

24°

DECLINATION SAME NAME AS LATITUDE

24°

LAT.	65°		66°		67°		68°		69°		LAT.
H.A.	Alt.	Az.	Alt.	Az.	Alt.	Az.	Alt.	Az.	Alt.	Az.	H.A.
45	39 56+55	123	39 23+56	123	38 50+56	124	38 16+56	125	37 42+56	125	315
46	39 34 55	122	39 03 55	122	38 30 56	123	37 57 57	124	37 24 57	124	314
47	39 13 55	120	38 42 55	121	38 11 55	122	37 39 56	122	37 06 57	123	313
48	38 51 54	119	38 21 55	120	37 51 55	121	37 20 56	121	36 48 57	122	312
49	38 28 55	118	38 00 55	119	37 30 56	120	37 00 56	120	36 30 56	121	311
50	38 06+55	117	37 38+55	118	37 10+55	119	36 41+56	119	36 11+57	120	310
51	37 43 55	116	37 17 55	117	36 49 56	118	36 21 56	118	35 52 57	119	309
52	37 21 54	115	36 55 55	116	36 28 56	116	36 01 56	117	35 34 56	118	308
53	36 57 55	114	36 33 54	115	36 07 55	115	35 41 56	116	35 14 57	117	307
54	36 34 54	113	36 10 55	114	35 46 55	114	35 21 56	115	34 55 56	116	306
55	36 11+54	112	35 48+55	113	35 25+55	113	35 00+56	114	34 36+56	115	305
56	35 47 54	111	35 25 55	112	35 03 55	112	34 40 55	113	34 16 56	114	304
57	35 24 53	110	35 03 54	111	34 41 55	111	34 19 56	112	33 56 56	113	303
58	35 00 54	109	34 40 54	110	34 19 55	110	33 58 56	111	33 36 56	112	302
59	34 36 53	108	34 17 54	109	33 57 55	109	33 37 55	110	33 16 56	111	301
60	34 11+54	107	33 54+54	108	33 35+55	108	33 16+55	109	32 56+56	110	300
61	33 47 54	106	33 30 54	107	33 13 54	107	32 55 55	108	32 36 56	109	299
62	33 23 53	105	33 07 54	106	32 50 55	106	32 33 55	107	32 15 56	108	298
63	32 58 54	104	32 43 54	105	32 28 54	105	32 12 55	106	31 55 55	107	297
64	32 34 53	103	32 20 54	104	32 05 55	104	31 50 55	105	31 34 56	106	296
65	32 09+53	102	31 56+54	103	31 42+55	103	31 28+55	104	31 14+55	105	295
66	31 44 53	101	31 32 54	102	31 20 54	102	31 06 55	103	30 53 55	104	294
67	31 19 53	100	31 08 54	101	30 57 54	101	30 45 54	102	30 32 55	103	293
68	30 54 53	99	30 44 54	100	30 34 54	100	30 23 54	101	30 11 55	102	292
69	30 29 53	98	30 20 54	99	30 11 54	99	30 00 55	100	29 50 55	101	291
70	30 04+53	97	29 56+54	98	29 47+55	99	29 38+55	99	29 29+55	100	290
71	29 39 53	96	29 32 54	97	29 24 55	98	29 16 55	98	29 07 56	99	289
72	29 14 53	96	29 08 53	96	29 01 54	97	28 54 55	97	28 46 55	98	288
73	28 49 53	95	28 43 54	95	28 38 54	96	28 32 54	96	28 25 55	97	287
74	28 23 53	94	28 19 54	94	28 14 55	95	28 09 55	95	28 03 56	96	286
75	27 58+53	93	27 55+53	93	27 51+54	94	27 47+54	94	27 42+55	95	285
76	27 33 53	92	27 30 54	92	27 28 54	93	27 24 55	93	27 21 55	94	284
77	27 07 53	91	27 06 54	91	27 04 54	92	27 02 55	92	26 59 55	93	283
78	26 42 53	90	26 42 53	91	26 41 54	91	26 40 54	92	26 38 55	92	282
79	26 17 53	89	26 17 54	90	26 18 54	90	26 17 55	91	26 16 55	91	281
80	25 51+53	88	25 53+54	89	25 54+54	89	25 55+54	90	25 55+55	90	280
81	25 26 53	87	25 29 53	88	25 31 54	88	25 32 55	89	25 33 55	89	279
82	25 01 53	86	25 04 54	87	25 07 54	87	25 10 54	88	25 12 55	88	278
83	24 36 53	86	24 40 54	86	24 44 54	86	24 47 55	87	24 50 55	87	277
84	24 10 53	85	24 16 53	85	24 21 54	86	24 25 55	86	24 29 55	86	276
85	23 45+53	84	23 51+54	84	23 57+54	85	24 03+54	85	24 08+55	86	275
86	23 20 53	83	23 27 54	83	23 34 54	84	23 40 55	84	23 46 55	85	274
87	22 55 53	82	23 03 54	82	23 11 54	83	23 18 55	83	23 25 55	84	273
88	22 30 53	81	22 39 54	82	22 47 55	82	22 56 54	82	23 03 56	83	272
89	22 05 53	80	22 15 54	81	22 24 55	81	22 33 55	81	22 42 55	82	271
90	21 40+53	79	21 51+54	80	22 01+55	80	22 11+55	81	22 21+55	81	270

In South { For argument H.A. on the left, True Azimuth = $180^\circ +$ Tabulated Azimuth. } See
 Latitudes { For argument H.A. on the right, True Azimuth = $180^\circ -$ Tabulated Azimuth. } p. 9

65°		66°		67°		68°		69°		LAT.
Alt.	Az.	Alt.	Az.	Alt.	Az.	Alt.	Az.	Alt.	Az.	H.A.
21 40+53	79	21 51+54	80	22 01+55	80	22 11+55	81	22 21+55	81	270
21 15 53	78	21 27 54	79	21 38 55	79	21 49 55	80	22 00 55	80	269
20 50 54	78	21 03 54	78	21 15 55	78	21 27 55	79	21 39 55	79	268
20 26 53	77	20 39 54	77	20 52 55	77	21 05 55	78	21 18 55	78	267
20 01 54	76	20 16 53	76	20 30 54	77	20 43 55	77	20 57 55	77	266
19 37+53	75	19 52+54	75	20 07+54	76	20 22+54	76	20 36+55	76	265
19 12 54	74	19 28 54	74	19 44 55	75	20 00 55	75	20 15 55	76	264
18 48 54	73	19 05 54	74	19 22 54	74	19 38 55	74	19 54 56	75	263
18 24 53	72	18 42 54	73	18 59 55	73	19 17 55	73	19 34 55	74	262
18 00 53	72	18 18 55	72	18 37 55	72	18 55 55	72	19 13 56	73	261
17 36+54	71	17 55+55	71	18 15+54	71	18 34+55	72	18 53+55	72	260
17 12 54	70	17 32 55	70	17 53 54	70	18 13 55	71	18 32 56	71	259
16 48 54	69	17 10 54	69	17 31 55	70	17 52 55	70	18 12 56	70	258
16 25 54	68	16 47 54	68	17 09 55	69	17 31 55	69	17 52 56	69	257
16 01 54	67	16 24 55	67	16 47 55	68	17 10 55	68	17 32 56	68	256
15 38+54	66	16 02+55	67	16 26+55	67	16 49+55	67	17 12+56	67	255
15 15 54	66	15 40 54	66	16 04 55	66	16 28 56	66	16 52 56	67	254
