	88	306
55	42 47+24	84	42 53+25	85	42 58+26	86	43 02+28	87	43 05+29	88	305
56	41 58 24	83	42 05 25	84	42 10 27	85	42 15 28	86	42 18 30	87	304
57	41 09 25	83	41 16 26	84	41 22 27	85	41 28 28	85	41 32 29	86	303
58	40 21 24	82	40 28 26	83	40 35 27	84	40 41 28	85	40 45 30	86	302
59	39 32 24	82	39 40 26	83	39 47 27	84	39 54 28	84	39 59 29	85	301
60	38 43+25	81	38 52+26	82	39 00+27	83	39 07+28	84	39 13+29	85	300
61	37 55 25	81	38 04 26	82	38 12 27	82	38 20 28	83	38 26 30	84	299
62	37 06 25	80	37 16 26	81	37 25 27	82	37 33 28	83	37 40 29	84	298
63	36 18 25	80	36 28 26	81	36 37 28	81	36 46 28	82	36 54 29	83	297
64	35 30 25	80	35 40 27	80	35 50 28	81	35 59 29	82	36 07 30	82	296
65	34 41+26	79	34 52+27	80	35 03+27	80	35 12+29	81	35 21+30	82	295
66	33 53 26	79	34 05 27	79	34 16 27	80	34 26 29	81	34 35 30	81	294
67	33 05 26	78	33 17 27	79	33 28 29	79	33 39 29	80	33 49 30	81	293
68	32 17 26	78	32 30 27	78	32 41 29	79	32 53 29	80	33 03 31	80	292
69	31 29 26	77	31 42 27	78	31 54 29	78	32 06 30	79	32 17 31	80	291
70	30 41+27	77	30 55+27	77	31 08+28	78	31 20+30	79	31 31+31	79	290
71	29 54 26	76	30 07 28	77	30 21 29	77	30 34 29	78	30 46 31	79	289
72	29 06 27	76	29 20 28	76	29 34 29	77	29 47 30	77	30 00 31	78	288
73	28 18 28	75	28 33 28	76	28 48 29	76	29 01 31	77	29 15 31	78	287
74	27 31 27	75	27 46 29	75	28 01 29	76	28 15 31	76	28 29 32	77	286
75	26 44+27	74	26 59+29	75	27 15+29	75	27 30+30	76	27 44+31	76	285
76	25 56 28	74	26 13 28	74	26 28 30	75	26 44 31	75	26 59 31	76	284
77	25 09 28	74	25 26 29	74	25 42 30	74	25 58 31	75	26 14 31	75	283
78	24 22 29	73	24 39 30	73	24 56 31	74	25 13 31	74	25 29 32	75	282
79	23 35 29	73	23 53 30	73	24 10 31	73	24 27 32	74	24 44 32	74	281
80	22 49+28	72	23 07+30	73	23 25+30	73	23 42+32	73	23 59+32	74	280
81	22 02 29	72	22 21 30	72	22 39 31	72	22 57 32	73	23 14 33	73	279
82	21 15 30	71	21 35 30	72	21 53 31	72	22 12 32	72	22 30 33	73	278
83	20 29 30	71	20 49 30	71	21 08 31	71	21 27 32	72	21 45 34	72	277
84	19 43 30	70	20 03 31	71	20 23 31	71	20 42 33	71	21 01 34	72	276
85	18 57+30	70	19 17+31	70	19 38+31	70	19 57+33	71	20 17+34	71	275
86	18 11 30	69	18 32 31	70	18 53 32	70	19 13 33	70	19 33 34	71	274
87	17 25 31	69	17 46 32	69	18 08 32	69	18 29 33	70	18 49 34	70	273
88	16 39 31	68	17 01 32	69	17 23 33	69	17 44 34	69	18 06 34	69	272
89	15 54 31	68	16 16 32	68	16 39 33	68	17 00 34	69	17 22 35	69	271
90	15 09+31	67	15 32+32	68	15 54+33	68	16 17+34	68	16 39+35	68	270

In South { For argument H.A. on the left, True Azimuth = $180^\circ + \text{Tabulated Azimuth}$. } See
 Latitudes { For argument H.A. on the right, True Azimuth = $180^\circ - \text{Tabulated Azimuth}$. } p. 91.

27°

DECLINATION **SAME** NAME AS LATITUDE

27°

LAT.	35°		36°		37°		38°		39°		LAT.
H.A.	Alt.	Az.	Alt.	Az.	Alt.	Az.	Alt.	Az.	Alt.	Az.	H.A.
90	15 09+31	67	15 32+32	68	15 54+33	68	16 17+34	68	16 39+35	68	270
91	14 24 31	67	14 47 33	67	15 10 34	67	15 33 34	68	15 56 35	68	269
92	13 39 32	66	14 02 33	67	14 26 34	67	14 49 35	67	15 13 35	67	268
93	12 54 32	66	13 18 33	66	13 42 34	66	14 06 35	67	14 30 36	67	267
94	12 09 33	65	12 34 34	66	12 59 34	66	13 23 35	66	13 47 36	66	266
95	11 25+33	65	11 50+34	65	12 15+35	65	12 40+36	65	13 05+36	66	265
96	10 41+33	64	11 07 34	65	11 32 35	65	11 58 35	65	12 23 36	65	264
97	...		10 23+35	64	10 49 35	64	11 15 36	64	11 41 36	65	263
98	...		...		10 06+36	64	10 33+36	64	10 59 37	64	262
99	...		...		...		...		10 18+37	63	261
100	...		...		...		...		...		260

27°

DECLINATION **CONTRARY** NAME TO LATITUDE

27°

LAT.	35°		36°		37°		38°		39°		LAT.
H.A.	Alt.	Az.	Alt.	Az.	Alt.	Az.	Alt.	Az.	Alt.	Az.	H.A.
45	14 52-48	139	14 07-49	139	13 21-49	140	12 36-50	140	11 50-50	140	315
46	14 20 48	139	13 35 48	139	12 50 48	139	12 05 49	139	11 20 49	139	314
47	13 47 47	138	13 03 48	138	12 18 47	138	11 34 48	138	10 49 48	138	313
48	13 14 46	137	12 30 47	137	11 46 47	137	11 02 47	138	10 18-48	138	312
49	12 41 47	136	11 57 46	137	11 14 47	137	10 31-48	137	...		311
50	12 07-46	136	11 24-46	136	10 41-47	136	...		...		310
51	11 32 45	135	10 50 46	135	10 08-46	135	...		...		309
52	10 58 45	134	10 16-45	134	...		...		...		308
53	10 23-45	134	...		...		...		...		307
54	...		...		...		...		...		306
55	...		...		...		...		...		305

In North { For argument H.A. on the left, True Azimuth = 360° - Tabulated Azimuth. } See
 Latitudes { For argument H.A. on the right, True Azimuth = Tabulated Azimuth. } p. 90.

LAT.	35°		36°		37°		38°		39°		LAT.
H.A.	Alt.	Az.	Alt.	Az.	Alt.	Az.	Alt.	Az.	Alt.	Az.	H.A.
0	^d 28 02-60	180	^d 27 02-60	180	^d 26 02-60	180	^d 25 02-60	180	^d 24 02-60	180	360
1	28 01 60	179	27 01 60	179	26 01 60	179	25 01 60	179	24 01 59	179	359
2	28 00 60	178	27 00 60	178	26 00 60	178	25 00 60	178	24 00 60	178	358
3	27 58 60	177	26 58 60	177	25 58 60	177	24 58 60	177	23 58 60	177	357
4	27 55 60	176	26 55 60	176	25 55 60	176	24 55 60	176	23 55 59	176	356
5	27 51-60	175	26 51-60	175	25 51-59	175	24 52-60	175	23 52-60	175	355
6	27 46 60	174	26 46 59	174	25 47 60	174	24 47 59	174	23 48 60	174	354
7	27 40 59	173	26 41 60	173	25 41 59	173	24 42 60	173	23 42 59	173	353
8	27 34 59	172	26 35 60	172	25 35 59	172	24 36 60	172	23 37 60	172	352
9	27 27 60	171	26 27 59	171	25 28 59	171	24 29 59	171	23 30 60	171	351
10	27 19-60	170	26 20-60	170	25 20-59	170	24 21-59	170	23 22-59	170	350
11	27 10 59	169	26 11 59	169	25 12 59	169	24 13 59	169	23 14 59	169	349
12	27 00 59	168	26 01 59	168	25 03 59	168	24 04 59	168	23 05 59	168	348
13	26 49 58	167	25 51 59	167	24 52 58	167	23 54 59	167	22 55 58	167	347
14	26 38 59	166	25 40 59	166	24 41 58	166	23 43 58	166	22 45 59	166	346
15	26 26-59	165	25 28-59	165	24 30-59	165	23 32-59	165	22 34-59	166	345
16	26 12 58	164	25 15 58	164	24 17 58	164	23 19 58	164	22 22 59	165	344
17	25 59 58	163	25 01 58	163	24 04 58	163	23 06 58	164	22 09 58	164	343
18	25 44 57	162	24 47 58	162	23 50 58	162	22 53 58	163	21 55 57	163	342
19	25 29 58	161	24 32 57	161	23 35 57	162	22 38 57	162	21 41 57	162	341
20	25 12-57	160	24 16-57	160	23 20-58	161	22 23-57	161	21 26-57	161	340
21	24 56 57	159	23 59 56	160	23 03 57	160	22 07 57	160	21 11 57	160	339
22	24 38 56	158	23 42 56	159	22 46 56	159	21 50 56	159	20 55 57	159	338
23	24 20 57	158	23 24 56	158	22 29 57	158	21 33 56	158	20 38 57	158	337
24	24 00 55	157	23 05 56	157	22 10 56	157	21 15 56	157	20 20 56	157	336
25	23 41-56	156	22 46-56	156	21 51-56	156	20 56-55	156	20 02-56	156	335
26	23 20 55	155	22 26 55	155	21 32 56	155	20 37 56	155	19 43 56	155	334
27	22 59 55	154	22 05 55	154	21 11 55	154	20 17 55	154	19 23 55	155	333
28	22 37 54	153	21 44 55	153	20 50 55	153	19 56 55	154	19 03 55	154	332
29	22 14 54	152	21 21 54	152	20 28 54	153	19 35 55	153	18 42 55	153	331
30	21 51-54	151	20 59-54	152	20 06-54	152	19 13-54	152	18 20-54	152	330
31	21 27 53	150	20 35 53	151	19 43 54	151	18 51 54	151	17 58 54	151	329
32	21 03 53	150	20 11 53	150	19 19 53	150	18 27 53	150	17 35 53	150	328
33	20 38 53	149	19 46 52	149	18 55 53	149	18 04 54	149	17 12 53	149	327
34	20 12 52	148	19 21 52	148	18 30 53	148	17 39 53	148	16 48 53	149	326
35	19 46-52	147	18 55-52	147	18 05-53	147	17 14-52	148	16 24-53	148	325
36	19 19 52	146	18 29 52	146	17 39 52	147	16 49 53	147	15 59 53	147	324
37	18 51 51	145	18 02 52	146	17 12 51	146	16 23 52	146	15 33 52	146	323
38	18 23 51	145	17 34 51	145	16 45 51	145	15 56 51	145	15 07 52	145	322
39	17 55 51	144	17 06 51	144	16 18 51	144	15 29 51	144	14 40 51	145	321
40	17 25-50	143	16 37-50	143	15 49-50	143	15 01-51	144	14 13-51	144	320
41	16 56 50	142	16 08 50	143	15 21 50	143	14 33 50	143	13 45 50	143	319
42	16 26 50	142	15 39 50	142	14 52 50	142	14 04 50	142	13 17 50	142	318
43	15 55 49	141	15 08 49	141	14 22 50	141	13 35 49	141	12 49 51	141	317
44	15 24 49	140	14 38 49	140	13 52 49	140	13 06 50	141	12 19 49	141	316
45	14 52-48	139	14 07-49	139	13 21-49	140	12 36-50	140	11 50-50	140	315

In South { For argument H.A. on the left, True Azimuth = 180° + Tabulated Azimuth. } See
 Latitudes { For argument H.A. on the right, True Azimuth = 180° - Tabulated Azimuth. } p. 91.

LAT.	35°		36°		37°		38°		39°		LAT.
H.A.	Alt.	Az.	Alt.	Az.	Alt.	Az.	Alt.	Az.	Alt.	Az.	H.A.
0	°	d	°	d	°	d	80 00+60	180	79 00+60	180	360
1	...	...	...	...	...	...	79 58 60	175	78 58 60	175	359
2	...	...	...	...	...	...	79 52 59	170	78 53 59	171	358
3	...	...	...	...	...	...	79 42 58	165	78 43 59	166	357
4	...	...	...	...	...	...	79 27 57	160	78 31 57	162	356
5	...	...	...	...	...	...	79 10+55	156	78 15+56	158	355
6	...	...	...	...	79 41+52	149	78 49 54	152	77 56 54	154	354
7	...	...	...	...	79 15 50	145	78 25 52	148	77 34 53	150	353
8	...	...	79 31+46	138	78 46 48	141	77 58 51	144	77 09 52	146	352
9	79 37+41	130	78 57 44	134	78 15 46	137	77 29 49	140	76 42 50	143	351
10	78 59+38	127	78 21+42	131	77 41+45	134	76 58+47	137	76 13+49	140	350
11	78 19 36	124	77 44 40	128	77 06 42	131	76 25 45	134	75 42 47	137	349
12	77 37 35	121	77 05 38	125	76 29 41	128	75 50 44	131	75 10 45	134	348
13	76 55 33	119	76 24 37	122	75 51 39	126	75 14 42	129	74 36 44	132	347
14	76 11 32	117	75 43 35	120	75 11 38	123	74 37 41	126	74 00 43	129	346
15	75 27+31	115	75 00+34	118	74 31+36	121	73 58+40	124	73 23+42	127	345
16	74 42 29	113	74 17 33	116	73 49 36	119	73 19 38	122	72 46 40	125	344
17	73 56 29	111	73 33 32	114	73 07 35	117	72 38 37	120	72 07 39	123	343
18	73 10 28	110	72 49 30	113	72 24 34	116	71 57 36	118	71 27 39	121	342
19	72 24 27	108	72 04 29	111	71 41 32	114	71 15 35	117	70 47 37	119	341
20	71 37+26	107	71 18+29	110	70 57+31	112	70 32+35	115	70 06+36	118	340
21	70 50 25	106	70 32 29	108	70 12 31	111	69 49 34	114	69 24 36	116	339
22	70 02 25	104	69 46 28	107	69 27 30	110	69 06 32	112	68 42 35	114	338
23	69 14 25	103	68 59 28	106	68 42 29	108	68 22 32	111	67 59 35	113	337
24	68 27 24	102	68 13 26	105	67 56 29	107	67 37 32	109	67 16 34	112	336
25	67 38+24	101	67 26+26	104	67 10+29	106	66 53+30	108	66 33+33	110	335
26	66 50 24	100	66 38 26	103	66 24 28	105	66 08 30	107	65 49 32	109	334
27	66 02 23	99	65 51 25	102	65 38 27	104	65 22 30	106	65 05 32	108	333
28	65 13 23	99	65 03 25	101	64 51 27	103	64 37 29	105	64 20 32	107	332
29	64 25 22	98	64 15 25	100	64 04 27	102	63 51 29	104	63 35 32	106	331
30	63 36+22	97	63 28+24	99	63 17+27	101	63 05+29	103	62 51+30	105	330
31	62 47 22	96	62 40 24	98	62 30 27	100	62 19 28	102	62 05 31	104	329
32	61 58 22	95	61 52 24	97	61 43 26	99	61 32 29	101	61 20 30	103	328
33	61 09 22	95	61 03 24	97	60 56 26	98	60 46 28	100	60 34 30	102	327
34	60 20 22	94	60 15 24	96	60 08 26	98	59 59 28	99	59 49 29	101	326
35	59 31+22	93	59 27+24	95	59 21+25	97	59 13+27	98	59 03+29	100	325
36	58 42 22	93	58 38 24	94	58 33 25	96	58 26 27	98	58 17 29	99	324
37	57 53 22	92	57 50 24	94	57 45 26	95	57 39 27	97	57 31 29	98	323
38	57 04 22	92	57 02 23	93	56 58 25	95	56 52 27	96	56 45 28	98	322
39	56 15 22	91	56 13 24	92	56 10 25	94	56 05 27	95	55 59 28	97	321
40	55 26+21	90	55 25+23	92	55 22+25	93	55 18+27	95	55 12+29	96	320
41	54 37 21	90	54 36 24	91	54 34 25	93	54 31 26	94	54 26 28	95	319
42	53 47 22	89	53 48 23	91	53 46 25	92	53 44 26	93	53 39 29	95	318
43	52 58 22	89	52 59 24	90	52 58 25	91	52 56 27	93	52 53 28	94	317
44	52 09 22	88	52 11 23	89	52 11 25	91	52 09 27	92	52 06 29	93	316
45	51 20+22	88	51 22+24	89	51 23+25	90	51 22+26	91	51 20+28	93	315

In North { For argument H.A. on the left, True Azimuth = $360^\circ - \text{Tabulated Azimuth}$. } See
 Latitudes { For argument H.A. on the right, True Azimuth = Tabulated Azimuth. } p. 90.

LAT.	35°		36°		37°		38°		39°		LAT.
H.A.	Alt.	Az.	Alt.	Az.	Alt.	Az.	Alt.	Az.	Alt.	Az.	H.A.
45	51 20+22	88	51 22+24	89	51 23+25	90	51 22+26	91	51 20+28	93	315
46	50 31 22	87	50 34 23	88	50 35 25	89	50 35 26	91	50 33 28	92	314
47	49 42 22	87	49 45 24	88	49 47 25	89	49 47 27	90	49 47 28	91	313
48	48 53 22	86	48 57 23	87	48 59 25	88	49 00 27	89	49 00 28	91	312
49	48 04 22	86	48 08 24	87	48 11 25	88	48 13 26	89	48 13 28	90	311
50	47 15+22	85	47 20+24	86	47 23+25	87	47 26+26	88	47 27+28	89	310
51	46 26 23	85	46 31 24	86	46 35 26	87	46 38 27	88	46 40 28	89	309
52	45 37 23	84	45 43 24	85	45 48 25	86	45 51 27	87	45 54 28	88	308
53	44 48 23	84	44 55 24	85	45 00 25	86	45 04 27	87	45 07 28	88	307
54	44 00 23	83	44 06 25	84	44 12 26	85	44 17 27	86	44 21 28	87	306
55	43 11+23	83	43 18+25	84	43 24+26	84	43 30+27	85	43 34+28	86	305
56	42 22 23	82	42 30 24	83	42 37 26	84	42 43 27	85	42 48 28	86	304
57	41 34 23	82	41 42 25	83	41 49 26	83	41 56 27	84	42 01 29	85	303
58	40 45 24	81	40 54 25	82	41 02 26	83	41 09 27	84	41 15 28	85	302
59	39 56 24	81	40 06 25	82	40 14 26	82	40 22 27	83	40 28 29	84	301
60	39 08+24	80	39 18+25	81	39 27+26	82	39 35+27	83	39 42+29	84	300
61	38 20 24	80	38 30 25	81	38 39 27	81	38 48 28	82	38 56 29	83	299
62	37 31 25	79	37 42 26	80	37 52 27	81	38 01 28	82	38 09 29	82	298
63	36 43 25	79	36 54 26	80	37 05 27	80	37 14 28	81	37 23 29	82	297
64	35 55 25	78	36 07 25	79	36 18 27	80	36 28 28	81	36 37 29	81	296
65	35 07+25	78	35 19+26	79	35 30+28	79	35 41+28	80	35 51+30	81	295
66	34 19 25	78	34 32 26	78	34 43 28	79	34 55 28	80	35 05 30	80	294
67	33 31 25	77	33 44 27	78	33 57 27	78	34 08 29	79	34 19 30	80	293
68	32 43 26	77	32 57 26	77	33 10 27	78	33 22 29	79	33 34 29	79	292
69	31 55 26	76	32 09 27	77	32 23 28	77	32 36 29	78	32 48 30	79	291
70	31 08+26	76	31 22+27	76	31 36+28	77	31 50+29	77	32 02+30	78	290
71	30 20 27	75	30 35 28	76	30 50 28	76	31 03 30	77	31 17 30	78	289
72	29 33 26	75	29 48 28	75	30 03 29	76	30 17 30	76	30 31 31	77	288
73	28 46 26	74	29 01 28	75	29 17 29	75	29 32 29	76	29 46 31	77	287
74	27 58 27	74	28 15 28	74	28 30 29	75	28 46 30	75	29 01 31	76	286
75	27 11+27	73	27 28+28	74	27 44+30	74	28 00+30	75	28 15+32	75	285
76	26 24 28	73	26 41 29	73	26 58 30	74	27 15 30	74	27 30 32	75	284
77	25 37 28	73	25 55 29	73	26 12 30	73	26 29 31	74	26 45 32	74	283
78	24 51 27	72	25 09 29	73	25 27 29	73	25 44 31	73	26 01 31	74	282
79	24 04 28	72	24 23 29	72	24 41 30	72	24 59 31	73	25 16 32	73	281
80	23 17+29	71	23 37+29	72	23 55+31	72	24 14+31	72	24 31+33	73	280
81	22 31 29	71	22 51 29	71	23 10 30	72	23 29 31	72	23 47 32	72	279
82	21 45 29	70	22 05 30	71	22 24 31	71	22 44 32	71	23 03 32	72	278
83	20 59 29	70	21 19 30	70	21 39 31	71	21 59 32	71	22 19 32	71	277
84	20 13 29	69	20 34 30	70	20 54 32	70	21 15 32	70	21 35 33	71	276
85	19 27+30	69	19 48+31	69	20 09+32	70	20 30+33	70	20 51+33	70	275
86	18 41 30	68	19 03 31	69	19 25 32	69	19 46 33	69	20 07 34	70	274
87	17 56 30	68	18 18 31	68	18 40 32	69	19 02 33	69	19 23 34	69	273
88	17 10 31	67	17 33 32	68	17 56 32	68	18 18 33	68	18 40 34	69	272
89	16 25 31	67	16 48 32	67	17 12 32	68	17 34 34	68	17 57 34	68	271
90	15 40+32	66	16 04+32	67	16 27+33	67	16 51+34	67	17 14+34	68	270

In South { For argument H.A. on the left, True Azimuth = $180^\circ + \text{Tabulated Azimuth}$. } See
 Latitudes { For argument H.A. on the right, True Azimuth = $180^\circ - \text{Tabulated Azimuth}$. } p. 91.

28°

DECLINATION **SAME** NAME AS LATITUDE

28°

LAT.	35°		36°		37°		38°		39°		LAT.
H.A.	Alt.	Az.	Alt.	Az.	Alt.	Az.	Alt.	Az.	Alt.	Az.	H.A.
90	15 40+32	66	16 04+32	67	16 27+33	67	16 51+34	67	17 14+34	68	270
91	14 55 32	66	15 20 32	66	15 44 33	66	16 07 34	67	16 31 35	67	269
92	14 11 32	65	14 35 33	66	15 00 33	66	15 24 35	66	15 48 35	66	268
93	13 26 33	65	13 51 33	65	14 16 34	65	14 41 35	66	15 06 35	66	267
94	12 42 33	65	13 08 33	65	13 33 34	65	13 58 35	65	14 23 36	65	266
95	11 58+33	64	12 24+34	64	12 50+34	64	13 16+35	65	13 41+36	65	265
96	11 14 33	64	11 41 34	64	12 07 35	64	12 33 36	64	12 59 37	64	264
97	10 31+33	63	10 58 34	63	11 24 35	63	11 51 36	64	12 17 37	64	263
98	...		10 15+34	63	10 42 35	63	11 09 36	63	11 36 37	63	262
99	...		...		10 00+35	62	10 27+37	62	10 55 37	63	261
100	...		...		...		...		10 14+37	62	260

28°

DECLINATION **CONTRARY** NAME TO LATITUDE

28°

LAT.	35°		36°		37°		38°		39°		LAT.
H.A.	Alt.	Az.	Alt.	Az.	Alt.	Az.	Alt.	Az.	Alt.	Az.	H.A.
45	14 04-48	140	13 18-48	140	12 32-48	140	11 46-49	140	11 00-49	141	315
46	13 32 47	139	12 47 48	139	12 02 49	140	11 16 48	140	10 31 49	140	314
47	13 00 47	138	12 15 47	139	11 31 48	139	10 46 49	139	10 01-49	139	313
48	12 28 47	138	11 43 47	138	10 59 48	138	10 15-48	138	...		312
49	11 54 46	137	11 11 47	137	10 27-47	137	...		...		311
50	11 21-46	136	10 38-47	137	...		...		...		310
51	10 47 45	136	10 04-45	136	...		...		...		309
52	10 13-45	135	...		...		...		...		308
53	...		...		...		...		...		307
54	...		...		...		...		...		306
55	...		...		...		...		...		305

In North { For argument H.A. on the left, True Azimuth = 360° - Tabulated Azimuth. } See
 Latitudes { For argument H.A. on the right, True Azimuth = Tabulated Azimuth. } p. 90.

LAT.	35°		36°		37°		38°		39°		LAT.
H.A.	Alt.	Az.	Alt.	Az.	Alt.	Az.	Alt.	Az.	Alt.	Az.	H.A.
0	27 02-60	180	26 02-60	180	25 02-60	180	24 02-60	180	23 02-60	180	360
1	27 01 60	179	26 01 60	179	25 01 60	179	24 01 59	179	23 02 60	179	359
2	27 00 60	178	26 00 60	178	25 00 60	178	24 00 60	178	23 00 60	178	358
3	26 58 60	177	25 58 60	177	24 58 60	177	23 58 60	177	22 58 59	177	357
4	26 55 60	176	25 55 60	176	24 55 60	176	23 55 59	176	22 56 60	176	356
5	26 51-60	175	25 51-59	175	24 52-60	175	23 52-60	175	22 52-60	175	355
6	26 46 59	174	25 47 60	174	24 47 60	174	23 48 60	174	22 48 60	174	354
7	26 41 60	173	25 41 59	173	24 42 60	173	23 42 59	173	22 43 60	173	353
8	26 35 60	172	25 35 59	172	24 36 60	172	23 36 59	172	22 37 59	172	352
9	26 27 59	171	25 28 59	171	24 29 59	171	23 30 60	171	22 30 59	171	351
10	26 19-59	170	25 20-59	170	24 21-59	170	23 22-59	170	22 23-59	170	350
11	26 11 59	169	25 12 59	169	24 13 59	169	23 14 59	169	22 15 59	170	349
12	26 01 59	168	25 02 59	168	24 04 59	168	23 05 59	168	22 06 59	169	348
13	25 51 59	167	24 52 59	167	23 54 59	167	22 55 59	168	21 57 59	168	347
14	25 39 58	166	24 41 58	166	23 43 59	167	22 45 59	167	21 46 58	167	346
15	25 27-58	165	24 29-58	165	23 31-58	166	22 33-58	166	21 35-58	166	345
16	25 14 58	164	24 17 58	165	23 19 58	165	22 21 58	165	21 23 58	165	344
17	25 01 58	163	24 03 57	164	23 06 58	164	22 08 58	164	21 11 58	164	343
18	24 47 58	163	23 49 57	163	22 52 58	163	21 55 58	163	20 58 58	163	342
19	24 31 57	162	23 35 58	162	22 38 58	162	21 41 58	162	20 44 58	162	341
20	24 15-57	161	23 19-57	161	22 22-57	161	21 26-58	161	20 29-57	161	340
21	23 59 57	160	23 03 57	160	22 06 57	160	21 10 57	160	20 14 58	160	339
22	23 42 57	159	22 46 57	159	21 50 57	159	20 54 57	159	19 58 57	159	338
23	23 23 56	158	22 28 56	158	21 32 56	158	20 37 57	158	19 41 57	159	337
24	23 05 56	157	22 09 56	157	21 14 56	157	20 19 56	157	19 24 57	158	336
25	22 45-55	156	21 50-55	156	20 55-55	156	20 01-57	157	19 06-57	157	335
26	22 25 55	155	21 31 56	155	20 36 56	156	19 41 55	156	18 47 56	156	334
27	22 04 55	154	21 10 55	155	20 16 55	155	19 22 56	155	18 28 56	155	333
28	21 43 55	154	20 49 55	154	19 55 55	154	19 01 55	154	18 08 56	154	332
29	21 20 54	153	20 27 54	153	19 34 55	153	18 40 54	153	17 47 55	153	331
30	20 57-53	152	20 05-54	152	19 12-55	152	18 19-55	152	17 26-55	152	330
31	20 34 54	151	19 42 54	151	18 49 54	151	17 57 55	151	17 04 54	152	329
32	20 10 53	150	19 18 54	150	18 26 54	150	17 34 54	151	16 42 55	151	328
33	19 45 53	149	18 54 53	149	18 02 53	150	17 10 53	150	16 19 54	150	327
34	19 20 53	148	18 29 53	149	17 37 52	149	16 46 53	149	15 55 53	149	326
35	18 54-52	148	18 03-52	148	17 12-52	148	16 22-53	148	15 31-53	148	325
36	18 27 51	147	17 37 52	147	16 47 52	147	15 56 52	147	15 06 53	147	324
37	18 00 51	146	17 10 51	146	16 21 52	146	15 31 52	147	14 41 53	147	323
38	17 32 50	145	16 43 51	145	15 54 52	146	15 05 52	146	14 15 52	146	322
39	17 04 50	144	16 15 50	145	15 27 51	145	14 38 52	145	13 49 52	145	321
40	16 35-50	144	15 47-50	144	14 59-51	144	14 10-51	144	13 22-51	144	320
41	16 06 49	143	15 18 50	143	14 31 51	143	13 43 51	143	12 55 51	144	319
42	15 36 49	142	14 49 49	142	14 02 50	142	13 14 50	143	12 27 51	143	318
43	15 06 49	141	14 19 49	142	13 32 49	142	12 46 50	142	11 58 50	142	317
44	14 35 48	141	13 49 49	141	13 03 49	141	12 16 49	141	11 30 50	141	316
45	14 04-48	140	13 18-48	140	12 32-48	140	11 46-49	140	11 00-49	141	315

In South { For argument H.A. on the left, True Azimuth = $180^\circ +$ Tabulated Azimuth. } See
 Latitudes { For argument H.A. on the right, True Azimuth = $180^\circ -$ Tabulated Azimuth. } p. 91

EXPLANATION

By agreement with the Admiralty, the *Astronomical Navigation Tables* are produced by H.M. Nautical Almanac Office to the general requirements of the Air Ministry.

These tables are designed to give, in a simple and direct manner, the solution of the astronomical spherical triangle that occurs in navigational practice. They have been planned for use with the *Air Almanac* (Air Publication 1602) and are consequently designed primarily to meet the requirements of modern air navigation: their use can however be extended to surface navigation, as in the case of the *Air Almanac*, within the limitations of the precision of the tabulated altitude and azimuth.

The general object of the *Astronomical Navigation Tables* is to facilitate the calculation of the Altitude and Azimuth of an observed heavenly body, as seen from some position close to that of the observer. This information, together with the observed altitude, allows to be plotted on the chart a position line upon which the observer must lie; two such position lines serve in general to determine the position of the observer. The tables have been arranged with special relation to the determination of the altitude and azimuth when an assumed position is adopted such that the latitude and hour angle are both integral degrees; interpolation in this case is consequently restricted to interpolation to the declination of the body observed, and provision has been made for this to be done in a simple manner. The precision of the tabulated data is consistent with that adopted for the *Air Almanac*, namely that the altitudes are given to the nearest minute of arc, and so are correct to within 0'·5; this standard of precision is sufficient for all purposes of air navigation and, in fact, is at present (1938) considerably greater than the precision obtainable in an altitude observed with a bubble sextant. Although these tables have been prepared in conjunction with the *Air Almanac*, they are equally applicable for use with any other almanac from which the Greenwich Hour Angle and Declination of the body observed can be found for the time of observation; it is intended, however, that the two publications should provide, in the most convenient form, all the material for a rapid solution of the navigator's problem, for all practical observations.

The *Astronomical Navigation Tables* consist of main tables and auxiliary tables. The main tables give the Tabulated Altitude, to the nearest minute of arc, and the Tabulated Azimuth, to the nearest degree, with the three arguments:—

Latitude —each integral degree from S.64° to N.64°.

Declination—for 22 selected stars for the epoch 1940 and each integral degree from S.28° to N.28°.

Hour Angle—each integral degree for which the altitude is greater than 10°* and less than 80°.

Thus for every combination of an integral degree of latitude, declination and hour angle in the above ranges, the tables give immediately the quantities required.

* This limit is decreased for latitudes above 55°, for declinations appropriate to the Sun (0°–23°), since in these latitudes the Sun is at a low altitude for long periods of each day, when observation of other bodies is not possible.

EXPLANATION

In the case of the separate tabulations for the 22 stars, the values of the declinations used in the tables are those of the stars themselves at the middle of 1940; the declinations of the stars change slowly owing to precession and to other causes, but the effect of these changes can be allowed for by means of a simple correcting term, which although smaller, is catered for in a similar way to the interpolation for the declination of other bodies. The stars have been selected for their brightness and their distribution in the sky, and are the same in both name and number as stars Nos. 1-22 in the *Air Almanac*. The tables for integral degrees of declination are applicable to observations of the Sun, Moon and planets, as well as for all stars with declinations between S.29° and N.29°; a list of 13 such stars is given in the *Air Almanac* (Nos. 23-35). It is only for stars outside these limits of declination, in particular stars Nos. 36-50 in the *Air Almanac*, that these tables are not applicable; some other method of obtaining the altitude and azimuth must then be employed. The 22 stars catered for separately may however be regarded as generally sufficient for all practical purposes of air navigation; with the 13 additional stars to be used in exceptional circumstances, reference to other methods should be unnecessary.

The interpolation of tables with three arguments is both laborious and difficult, and should be avoided wherever possible; no provision has therefore been made for interpolation other than for declination, and the navigator should not interpolate for latitude and hour angle, but should use an assumed position so that this may be avoided. The arrangement of the tables, however, allows for interpolation for latitude and hour angle without, in general, the necessity for the comparison of figures on different pages, and the tables may therefore be interpolated for these arguments for the solution of special problems.

The tabulated altitude includes the effect of atmospheric refraction, and is thus directly comparable with the corrected sextant reading; it is in fact the altitude of the body as would be measured by an observer. The refraction included is based on the mean value of the refraction at a height of 5,000 feet in normal conditions, and it is unlikely that at heights in that neighbourhood the refraction will differ by more than 0.5 from that used. Table VI on page 222 gives the adjustment necessary at heights that differ materially from the basic height adopted; the values in this table should only be applied in extreme cases, and where great accuracy is necessary.

The tabulated azimuth is measured from the elevated pole either to the east or to the west. This can be converted to true azimuth, measured always from the north through east, either by the rules given at the foot of each page, or by the use of Table III on pages 90 and 91.

For the greater convenience of the user, the tables are issued in thirteen volumes, each of which caters for a belt of latitude, 5° in width, in both the northern and southern hemispheres. In each volume tabulations are given for five integral degrees of latitude; working from an assumed position, whose latitude is taken to be the nearest integral degree to that of the D.R. (or estimated) position of the observer, each tabular latitude suffices to cover observations from positions within 0° 30' of the integral degree used. The Explanation and auxiliary tables are reprinted in each volume.

Each volume consists of two main parts, pages 2-89 giving the tabulations for the selected 22 stars and pages 94-209 those for declinations 0°-28°. Each part is

EXPLANATION

divided into sections of four pages, covering one star or one whole degree of declination; separate indexes on the margin enable immediate reference to be made to the first opening of each section. Throughout, the arrangement of the tabulations in each section is generally the same; the five values of latitude (LAT.) are given across the page and the values of the hour angle (H.A.) down the page. For the stars, the tabulations for NORTH latitudes precede those for SOUTH latitudes, and for the integral degrees of declination, those for the SAME name as the latitude precede those for CONTRARY name. The amount of tabulation varies in each case with different stars and declinations, and in some cases there are no tabulations either in north or in south latitudes, as the star or a body of the given declination does not reach an altitude which makes it suitable for observation in those latitudes; occasionally it has been necessary to continue the tabulation from one page on to the previous page, and for one or two stars, in south latitudes, on to two pages before.

For the stars, each column refers to a given latitude, and contains for all applicable values of the hour angle, the altitude (Alt.), its variation with time (t) and the azimuth (Az.). For the degrees of declination, the variation t is replaced by the difference (d) between the altitude given and that for the following degree. The procedure of entering and interpolating the tables is not appreciably different in the two cases.

An assumed position is taken close to the D.R. position so that the latitude is an integral degree, while the longitude is chosen so that the hour angle, formed by the combination of longitude (*added if east, subtracted if west*) with the G.H.A., taken from the *Air Almanac*, is also an integral degree. The appropriate part (star or degree of declination) is chosen, and the correct section obtained by the marginal index, using the star number, or the integral degree numerically *less* than the declination of the observed body as found from the *Air Almanac*. In this section, the column is chosen corresponding to the assumed latitude, care being taken to select the correct hemisphere. In this column, the values of Alt., t , and Az. can be read off for the stars, corresponding to the particular integral hour angle; for a degree of declination, the values of Alt., d and Az. are similarly found.

The tabulated altitude must now be corrected, in the case of the 22 stars, for the effect of precession, and for other bodies, interpolated to the true declination. Table I on the inside front cover gives the correction to be applied to the altitude of the stars for all years to 2000 for values of t ; this correction must be added or subtracted according to the sign prefixed to t . For each star a limiting year is given before which this correction cannot exceed $1'$, and there is therefore no need to apply it until after that date. Similarly, the inside back cover and its facing page contain Table XV, with arguments d and the minutes of the declination of the body, giving the correction to be applied to the tabulated altitude taken out for an integral degree; this correction is to be applied to the tabulated altitude with the same sign as that of d .

It is unnecessary to correct the tabulated azimuth in any way, but it must of course be converted to true azimuth before being used to plot a position line.

Having thus obtained the corrected tabulated altitude and the true azimuth, the position line is drawn in the usual manner. The intercept is obtained from the difference between the corrected sextant reading and the corrected tabulated altitude, and is set off from the assumed position either *towards* the direction given

EXPLANATION

by the true azimuth or in the opposite direction (*away* from), according to the following rules:

Corr. Tab. Alt. *less* than Corr. Sext. Rdg., intercept *towards*;

Corr. Tab. Alt. *greater* than Corr. Sext. Rdg., intercept *away*.

The position line is then drawn at right angles to the intercept through the point so obtained. The expression corrected sextant reading is used conveniently for the observed altitude to emphasize that this quantity is the altitude as measured by the sextant, corrected only for sextant errors and for dome refraction if applicable. As the atmospheric refraction is catered for in the tabulated altitude, no correction for this should be applied to the sextant reading.

If the assumed position is close to the true position, a slight inaccuracy in plotting the tabulated azimuth is unimportant; when the tabulated azimuth is near 0° or 180° advantage may be taken of this to draw the position line simply as part of a parallel of latitude. A double border rule, given when the azimuth is within a few degrees of the meridian, indicates the portions of the tables where this can be done without great error; the limit of azimuth has been varied slightly in different volumes, according to the latitude, so as to reduce the error due to this simplified procedure. The accuracy of this method depends upon the error in the assumed longitude; for an error of 20 miles in the D.R. longitude, the maximum error introduced into the deduced latitude is about 2 miles, while the remaining error (due to the use of an assumed position) may reach a maximum of 2 miles in the worst case. This method should therefore only be adopted either when errors up to about 4 miles can be tolerated, or when the D.R. longitude is known to be fairly accurate; if the D.R. position is liable to much greater error than 20 miles, this method should not be used. An assumed position is taken and the tables entered in exactly the same way (whether for stars or other bodies) as for an ordinary observation, but there is now no necessity to take out the azimuth or to convert to true azimuth. The tabulated altitude is corrected by Table I or Table XV as necessary, and the intercept formed by the usual rules. The intercept is then set off from the assumed position *towards* or *away* from the direction of the object observed, this direction being taken as true north or true south; the position line is thus drawn in as a parallel of latitude. Although the procedure of entering the tables is exactly the same, this method saves a considerable amount of work in the plotting of the position line.

A list of the auxiliary tables is given in the list of contents; in general the titles of these tables are self-explanatory and their use either self-evident or explained on the page concerned.

Tables VII, VIII, IX, X, XI and XIII are arranged as critical tables, so that the result is obtained immediately without interpolation. The argument is divided into intervals, successive intervals corresponding to successive values of the result; for any values of the argument, inside one of these intervals, the corresponding result is the quantity opposite that interval and has in general a maximum error of less than half a unit in the last figure given; when successive values of the result are not consecutive integers, this error can rise to half the difference between successive values. The tabulated values of the argument correspond to half-way values of the result, and these are always chosen so that when the argument is exactly equal to one of the tabulated values, the nearest value of the result is the one corresponding to the previous interval. Thus the rule to be followed is:

When the argument is an exact tabulated value, the *upper* of the two possible values of the result should be taken.

ILLUSTRATIONS

Example 1.—On 1939 September 30, local date, about two hours after sunset, in dead reckoning position latitude $38^{\circ} 17' N.$, longitude $125^{\circ} 20' W.$, star number 5 (Altair) was observed to obtain a position line. Corrected sextant reading $58^{\circ} 39'$; G.M.T. of observation $04^h 18^m 14^s$.

From Table IV, page 92 :

Long. $120^{\circ} W.$ (approx.)		
Approx.	Hrs.	Date
L.M.T.	2000	Sept. 30
G.M.T.	0400	Oct. 1

From page 18 :

Lat. of ass. position $38^{\circ} NORTH$

Tab. Alt.	.	.	59	05
Correction	.	.	—	—
Corr. Tab. Alt.	.	.	59	05
Corr. Sext. Rdg.	.	.	58	39
Intercept	.	.		26' away

From *Air Almanac*, 1939 Oct. 1 :

G.H.A. γ	($04^h 10^m$)	.	71	36
Increment	($8^m 14^s$)	.	2	04
S.H.A.	(No. 5)	.	63	02
G.H.A. of star		.	136	36
Long. of ass. position		.	—125	36

Star No. 5

H.A. 11°

No correction for date is necessary in 1939.

Tab. Az. 158°

Assumed position : From Table III,
 Lat. $38^{\circ} N.$ page 90 :
 Long. $125^{\circ} 36' W.$ True Az. $202^{\circ} T.$

Example 2.—On 1950 August 17, Greenwich date, in dead reckoning position latitude $35^{\circ} 52' S.$, longitude $26^{\circ} 29' E.$, star number 4 (Alpheratz) was observed to obtain a position line. From the *Almanac* of that date it was found that the G.H.A. of the star corresponding to the G.M.T. of observation was $355^{\circ} 14'$. Corrected sextant reading $22^{\circ} 10'$.

G.H.A. of star	355	14
Long. of ass. position	+ 26	46
	382	00
	—360	

From page 17 :

Lat. of ass. position $36^{\circ} SOUTH$

Tab. Alt.	.	.	22	02
Correction (Table I)	.	—	3	
Corr. Tab. Alt.	.	.	21	59
Corr. Sext. Rdg.	.	.	22	10
Intercept	.	.		11' towards

Star No. 4

H.A. 22°

Time . . . —19
 Year . . . 1950

Tab. Az. 159°

Assumed position : From Table III,
 Lat. $36^{\circ} S.$ page 91 :
 Long. $26^{\circ} 46' E.$ True Az. $339^{\circ} T.$

ILLUSTRATIONS

Example 3.—On 1939 October 1, local date, at approximate local noon, in dead reckoning position latitude $38^{\circ} 40' S.$, longitude $22^{\circ} 07' W.$, the Sun was observed to obtain a position line. Corrected sextant reading $54^{\circ} 13'$; G.M.T. of observation $13^h 11^m 27^s$.

From Table IV, page 92 :

Long. $15^{\circ} W.$ (approx.)		
Approx.	Hrs.	Date
L.M.T.	1200	Oct. 1
G.M.T.	1300	Oct. 1

From *Air Almanac*, 1939 Oct. 1 :

G.H.A.	($13^h 10^m$)	.	$20^{\circ} 02'$
Increment	($1^m 27^s$)	.	22
G.H.A. of Sun	.	.	$20^{\circ} 24'$
Long. of ass. position	.	-	$22^{\circ} 24'$
		-	$2^{\circ} 00'$
			+360

From page 102 :

Lat. of ass. position	39° S.	Dec. 2° 58' S.	SAME name	H.A. 358°
Tab. Alt.	52° 58'	d	+60	Tab. Az. 177°
Correction (Table XV)	+ 58	Minutes of dec.	58	
Corr. Tab. Alt.	53 56			
Corr. Sext. Rdg.	54 13			
Intercept	17' towards			
		Assumed position :		From Table III,
		Lat. 39° S.		page 91 :
		Long. 22° 24' W.		True Az. 003° T.

Since there is a double border rule opposite the entry on page 102, this observation may be reduced by the method described on page 213. In this case the intercept is set off from the assumed position *towards* the Sun (i.e. northwards), and the position line drawn as a parallel of latitude. There is then no necessity to take out the tabulated azimuth.

Example 4.—On 1939 October 2, local date, about an hour before sunrise, in dead reckoning position latitude $34^{\circ} 38' N.$, longitude $147^{\circ} 58' E.$, star number 35 (Wezen) was observed to obtain a position line. Corrected sextant reading $24^{\circ} 23'$; G.M.T. of observation $18^h 58^m 19^s$.

From Table IV, page 93 :

Long. $150^{\circ} E.$ (approx.)		
Approx.	Hrs.	Date
L.M.T.	0500	Oct. 2
G.M.T.	1900	Oct. 1

From *Air Almanac*, 1939 Oct. 1 :

G.H.A. Υ	($18^h 50^m$)	.	$292^{\circ} 06'$
Increment	($8^m 19^s$)	.	2 05
S.H.A.	(No. 35)	.	$253^{\circ} 31'$
G.H.A. of star	.	.	$547^{\circ} 42'$
Long. of ass. position	.	+	$148^{\circ} 18'$
			$696^{\circ} 00'$
			-360

From page 201 :

Lat. of ass. position	35° N.	Dec. 26° 18' S.	CONTRARY name	H.A. 336°
Tab. Alt.	24 56	d	-56	Tab. Az. 156°
Correction (Table XV) -	17	Minutes of dec. 18		
Corr. Tab. Alt.	24 39			
Corr. Sext. Rdg.. . . .	24 23	Assumed position :		
Intercept	16' away	Lat. 35° N.		
		Long. 148° 18' E.		
		From Table III, page 90 : True Az. 156° T.		

IVa.—CHANGE OF SEXTANT READING WITH TIME

Due to motion of
body observed

Due to motion of observer

True Azi- muth of body	Latitude			True Azi- muth of body
	35°	37°	39°	
090	+37	+36	+35	090
095	37	36	35	085
100	36	35	34	080
105	36	35	34	075
110	35	34	33	070
115	33	33	32	065
120	+32	+31	+30	060
125	30	29	29	055
130	28	28	27	050
135	26	25	25	045
140	24	23	22	040
145	21	21	20	035
150	+18	+18	+17	030
155	16	15	15	025
160	13	12	12	020
165	10	9	9	015
170	6	6	6	010
175	+3	+3	+3	005
180	0	0	0	000
185	-3	-3	-3	355
190	6	6	6	350
195	10	9	9	345
200	13	12	12	340
205	16	15	15	335
210	-18	-18	-17	330
215	21	21	20	325
220	24	23	22	320
225	26	25	25	315
230	28	28	27	310
235	30	29	29	305
240	-32	-31	-30	300
245	33	33	32	295
250	35	34	33	290
255	36	35	34	285
260	36	35	34	280
265	37	36	35	275
270	-37	-36	-35	270

Difference between True Az. of body and Track	Ground speed in m.p.h.									Difference between True Az. of body and Track
	100	130	160	190	220	250	280	310	340	
000	+4	+6	+7	+8	+10	+11	+12	+13	+15	360
005	4	6	7	8	10	11	12	13	15	355
010	4	6	7	8	9	11	12	13	15	350
015	4	5	7	8	9	10	12	13	14	345
020	4	5	7	8	9	10	11	13	14	340
025	4	5	6	7	9	10	11	12	13	335
030	+4	+5	+6	+7	+8	+9	+11	+12	+13	330
035	4	5	6	7	8	9	10	11	12	325
040	3	4	5	6	7	8	9	10	11	320
045	3	4	5	6	7	8	9	10	10	315
050	3	4	4	5	6	7	8	9	9	310
055	2	3	4	5	5	6	7	8	8	305
060	+2	+3	+3	+4	+5	+5	+6	+7	+7	300
065	2	2	3	3	4	5	5	6	6	295
070	1	2	2	3	3	4	4	5	5	290
075	1	1	2	2	2	3	3	3	4	285
080	+1	+1	1	1	2	2	2	2	3	280
085	0	0	+1	+1	+1	+1	+1	+1	+1	275
090	0	0	0	0	0	0	0	0	0	270
095	0	0	-1	-1	-1	-1	-1	-1	-1	265
100	-1	-1	1	1	2	2	2	2	3	260
105	1	1	2	2	2	3	3	3	4	255
110	1	2	2	3	3	4	4	5	5	250
115	2	2	3	3	4	5	5	6	6	245
120	-2	-3	-3	-4	-5	-5	-6	-7	-7	240
125	2	3	4	5	5	6	7	8	8	235
130	3	4	4	5	6	7	8	9	9	230
135	3	4	5	6	7	8	9	10	10	225
140	3	4	5	6	7	8	9	10	11	220
145	4	5	6	7	8	9	10	11	12	215
150	-4	-5	-6	-7	-8	-9	-11	-12	-13	210
155	4	5	6	7	9	10	11	12	13	205
160	4	5	7	8	9	10	11	13	14	200
165	4	5	7	8	9	10	12	13	14	195
170	4	6	7	8	9	11	12	13	15	190
175	4	6	7	8	10	11	12	13	15	185
180	-4	-6	-7	-8	-10	-11	-12	-13	-15	180

The theoretical change of sextant reading in any interval of time depends partly on the motion of the body observed across the sky and partly on the motion of the observer over the Earth's surface.

The two tables above give this change, in an interval of three minutes of time, due to each of these causes; a + sign denotes that the sextant reading is increasing, and a - sign that it is decreasing. The theoretical change of sextant reading in three minutes of time is obtained by combining the appropriate entries from each table.

IVb.—CHANGE OF SEXTANT READING WITH TIME

Interval of time	Change in 3 ^m (from Table IVa)								Interval of time
	0' 3' 6'	9' 12' 15'	18' 21' 24'	27' 30' 33'	36' 39' 42'	45' 48' 51'	54' 57' 60'		
0 00	0 0 0	0 0 0	0 0 0	0 0 0	0 0 0	0 0 0	0 0 0	0 00	
05	0 0 0	0 0 0	0 1 1	1 1 1	1 1 1	1 1 1	2 2 2	05	
10	0 0 0	0 1 1	1 1 1	2 2 2	2 2 2	2 3 3	3 3 3	10	
15	0 0 0	1 1 1	2 2 2	2 2 3	3 3 4	4 4 4	4 5 5	15	
20	0 0 1	1 1 2	2 2 3	3 3 4	4 4 5	5 5 6	6 6 7	20	
25	0 0 1	1 2 2	2 3 3	4 4 5	5 5 6	6 7 7	8 8 8	25	
0 30	0 0 1	2 2 2	3 4 4	4 5 6	6 6 7	8 8 8	9 10 10	0 30	
35	0 1 1	2 2 3	4 4 5	5 6 6	7 8 8	9 9 10	10 11 12	35	
40	0 1 1	2 3 3	4 5 5	6 7 7	8 9 9	10 11 11	12 13 13	40	
45	0 1 2	2 3 4	4 5 6	7 8 8	9 10 10	11 12 13	14 14 15	45	
50	0 1 2	2 3 4	5 6 7	8 8 9	10 11 12	12 13 14	15 16 17	50	
0 55	0 1 2	3 4 5	6 6 7	8 9 10	11 12 13	14 15 16	16 17 18	0 55	
1 00	0 1 2	3 4 5	6 7 8	9 10 11	12 13 14	15 16 17	18 19 20	1 00	
05	0 1 2	3 4 5	6 8 9	10 11 12	13 14 15	16 17 18	20 21 22	05	
10	0 1 2	4 5 6	7 8 9	10 12 13	14 15 16	18 19 20	21 22 23	10	
15	0 1 2	4 5 6	8 9 10	11 12 14	15 16 18	19 20 21	22 24 25	15	
20	0 1 3	4 5 7	8 9 11	12 13 15	16 17 19	20 21 23	24 25 27	20	
25	0 1 3	4 6 7	8 10 11	13 14 16	17 18 20	21 23 24	26 27 28	25	
1 30	0 2 3	4 6 8	9 10 12	14 15 16	18 20 21	22 24 26	27 28 30	1 30	
35	0 2 3	5 6 8	10 11 13	14 16 17	19 21 22	24 25 27	28 30 32	35	
40	0 2 3	5 7 8	10 12 13	15 17 18	20 22 23	25 27 28	30 32 33	40	
45	0 2 4	5 7 9	10 12 14	16 18 19	21 23 24	26 28 30	32 33 35	45	
50	0 2 4	6 7 9	11 13 15	16 18 20	22 24 26	28 29 31	33 35 37	50	
1 55	0 2 4	6 8 10	12 13 15	17 19 21	23 25 27	29 31 33	34 36 38	1 55	
2 00	0 2 4	6 8 10	12 14 16	18 20 22	24 26 28	30 32 34	36 38 40	2 00	
05	0 2 4	6 8 10	12 15 17	19 21 23	25 27 29	31 33 35	38 40 42	05	
10	0 2 4	6 9 11	13 15 17	20 22 24	26 28 30	32 35 37	39 41 43	10	
15	0 2 4	7 9 11	14 16 18	20 22 25	27 29 32	34 36 38	40 43 45	15	
20	0 2 5	7 9 12	14 16 19	21 23 26	28 30 33	35 37 40	42 44 47	20	
25	0 2 5	7 10 12	14 17 19	22 24 27	29 31 34	36 39 41	44 46 48	25	
2 30	0 2 5	8 10 12	15 18 20	22 25 28	30 32 35	38 40 42	45 48 50	2 30	
35	0 3 5	8 10 13	16 18 21	23 26 28	31 34 36	39 41 44	46 49 52	35	
40	0 3 5	8 11 13	16 19 21	24 27 29	32 35 37	40 43 45	48 51 53	40	
45	0 3 6	8 11 14	16 19 22	25 28 30	33 36 38	41 44 47	50 52 55	45	
50	0 3 6	8 11 14	17 20 23	26 28 31	34 37 40	42 45 48	51 54 57	50	
2 55	0 3 6	9 12 15	18 20 23	26 29 32	35 38 41	44 47 50	52 55 58	2 55	
3 00	0 3 6	9 12 15	18 21 24	27 30 33	36 39 42	45 48 51	54 57 60	3 00	

This table gives the theoretical change of sextant reading in any interval of time up to 3^m, in terms of the change in 3^m obtained from the tables on the opposite page. If the interval is greater than 3^m, it may be split into multiples of 3^m and a residue, and the corresponding entries from the table added together.

A knowledge of this change enables sights on different objects taken at slightly different times to be adjusted to a specified exact time, which may be either the exact time of one of them or a moment when a fix is required for a particular reason.

NOTES

NOTES

NOTES

N. 35°-39°

**V.—DIFFERENCE BETWEEN RHUMB LINE
AND GREAT CIRCLE DISTANCES**

S. 35°-39°

Latitude of Destination	Change of Longitude						Latitude of Destination
	5° 10° 15°	20° 25° 30°	35° 40° 45°	50° 55° 60°	65° 70° 75°	80° 85° 90°	
N. 60°	0 1 2	5 8 12	17 24 33	44 57 72	92 113 139	168 201 238	S. 60°
55	0 1 2	4 6 10	15 21 30	40 52 67	85 106 131	159 191 229	55
50	0 1 1	3 5 8	13 19 26	36 48 62	79 99 123	150 182 218	50
45	0 0 1	2 4 7	11 17 24	33 44 57	74 93 115	141 172 206	45
40	0 0 1	2 4 6	10 15 22	30 41 53	68 86 108	132 161 194	40
N. 35	0 0 1	2 3 6	9 14 20	28 38 49	63 80 100	123 150 182	S. 35
30	0 0 1	2 3 6	9 13 19	26 35 46	59 74 92	114 139 168	30
25	0 0 1	2 3 5	8 12 17	24 32 42	54 68 85	104 127 154	25
20	0 0 1	2 3 5	8 11 16	22 29 38	49 62 77	94 115 140	20
15	0 0 1	2 3 5	7 10 15	20 26 34	44 55 69	84 103 125	15
N. 10	0 0 1	2 3 4	7 10 13	18 24 30	39 49 60	74 91 110	S. 10
N. 5	0 0 1	2 3 4	6 9 12	16 21 27	34 42 52	64 78 95	S. 5
0	0 0 1	1 2 4	5 8 10	14 18 23	29 36 45	55 66 80	0
S. 5	0 0 1	1 2 3	5 6 9	12 15 19	24 30 37	45 55 66	N. 5
10	0 0 1	1 2 3	4 5 7	10 12 16	20 24 30	37 44 53	10
S. 15	0 0 0	1 2 2	3 4 6	8 10 13	16 19 24	29 35 42	N. 15
20	0 0 0	1 1 2	3 4 5	6 8 10	12 15 18	22 27 32	20
25	0 0 0	1 1 2	2 3 4	5 6 8	10 12 14	17 21 25	25
30	0 0 0	1 1 1	2 3 3	4 6 7	8 10 12	15 17 20	30
35	0 0 0	1 1 1	2 3 4	5 6 7	8 10 12	14 17 20	35
S. 40	0 0 0	1 1 2	2 3 4	5 7 8	10 12 15	17 20 23	N. 40
45	0 0 1	1 2 2	3 5 6	8 9 12	14 17 20	24 28 32	45
50	0 0 1	2 2 4	5 7 9	11 14 17	20 25 29	34 40 47	50
55	0 1 1	2 4 5	7 10 13	16 20 25	30 36 43	50 59 69	55
S. 60	0 1 2	3 5 8	11 14 18	23 29 35	43 51 60	71 84 98	N. 60

This table gives the difference, in nautical miles, between the distance from one place to another by the Rhumb Line track and the distance by the Great Circle track. It is based on a *Latitude of Departure* of 37°, but may be used for any place of departure between latitudes 35° and 39°. Of the two argument columns headed *Latitude of Destination*, the one on the left is to be used when the place of departure lies between N. 35° and N. 39°, and the one on the right when the place of departure lies between S. 35° and S. 39°.

The table is intended to give only the approximate difference of distance between the two tracks. For intermediate values of the arguments *Latitude of Destination* and *Change of Longitude*, the figures in the table should be interpolated by inspection. If the *Latitude of Departure* differs by the maximum of 2½° from that on which the table is based, the error in the result will not exceed 2 miles up to a *Change of Longitude* of 50°, but may reach 5 miles for a change of 70°, and 11 miles for a change of 90°.

Example.—Required the difference in distance between the Rhumb Line track and the Great Circle track from Lisbon (Lat. 38° 42' N., Long. 9° 08' W.) to Boston (Lat. 42° 21' N., Long. 71° 03' W.).

Entering the argument column on the left with the *Latitude of Destination* of 42° 21' N., and interpolating by inspection for the *Change of Longitude* of 61° 55', it will be seen that the difference in distance is about 60 nautical miles.

VI.—ADJUSTMENT TO REFRACTION IN SPECIAL CONDITIONS

Height in feet	Observed Altitude						Height in metres
	10°	15°	20°	30°	45°	60°	
0	-1	0	0	0	0	0	0
5000	0	0	0	0	0	0	1500
10000	+1	0	0	0	0	0	3000
15000	1	+1	+1	0	0	0	4600
20000	2	1	1	+1	0	0	6100
25000	2	1	1	1	0	0	7600
30000	3	2	1	1	0	0	9100
35000	3	2	1	1	+1	0	10700
40000	+3	+2	+2	+1	+1	0	12200

This table gives the additional correction for refraction to be applied to the *observed* altitude beyond that already included in the altitude tabulated in the main tables. It is only intended for use by an observer at great heights when special accuracy is required.

VII.—TRUE AZIMUTH OF THE POLE STAR

1940-1960		1960-1980		1980-2000	
L.H.A. °	True Azi- muth	L.H.A. °	True Azi- muth	L.H.A. °	True Azi- muth
0	001	0	001	0	001
2	000	3	000	4	000
51	359	58	359	66	359
182	000	183	000	184	000
231	001	238	001	246	001
360	360	360	360	360	360

These tables give the True Azimuth of the Pole Star, over various periods of time, for an observer between latitudes N. 35° and N. 39°. The argument L.H.A.° is obtained from G.H.A.° by *subtracting west* longitude or *adding east* longitude.

VIII.—DIP OF THE SEA HORIZON

Height in feet	Height in metres	Height in feet	Height in metres	Height in feet	Height in metres	Height in feet	Height in metres	Height in feet	Height in metres	Height in feet	Height in metres
0	0	437	133	1700	520	3810	1160	6740	2050		
2	1	481	146	1790	546	3930	1200	6910	2100		
6	2	527	160	1880	573	4060	1230	7080	2160		
12	3	575	175	1970	600	4190	1270	7250	2210		
21	4	625	190	2060	628	4330	1320	7430	2260		
31	5	677	206	2150	657	4460	1360	7610	2320		
43	6	731	222	2250	686	4600	1400	7790	2370		
58	7	787	240	2340	716	4740	1440	7970	2420		
75	8	845	257	2440	746	4880	1480	8150	2480		
93	9	906	276	2550	777	5020	1530	8340	2540		
114	10	968	295	2650	809	5170	1570	8520	2590		
137	11	1030	314	2760	841	5320	1620	8710	2650		
162	12	1090	332	2860	874	5470	1660	8900	2710		
189	13	1160	352	2980	908	5620	1710	9100	2770		
218	14	1230	373	3090	942	5770	1760	9290	2830		
250	15	1310	399	3200	977	5930	1800	9490	2890		
283	16	1380	422	3320	1010	6090	1850	9690	2950		
318	17	1460	446	3440	1040	6250	1900	9890	3010		
356	18	1540	470	3560	1080	6410	1950	10100	3070		
395	19	1620	495	3680	1120	6580	2000	10300	3140		
437	20	1700	520	3810	1160	6740	2050	10500	3200		

This table gives the dip of the sea horizon, in minutes of arc, with argument height of eye of the observer in feet or in metres. It is only required when the altitude is measured from the sea horizon. The dip is to be *subtracted* from the observed altitude.

IX.—DISTANCE TO THE SEA HORIZON IN NAUTICAL MILES

Height in feet	Dist.	Height in metres	Height in feet	Dist.	Height in metres	Height in feet	Dist.	Height in metres	Height in feet	Dist.	Height in metres	Height in feet	Dist.	Height in metres	Height in feet	Dist.	Height in metres
0		0	287	20	87	1120	39	341	2500	58	762	4420	77	1340	6890	96	2100
1	1		317	21	96	1170	40	359	2580	59	788	4540	78	1380	7040	97	2140
4	2	1	349	22	106	1240	41	378	2670	60	815	4650	79	1420	7180	98	2190
9	3	2	382	23	116	1300	42	396	2760	61	843	4770	80	1450	7330	99	2230
15	4	4	417	24	127	1360	43	416	2850	62	871	4900	81	1490	7480	100	2280
22	5	6	453	25	138	1430	44	436	2950	63	900	5020	82	1530	7630	101	2320
31	6	9	491	26	149	1490	45	456	3040	64	929	5140	83	1560	7780	102	2370
42	7	12	531	27	161	1560	46	477	3140	65	958	5270	84	1600	7940	103	2420
54	8	16	571	28	174	1630	47	498	3240	66	988	5390	85	1640	8100	104	2460
68	9	20	614	29	187	1700	48	520	3340	67	1010	5520	86	1680	8250	105	2510
83	10	25	658	30	200	1770	49	543	3440	68	1050	5650	87	1720	8410	106	2560
100	11	30	703	31	214	1850	50	564	3540	69	1080	5780	88	1760	8570	107	2610
118	12	36	750	32	228	1920	51	587	3650	70	1110	5920	89	1800	8730	108	2660
137	13	42	798	33	243	2000	52	611	3750	71	1140	6050	90	1840	8900	109	2710
158	14	48	848	34	258	2080	53	635	3860	72	1170	6190	91	1880	9060	110	2760
181	15	55	900	35	274	2160	54	659	3970	73	1210	6330	92	1920	9230	111	2810
205	16	62	953	36	290	2240	55	684	4080	74	1240	6460	93	1970	9400	112	2860
231	17	70	1000	37	307	2320	56	709	4190	75	1270	6610	94	2010	9560	113	2910
258	18	78	1060	38	324	2410	57	735	4310	76	1310	6750	95	2050	9740	114	2960
287	19	87	1120	39	341	2500		762	4420		1340	6890		2100	9910		3020

IX.—DISTANCE TO THE SEA HORIZON IN STATUTE MILES

Height in feet	Dist.	Height in metres	Height in feet	Dist.	Height in metres	Height in feet	Dist.	Height in metres	Height in feet	Dist.	Height in metres	Height in feet	Dist.	Height in metres	Height in feet	Dist.	Height in metres
0		0	288	23	87	1120	45	344	2520	67	768	4460	89	1360	6960	111	2120
1	1		314	24	95	1180	46	359	2590	68	791	4560	90	1390	7080	112	2160
3	2	1	342	25	104	1230	47	375	2670	69	815	4670	91	1420	7210	113	2190
6	3	2	370	26	113	1280	48	392	2750	70	839	4770	92	1450	7340	114	2230
11	4	3	400	27	122	1340	49	408	2830	71	863	4870	93	1480	7470	115	2270
17	5	5	431	28	131	1390	50	425	2910	72	888	4980	94	1510	7600	116	2310
24	6	7	463	29	141	1450	51	443	2990	73	913	5090	95	1550	7730	117	2350
32	7	9	496	30	151	1510	52	460	3080	74	938	5200	96	1580	7870	118	2390
41	8	12	530	31	161	1570	53	479	3160	75	964	5310	97	1610	8000	119	2440
51	9	15	565	32	172	1630	54	497	3250	76	990	5420	98	1650	8140	120	2480
62	10	19	602	33	183	1690	55	516	3330	77	1010	5530	99	1680	8280	121	2520
75	11	22	639	34	195	1750	56	535	3420	78	1040	5640	100	1720	8410	122	2560
89	12	27	678	35	206	1820	57	554	3510	79	1070	5750	101	1750	8550	123	2600
103	13	31	718	36	219	1880	58	574	3600	80	1090	5870	102	1790	8690	124	2650
119	14	36	759	37	231	1950	59	594	3690	81	1120	5990	103	1820	8830	125	2690
137	15	41	801	38	244	2010	60	615	3780	82	1150	6100	104	1860	8980	126	2730
155	16	47	845	39	257	2080	61	636	3880	83	1180	6220	105	1890	9120	127	2780
174	17	53	889	40	271	2150	62	657	3970	84	1210	6340	106	1930	9270	128	2820
195	18	59	935	41	285	2220	63	678	4070	85	1240	6460	107	1970	9410	129	2870
216	19	66	982	42	299	2290	64	700	4160	86	1270	6580	108	2000	9560	130	2910
239	20	73	1030	43	313	2370	65	723	4260	87	1300	6710	109	2040	9710	131	2960
263	21	80	1070	44	328	2440	66	745	4360	88	1330	6830	110	2080	9860	132	3000
288	22	87	1120	45	344	2520		768	4460		1360	6960		2120	10000	133	3050

These tables give the distance to the sea horizon, in nautical miles and in statute miles, with argument height of eye of the observer in feet or in metres.

At the moment when an object of known height is just appearing or disappearing over the sea horizon, its distance may be found by adding the distance corresponding to its height to the distance corresponding to the height of eye of the observer.

X.—TABLE OF RANGES IN NAUTICAL MILES

The tables below and on the opposite page give the distance, to the nearest 5 nautical miles, of an object, whose height is known and is *greater* than the height of the observer. The arguments of the table are the observed *angle of elevation* to the object, and the *difference in height* between the object and the observer, expressed in feet or in metres.

Example.—An observer, whose height is 1,500 feet, finds that the angle of elevation to the summit of a mountain, whose height is known to be 7,000 feet, is $0^{\circ} 48'$. Required the distance away of the mountain.

The difference in height between the mountain and the observer is $7,000 - 1,500 = 5,500$ feet. Entering on the opposite page the column headed $0^{\circ} 50'$ (the nearest tabulated value to $0^{\circ} 48'$), and choosing the left-hand of the two argument columns since the height is measured in feet, it is seen that 5,500 lies in the interval between 5,130 and 5,910, so that the distance of the mountain, to the nearest 5 miles, is 45 nautical miles.

The tables on pages 226 to 228 give the distance of an object, whose height is known, and is *less* than the height of the observer. The arguments of the table are the observed *angle of depression* to the object, and the *difference in height* between the observer and the object, expressed in feet or in metres. The distance is given to the nearest mile up to 10 nautical miles, and to the nearest 5 miles from 10 to 60 nautical miles.

Example.—An observer, whose height is 1,500 metres, finds that the angle of depression to a ship is $5^{\circ} 37'$. Required the distance away of the ship.

Entering on page 228 the column headed $5^{\circ} 30'$, and choosing the right-hand of the two argument columns, it is seen that 1,500 is an exact tabulated value, so that the distance away of the ship is 8 nautical miles.

On page 226, figures in *italics* represent the difference in height, *when the object observed is beyond the sea horizon*. If it is uncertain whether the object is beyond the horizon or not, and the two parts of the table give widely different results, there should be no doubt which is the correct one, while in doubtful cases the error will not be serious.

These tables are intended to give only the approximate range. They should prove a more reliable guide for large angles of elevation and depression than for small ones.

Height of object *greater* than height of observer

Angle of elevation																	
4° 00'			3° 40'			3° 20'			3° 00'			2° 40'			2° 20'		
Height in feet	Range	Height in metres	Height in feet	Range	Height in metres	Height in feet	Range	Height in metres	Height in feet	Range	Height in metres	Height in feet	Range	Height in metres	Height in feet	Range	Height in metres
0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
1060	5	325	978	5	298	890	5	271	801	5	244	712	5	217	624	5	190
3230	10	985	2960	10	904	2690	10	822	2430	10	741	2160	10	660	1900	10	579
5430	15	1650	4990	15	1520	4540	15	1380	4100	15	1250	3650	15	1110	3210	15	980
7670	20	2330	7050	20	2140	6430	20	1960	5810	20	1770	5190	20	1580	4570	20	1390
9950	25	3030	9150	25	2790	8350	25	2540	7550	25	2300	6750	25	2050	5960	25	1810
12200	30	3740	11200	30	3440	10300	30	3140	9340	30	2840	8360	30	2540	7390	30	2250
14600	35	4450	13400	35	4100	12300	35	3750	11100	35	3400	10000	35	3050	8850	35	2690
17000	40	5180	15600	40	4780	14300	40	4370	13000	40	3960	11600	40	3560	10300	40	3150
19400	45	5920	17900	45	5460	16400	45	5000	14900	45	4540	13400	45	4080	11900	45	3620
21900	50	6680	20200	50	6160	18500	50	5650	16800	50	5130	15100	50	4620	13400	50	4110
24400	55	7440	22500	55	6870	20600	55	6300	18800	55	5730	16900	55	5170	15100	55	4600
26900	60	8210	24900	60	7590	22800	60	6970	20800	60	6350	18800	60	5730	16700	60	5100
29500		9000	27300		8320	25100		7650	22800		6970	20600		6300	18400		5620

X.—TABLE OF RANGES IN NAUTICAL MILES
Height of object *greater* than height of observer

Angle of elevation

2° 00'			1° 50'			1° 40'			1° 30'			1° 20'			1° 10'		
Height in feet	Range	Height in metres	Height in feet	Range	Height in metres	Height in feet	Range	Height in metres	Height in feet	Range	Height in metres	Height in feet	Range	Height in metres	Height in feet	Range	Height in metres
0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
535	0	163	491	0	149	447	0	136	402	0	122	358	0	109	314	0	95
1630	5	498	1500	5	458	1370	5	417	1230	5	377	1100	5	336	971	5	296
2770	10	845	2550	10	777	2330	10	710	2100	10	643	1880	10	575	1660	10	508
3940	15	1200	3630	15	1100	3320	15	1010	3020	15	920	2710	15	826	2400	15	731
5160	20	1570	4760	20	1450	4360	20	1330	3960	20	1200	3570	20	1080	3170	20	966
6410	25	1950	5920	25	1800	5440	25	1650	4950	25	1510	4460	25	1360	3980	25	1210
7700	30	2340	7130	30	2170	6550	30	1990	5970	30	1820	5400	30	1640	4820	30	1470
9030	35	2750	8360	35	2550	7700	35	2340	7040	35	2140	6370	35	1940	5710	35	1740
10400	40	3160	9640	40	2940	8890	40	2710	8140	40	2480	7390	40	2250	6630	40	2020
11800	45	3590	10900	45	3340	10100	45	3080	9280	45	2820	8440	45	2570	7590	45	2310
13200	50	4030	12300	50	3750	11300	50	3470	10400	50	3180	9520	50	2900	8590	50	2620
14700	55	4480	13700	55	4170	12600	55	3860	11600	55	3550	10600	55	3240	9630	55	2930
16200	60	4950	15100	60	4610	14000	60	4270	12900	60	3930	11800	60	3600	10700	60	3260

Angle of elevation

1° 00'			0° 55'			0° 50'			0° 45'			0° 40'			0° 35'		
Height in feet	Range	Height in metres	Height in feet	Range	Height in metres	Height in feet	Range	Height in metres	Height in feet	Range	Height in metres	Height in feet	Range	Height in metres	Height in feet	Range	Height in metres
0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
270	0	82	247	0	75	225	0	68	203	0	62	181	0	55	159	0	48
839	5	255	772	5	235	706	5	215	640	5	195	573	5	174	507	5	154
1440	10	440	1330	10	406	1220	10	373	1110	10	339	1000	10	305	893	10	272
2090	15	637	1930	15	590	1780	15	542	1620	15	495	1470	15	448	1310	15	401
2770	20	845	2570	20	784	2370	20	724	2170	20	663	1970	20	602	1770	20	542
3490	25	1060	3250	25	991	3000	25	916	2760	25	842	2520	25	768	2270	25	694
4250	30	1290	3960	30	1200	3670	30	1120	3390	30	1030	3100	30	945	2810	30	858
5050	35	1530	4710	35	1430	4380	35	1330	4050	35	1230	3720	35	1130	3390	35	1030
5880	40	1790	5500	40	1670	5130	40	1560	4750	40	1450	4380	40	1330	4000	40	1220
6750	45	2060	6330	45	1930	5910	45	1800	5490	45	1670	5070	45	1540	4650	45	1410
7670	50	2330	7200	50	2190	6740	50	2050	6270	50	1910	5810	50	1770	5340	50	1620
8610	55	2620	8100	55	2470	7600	55	2310	7090	55	2160	6580	55	2000	6070	55	1850
9600	60	2920	9050	60	2750	8500	60	2590	7940	60	2420	7390	60	2250	6840	60	2080

Angle of elevation

0° 30'			0° 25'			0° 20'			0° 15'			0° 10'			0° 05'		
Height in feet	Range	Height in metres	Height in feet	Range	Height in metres	Height in feet	Range	Height in metres	Height in feet	Range	Height in metres	Height in feet	Range	Height in metres	Height in feet	Range	Height in metres
0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
137	0	41	115	0	35	93	0	28	71	0	21	48	0	14	26	0	8
440	5	134	374	5	114	308	5	93	241	5	73	175	5	53	109	5	33
782	10	238	671	10	204	561	10	171	450	10	137	339	10	103	229	10	69
1160	15	354	1000	15	306	852	15	259	697	15	212	542	15	165	387	15	118
1570	20	481	1380	20	420	1180	20	360	982	20	299	783	20	238	584	20	178
2030	25	620	1790	25	546	1540	25	471	1300	25	397	1060	25	323	818	25	249
2520	30	770	2240	30	683	1950	30	595	1660	30	507	1370	30	420	1090	30	332
3060	35	932	2720	35	831	2390	35	730	2060	35	629	1730	35	528	1400	35	427
3620	40	1100	3250	40	991	2870	40	877	2500	40	762	2120	40	648	1750	40	533
4230	45	1290	3810	45	1160	3390	45	1030	2970	45	907	2550	45	779	2130	45	651
4880	50	1480	4410	50	1340	3950	50	1200	3480	50	1060	3020	50	922	2560	50	780
5560	55	1690	5050	55	1540	4540	55	1380	4040	55	1230	3530	55	1070	3020	55	921
6280	60	1910	5730	60	1740	5180	60	1570	4620	60	1410	4070	60	1240	3520	60	1070

X.—TABLE OF RANGES IN NAUTICAL MILES
Height of object *less* than height of observer

Angle of depression																	
0° 05'			0° 10'			0° 15'			0° 20'			0° 25'			0° 30'		
Height in feet	Range	Height in metres	Height in feet	Range	Height in metres	Height in feet	Range	Height in metres	Height in feet	Range	Height in metres	Height in feet	Range	Height in metres	Height in feet	Range	Height in metres
0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
4	0	1	9	0	2	13	0	4	17	0	5	21	0	6	26	0	8
11	1	3	24	1	7	38	1	11	51	1	15	64	1	19	77	1	23
17	2	5	39	2	12	61	2	18	83	2	25	106	2	32	127	2	39
21	3	6	52	3	15	83	3	25	114	3	34	145	3	44	176	3	53
24	4	7	64	4	19	103	4	31	143	4	43	183	4	55	223	4	68
25	5	8	74	5	22	122	5	37	171	5	52	220	5	67	268	5	81
26	6	8	82	6	25	140	6	42	197	6	60	255	6	77	312	6	95
24	7	8	89	7	27	156	7	47	222	7	67	288	7	88	355	7	108
21	8	7	95	8	29	170	8	52	245	8	74	320	8	97	396	8	120
16	9	5	99	9	30	183	9	55	267	9	81	351	9	107	435	9	132
0	10	0	103	10	32	212	10	64	323	10	98	434	10	132	544	10	166
			77	15	24	231	15	70	386	15	117	541	15	164	695	15	212
			13	20	4	213	20	65	411	20	125	609	20	185	808	20	246
			0	25	0	155	25	48	398	25	122	640	25	195	884	25	269
						59	30	18	346	30	106	634	30	194	921	30	280
						0	35	0	258	35	79	590	35	180	921	35	281
									130	40	40	506	40	155	882	40	269
									0	45	0	385	45	118	805	45	246
												226	50	69	690	50	211
												28	55	9	537	55	164
												0	60	0	346	60	106

Angle of depression																	
0° 35'			0° 40'			0° 45'			0° 50'			0° 55'			1° 00'		
Height in feet	Range	Height in metres	Height in feet	Range	Height in metres	Height in feet	Range	Height in metres	Height in feet	Range	Height in metres	Height in feet	Range	Height in metres	Height in feet	Range	Height in metres
0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
30	0	9	35	0	10	39	0	12	44	0	13	48	0	14	52	0	16
91	1	27	104	1	31	117	1	35	130	1	39	144	1	43	157	1	47
150	2	45	172	2	52	194	2	59	216	2	65	238	2	72	260	2	79
207	3	63	238	3	72	269	3	82	300	3	91	331	3	100	362	3	110
263	4	80	302	4	92	342	4	104	382	4	116	422	4	128	462	4	140
317	5	96	366	5	111	414	5	126	463	5	141	512	5	156	560	5	170
370	6	112	427	6	130	485	6	147	542	6	165	600	6	182	657	6	200
421	7	128	488	7	148	554	7	168	620	7	189	687	7	209	753	7	229
471	8	143	546	8	166	621	8	189	696	8	212	772	8	235	847	8	258
519	9	158	603	9	183	687	9	209	771	9	235	855	9	260	939	9	286
655	10	199	765	10	233	876	10	267	986	10	300	1090	10	334	1200	10	368
850	15	259	1000	15	306	1160	15	353	1310	15	400	1470	15	448	1620	15	495
1000	20	307	1200	20	367	1400	20	428	1600	20	489	1800	20	549	2000	20	610
1120	25	343	1370	25	417	1610	25	491	1850	25	566	2100	25	640	2340	25	714
1200	30	368	1490	30	456	1780	30	543	2070	30	631	2350	30	719	2640	30	806
1250	35	381	1580	35	482	1910	35	583	2240	35	685	2570	35	786	2910	35	887
1260	40	384	1630	40	497	2000	40	612	2380	40	727	2760	40	841	3130	40	956
1230	45	374	1650	45	502	2060	45	629	2480	45	757	2900	45	885	3320	45	1010
1160	50	352	1620	50	494	2080	50	634	2540	50	776	3010	50	918	3470	50	1050
1050	55	319	1560	55	474	2070	55	629	2570	55	783	3080	55	938	3580	55	1090
899	60	274	1460	60	443	2010	60	611	2560	60	780	3110	60	947	3660	60	1110

For explanation, see page 224.

X.—TABLE OF RANGES IN NAUTICAL MILES

Height of object *less* than height of observer

Angle of depression																	
1° 10'			1° 20'			1° 30'			1° 40'			1° 50'			2° 00'		
Height in feet	Range	Height in metres	Height in feet	Range	Height in metres	Height in feet	Range	Height in metres	Height in feet	Range	Height in metres	Height in feet	Range	Height in metres	Height in feet	Range	Height in metres
0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
61	1	18	70	1	21	79	1	24	88	1	26	97	1	29	106	1	32
183	2	56	210	2	64	237	2	72	263	2	80	290	2	88	316	2	96
305	3	92	349	3	106	393	3	119	437	3	133	481	3	146	526	3	160
424	4	129	486	4	148	548	4	167	610	4	185	672	4	204	734	4	223
541	5	165	621	5	189	701	5	213	780	5	238	860	5	262	940	5	286
658	6	200	755	6	230	852	6	259	950	6	289	1040	6	319	1140	6	349
772	7	235	887	7	270	1000	7	305	1110	7	340	1230	7	375	1340	7	410
886	8	270	1010	8	310	1150	8	351	1280	8	391	1410	8	432	1550	8	472
997	9	304	1140	9	350	1290	9	395	1440	9	441	1590	9	487	1750	9	533
1100	10	337	1270	10	388	1440	10	440	1610	10	491	1780	10	542	1940	10	594
1430	15	435	1650	15	503	1870	15	570	2090	15	638	2310	15	705	2530	15	772
1930	20	589	2240	20	684	2550	20	778	2860	20	872	3170	20	967	3480	20	1066
2400	25	732	2790	25	853	3190	25	974	3590	25	1090	3990	25	1210	4390	25	1330
2830	30	862	3310	30	1010	3800	30	1150	4290	30	1300	4770	30	1450	5260	30	1600
3220	35	982	3790	35	1150	4370	35	1330	4940	35	1500	5520	35	1680	6090	35	1850
3570	40	1080	4230	40	1290	4900	40	1490	5560	40	1690	6230	40	1890	6890	40	2100
3880	45	1180	4640	45	1410	5390	45	1640	6140	45	1870	6890	45	2100	7650	45	2330
4160	50	1270	5000	50	1520	5840	50	1780	6680	50	2030	7530	50	2290	8370	50	2550
4400	55	1340	5330	55	1620	6260	55	1900	7190	55	2190	8120	55	2470	9050	55	2750
4600	60	1400	5620	60	1710	6640	60	2020	7660	60	2330	8670	60	2640	9690	60	2950
4760		1450	5870		1790	6980		2120	8080		2460	9190		2800	10300		3140

Angle of depression																	
2° 20'			2° 40'			3° 00'			3° 20'			3° 40'			4° 00'		
Height in feet	Range	Height in metres	Height in feet	Range	Height in metres	Height in feet	Range	Height in metres	Height in feet	Range	Height in metres	Height in feet	Range	Height in metres	Height in feet	Range	Height in metres
0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
123	1	37	141	1	43	159	1	48	176	1	53	194	1	59	212	1	64
369	2	112	422	2	128	476	2	145	529	2	161	582	2	177	636	2	193
614	3	187	703	3	214	792	3	241	880	3	268	969	3	295	1050	3	322
858	4	261	982	4	299	1100	4	337	1230	4	375	1350	4	412	1470	4	450
1090	5	335	1250	5	383	1410	5	432	1570	5	481	1730	5	529	1890	5	578
1340	6	408	1530	6	467	1730	6	527	1920	6	586	2120	6	646	2310	6	706
1570	7	481	1800	7	551	2040	7	621	2270	7	692	2500	7	762	2730	7	832
1810	8	553	2080	8	634	2340	8	715	2610	8	796	2880	8	877	3140	8	959
2050	9	625	2350	9	717	2650	9	809	2950	9	901	3250	9	993	3560	9	1080
2280	10	696	2620	10	799	2950	10	902	3290	10	1000	3630	10	1100	3970	10	1210
2970	15	908	3420	15	1040	3860	15	1170	4300	15	1310	4750	15	1440	5190	15	1580
4100	20	1250	4720	20	1430	5340	20	1620	5960	20	1810	6580	20	2000	7200	20	2190
5190	25	1580	5980	25	1820	6780	25	2060	7580	25	2310	8380	25	2550	9180	25	2790
6230	30	1900	7210	30	2190	8180	30	2490	9160	30	2790	10100	30	3090	11100	30	3380
7250	35	2210	8400	35	2560	9550	35	2910	10700	35	3260	11800	35	3610	13000	35	3960
8220	40	2500	9550	40	2910	10800	40	3310	12200	40	3720	13500	40	4120	14800	40	4530
9150	45	2790	10600	45	3250	12100	45	3710	13600	45	4170	15100	45	4620	16700	45	5090
10000	50	3060	11700	50	3570	13400	50	4090	15100	50	4600	16700	50	5120	18400	50	5630
10900	55	3320	12700	55	3890	14600	55	4460	16400	55	5020	18300	55	5590	20200	55	6160
11700	60	3570	13700	60	4190	15800	60	4810	17800	60	5440	19900	60	6060	21900	60	6680
12500		3810	14700		4490	16900		5160	19100		5840	21300		6510	23600		7190

For explanation, see page 224.

X.—TABLE OF RANGES IN NAUTICAL MILES

Height of object *less* than height of observer

Angle of depression																	
4° 30'			5° 00'			5° 30'			6° 00'			6° 30'			7° 00'		
Height in feet	Range	Height in metres	Height in feet	Range	Height in metres	Height in feet	Range	Height in metres	Height in feet	Range	Height in metres	Height in feet	Range	Height in metres	Height in feet	Range	Height in metres
0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
238	0	72	265	0	81	292	0	89	319	0	97	346	0	105	373	0	113
716	1	218	796	1	242	876	1	267	956	1	291	1030	1	316	1110	1	340
1190	2	363	1320	2	404	1450	2	444	1590	2	485	1720	2	526	1860	2	567
1660	3	507	1850	3	564	2040	3	621	2220	3	679	2410	3	736	2600	3	793
2130	4	651	2370	4	725	2610	4	798	2860	4	872	3100	4	945	3340	4	1010
2600	5	795	2900	5	885	3190	5	974	3490	5	1060	3780	5	1150	4080	5	1240
3070	6	938	3420	6	1040	3770	6	1150	4120	6	1250	4470	6	1360	4820	6	1460
3540	7	1080	3940	7	1200	4340	7	1320	4750	7	1440	5150	7	1570	5550	7	1690
4010	8	1220	4460	8	1360	4920	8	1500	5370	8	1630	5830	8	1770	6290	8	1910
4470	9	1360	4980	9	1510	5490	9	1670	6000	9	1830	6510	9	1980	7020	9	2140
5860	10	1780	6530	10	1990	7200	10	2190	7870	10	2390	8540	10	2600	9210	10	2800
8140	15	2480	9070	15	2760	10000	15	3050	10900	15	3330	11800	15	3620	12800	15	3910
10300	20	3160	11500	20	3530	12700	20	3890	14000	20	4260	15200	20	4630	16400	20	5000
12500	25	3830	14000	25	4280	15500	25	4730	16900	25	5180	18400	25	5630	19900	25	6080
14700	30	4490	16400	30	5020	18200	30	5550	19900	30	6080	21700	30	6620	23400	30	7150
16800	35	5140	18800	35	5750	20800	35	6360	22800	35	6980	24900	35	7590	26900	35	8210
18900	40	5780	21200	40	6470	23500	40	7160	25800	40	7860	28000	40	8550	30300	40	9250
21000	45	6400	23500	45	7180	26000	45	7950	28600	45	8730	31100	45	9510	33700	45	10200
23000	50	7020	25800	50	7870	28600	50	8730	31400	50	9590	34200	50	10400	37100	50	11300
25000	55	7620	28000	55	8550	31100	55	9490	34200	55	10400	37300	55	11300	40400	55	12300
26900	60	8210	30200	60	9230	33600	60	10200	36900	60	11200	40300	60	12200	43600	60	13300

Angle of depression																	
7° 30'			8° 00'			8° 30'			9° 00'			9° 30'			10° 00'		
Height in feet	Range	Height in metres	Height in feet	Range	Height in metres	Height in feet	Range	Height in metres	Height in feet	Range	Height in metres	Height in feet	Range	Height in metres	Height in feet	Range	Height in metres
0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
399	0	121	427	0	130	454	0	138	481	0	146	508	0	154	535	0	163
1190	1	365	1270	1	390	1360	1	415	1440	1	439	1520	1	464	1600	1	489
1990	2	608	2130	2	649	2260	2	691	2400	2	732	2540	2	774	2670	2	815
2790	3	851	2980	3	909	3170	3	966	3360	3	1020	3550	3	1080	3740	3	1140
3580	4	1090	3830	4	1160	4070	4	1240	4310	4	1310	4560	4	1390	4810	4	1460
4380	5	1330	4670	5	1420	4970	5	1510	5270	5	1600	5570	5	1690	5870	5	1790
5170	6	1570	5520	6	1680	5870	6	1790	6220	6	1890	6580	6	2000	6930	6	2110
5960	7	1810	6360	7	1940	6770	7	2060	7180	7	2180	7580	7	2310	8000	7	2430
6750	8	2050	7210	8	2190	7670	8	2330	8130	8	2470	8590	8	2610	9060	8	2760
7530	9	2290	8050	9	2420	8560	9	2610	9080	9	2760	9600	9	2920	10100	9	3080
9880	10	3010	10500	10	3220	11200	10	3420	11900	10	3630	12600	10	3840	13200	10	4050
13700	15	4200	14700	15	4480	15600	15	4770	16600	15	5060	17500	15	5350	18500	15	5640
17600	20	5370	18800	20	5740	20000	20	6110	21200	20	6480	22500	20	6860	23700	20	7230
21400	25	6530	22900	25	6980	24400	25	7440	25900	25	7890	27400	25	8350	28900	25	8810
25200	30	7680	26900	30	8220	28700	30	8760	30500	30	9290	32200	30	9830	34000	30	10300
28900	35	8820	30900	35	9440	33000	35	10000	35000	35	10600	37000	35	11300	39100	35	11900
32600	40	9950	34900	40	10600	37200	40	11300	39500	40	12000	41800	40	12700	44200	40	13400
36300	45	11000	38800	45	11800	41400	45	12600	44000	45	13400	46600	45	14200	49200	45	15000
39900	50	12100	42700	50	13000	45600	50	13900	48400	50	14700	51300	50	15600	54200	50	16500
43500	55	13200	46600	55	14200	49700	55	15100	52800	55	16100	56000	55	17000	59100	55	18000
47000	60	14300	50400	60	15300	53800	60	16400	57200	60	17400	60600	60	18400	64000	60	19500

For explanation, see page 224.

XI.—TEMPERATURE CONVERSION **FAHRENHEIT AND CENTIGRADE**

°F	°C	°F	°C	°F	°C	°F	°C	°F	°C	°F	°C	°F	°C
-52	-46	-14	-25	+23	-4	+61	+17	+99	+38	+137	+59	+175	+80
50	45	13	24	25	3	63	18	101	39	139	60	176	81
49	44	11	23	27	2	65	19	103	40	140	61	178	82
47	43	9	22	29	-1	67	20	104	41	142	62	180	83
45	42	7	21	31	0	68	21	106	42	144	63	182	84
43	41	5	20	32	+1	70	22	108	43	146	64	184	85
41	40	4	19	34	2	72	23	110	44	148	65	185	86
40	39	-2	18	36	3	74	24	112	45	149	66	187	87
38	38	0	17	38	4	76	25	113	46	151	67	189	88
36	37	+2	16	40	5	77	26	115	47	153	68	191	89
34	36	4	15	41	6	79	27	117	48	155	69	193	90
32	35	5	14	43	7	81	28	119	49	157	70	194	91
31	34	7	13	45	8	83	29	121	50	158	71	196	92
29	33	9	12	47	9	85	30	122	51	160	72	198	93
27	32	11	11	49	10	86	31	124	52	162	73	200	94
25	31	13	10	50	11	88	32	126	53	164	74	202	95
23	30	14	9	52	12	90	33	128	54	166	75	203	96
22	29	16	8	54	13	92	34	130	55	167	76	205	97
20	28	18	7	56	14	94	35	131	56	169	77	207	98
18	27	20	6	58	15	95	36	133	57	171	78	209	99
16	26	22	5	59	+16	97	+37	135	+58	173	+79	211	+100
-14	-26	+23	-5	+61		+99		+137		+175		+212	

XII.—CONVERSION FACTORS

Conversion	Ratio	Factor	Reciprocal
DISTANCE			
Statute Miles to Nautical Miles	66 to 76	0.8684	1.1515
Statute Miles „ Kilometres	66 „ 41	1.6093	0.6214
Nautical Miles „ Kilometres	76 „ 41	1.8531	0.5396
Feet „ Metres	25 „ 82	0.3048	3.2808
Yards „ Metres	32 „ 35	0.9144	1.0936
Fathoms „ Feet	6 „ 1	6.0	0.1667
SPEED			
Miles per hour to Knots	66 to 76	0.8684	1.1515
Miles per hour „ Metres per second	38 „ 85	0.4470	2.2369
Knots „ Metres per second	35 „ 68	0.5148	1.9426
Miles per hour „ Feet per second	22 „ 15	1.4667	0.6818
LIQUID MEASURE			
Gallons to Litres	50 to 11	4.5460	0.2200
WEIGHT			
Pounds to Kilograms	44 to 97	0.4536	2.2046
PRESSURE			
Inches of Mercury to Millibars	2100 to 62	33.87	0.02953

XIII.—CONVERSION OF TIME TO ARC

For Intervals of 10 ^m						Interpolation Table											
^h m	^s °	^h m	^s °	^h m	^s °	^m °	^s °	^m °	^s °	^m °	^s °	^m °	^s °	^m °	^s °	^m °	^s °
00 00	0 00	08 00	120 00	16 00	240 00	00 00	0 00	03 17	0 50	06 37	1 40						
10	2 30	10	122 30	10	242 30	02	0 01	22	0 51	42	1 41						
20	5 00	20	125 00	20	245 00	05	0 02	25	0 52	45	1 42						
30	7 30	30	127 30	30	247 30	10	0 03	30	0 53	50	1 43						
40	10 00	40	130 00	40	250 00	13	0 04	33	0 54	53	1 44						
50	12 30	50	132 30	50	252 30	18	0 05	38	0 55	58	1 45						
						21	0 06	41	0 56	01	1 46						
01 00	15 00	09 00	135 00	17 00	255 00	26	0 07	46	0 57	06	1 47						
10	17 30	10	137 30	10	257 30	29	0 08	49	0 58	09	1 48						
20	20 00	20	140 00	20	260 00	34	0 09	54	0 59	14	1 49						
30	22 30	30	142 30	30	262 30	37	0 10	57	1 00	17	1 50						
40	25 00	40	145 00	40	265 00	42	0 11	02	1 01	22	1 51						
50	27 30	50	147 30	50	267 30	45	0 12	05	1 02	25	1 52						
						50	0 13	10	1 03	30	1 53						
02 00	30 00	10 00	150 00	18 00	270 00	53	0 14	13	1 04	33	1 54						
10	32 30	10	152 30	10	272 30	58	0 15	18	1 05	38	1 55						
20	35 00	20	155 00	20	275 00	01	0 16	21	1 06	41	1 56						
30	37 30	30	157 30	30	277 30	06	0 17	26	1 07	46	1 57						
40	40 00	40	160 00	40	280 00	09	0 18	29	1 08	49	1 58						
50	42 30	50	162 30	50	282 30	14	0 19	34	1 09	54	1 59						
						17	0 20	37	1 10	57	2 00						
03 00	45 00	11 00	165 00	19 00	285 00	22	0 21	42	1 11	02	2 01						
10	47 30	10	167 30	10	287 30	25	0 22	45	1 12	05	2 02						
20	50 00	20	170 00	20	290 00	30	0 23	50	1 13	10	2 03						
30	52 30	30	172 30	30	292 30	33	0 24	53	1 14	13	2 04						
40	55 00	40	175 00	40	295 00	38	0 25	58	1 15	18	2 05						
50	57 30	50	177 30	50	297 30	41	0 26	01	1 16	21	2 06						
						46	0 27	06	1 17	26	2 07						
04 00	60 00	12 00	180 00	20 00	300 00	49	0 28	09	1 18	29	2 08						
10	62 30	10	182 30	10	302 30	54	0 29	14	1 19	34	2 09						
20	65 00	20	185 00	20	305 00	57	0 30	17	1 20	37	2 10						
30	67 30	30	187 30	30	307 30	02	0 31	22	1 21	42	2 11						
40	70 00	40	190 00	40	310 00	05	0 32	25	1 22	45	2 12						
50	72 30	50	192 30	50	312 30	10	0 33	30	1 23	50	2 13						
						13	0 34	33	1 24	53	2 14						
05 00	75 00	13 00	195 00	21 00	315 00	18	0 35	38	1 25	58	2 15						
10	77 30	10	197 30	10	317 30	21	0 36	41	1 26	01	2 16						
20	80 00	20	200 00	20	320 00	26	0 37	46	1 27	06	2 17						
30	82 30	30	202 30	30	322 30	29	0 38	49	1 28	09	2 18						
40	85 00	40	205 00	40	325 00	34	0 39	54	1 29	14	2 19						
50	87 30	50	207 30	50	327 30	37	0 40	57	1 30	17	2 20						
						42	0 41	02	1 31	22	2 21						
06 00	90 00	14 00	210 00	22 00	330 00	45	0 42	05	1 32	25	2 22						
10	92 30	10	212 30	10	332 30	50	0 43	10	1 33	30	2 23						
20	95 00	20	215 00	20	335 00	53	0 44	13	1 34	33	2 24						
30	97 30	30	217 30	30	337 30	58	0 45	18	1 35	38	2 25						
40	100 00	40	220 00	40	340 00	01	0 46	21	1 36	41	2 26						
50	102 30	50	222 30	50	342 30	06	0 47	26	1 37	46	2 27						
						09	0 48	29	1 38	49	2 28						
07 00	105 00	15 00	225 00	23 00	345 00	14	0 49	34	1 39	54	2 29						
10	107 30	10	227 30	10	347 30	17	0 50	37	1 40	57	2 30						
20	110 00	20	230 00	20	350 00	22		42		00							
30	112 30	30	232 30	30	352 30												
40	115 00	40	235 00	40	355 00												
50	117 30	50	237 30	50	357 30												

When the argument is an exact tabulated value, the upper of the two possible values of the result should be taken.

XIV.—CONVERSION OF ARC TO TIME

DEGREES												MINUTES	
°	'	°	'	°	'	°	'	°	'	°	'	°	'
0	00	60	4 00	120	8 00	180	12 00	240	16 00	300	20 00	0	00
1	04	61	4 04	121	8 04	181	12 04	241	16 04	301	20 04	1	04
2	08	62	4 08	122	8 08	182	12 08	242	16 08	302	20 08	2	08
3	12	63	4 12	123	8 12	183	12 12	243	16 12	303	20 12	3	12
4	16	64	4 16	124	8 16	184	12 16	244	16 16	304	20 16	4	16
5	20	65	4 20	125	8 20	185	12 20	245	16 20	305	20 20	5	20
6	24	66	4 24	126	8 24	186	12 24	246	16 24	306	20 24	6	24
7	28	67	4 28	127	8 28	187	12 28	247	16 28	307	20 28	7	28
8	32	68	4 32	128	8 32	188	12 32	248	16 32	308	20 32	8	32
9	36	69	4 36	129	8 36	189	12 36	249	16 36	309	20 36	9	36
10	40	70	4 40	130	8 40	190	12 40	250	16 40	310	20 40	10	40
11	44	71	4 44	131	8 44	191	12 44	251	16 44	311	20 44	11	44
12	48	72	4 48	132	8 48	192	12 48	252	16 48	312	20 48	12	48
13	52	73	4 52	133	8 52	193	12 52	253	16 52	313	20 52	13	52
14	56	74	4 56	134	8 56	194	12 56	254	16 56	314	20 56	14	56
15	1 00	75	5 00	135	9 00	195	13 00	255	17 00	315	21 00	15	1 00
16	1 04	76	5 04	136	9 04	196	13 04	256	17 04	316	21 04	16	1 04
17	1 08	77	5 08	137	9 08	197	13 08	257	17 08	317	21 08	17	1 08
18	1 12	78	5 12	138	9 12	198	13 12	258	17 12	318	21 12	18	1 12
19	1 16	79	5 16	139	9 16	199	13 16	259	17 16	319	21 16	19	1 16
20	1 20	80	5 20	140	9 20	200	13 20	260	17 20	320	21 20	20	1 20
21	1 24	81	5 24	141	9 24	201	13 24	261	17 24	321	21 24	21	1 24
22	1 28	82	5 28	142	9 28	202	13 28	262	17 28	322	21 28	22	1 28
23	1 32	83	5 32	143	9 32	203	13 32	263	17 32	323	21 32	23	1 32
24	1 36	84	5 36	144	9 36	204	13 36	264	17 36	324	21 36	24	1 36
25	1 40	85	5 40	145	9 40	205	13 40	265	17 40	325	21 40	25	1 40
26	1 44	86	5 44	146	9 44	206	13 44	266	17 44	326	21 44	26	1 44
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XV.—CORRECTION TO TABULATED ALTITUDE FOR MINUTES OF DECLINATION

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XV.—CORRECTION TO TABULATED ALTITUDE FOR MINUTES OF DECLINATION

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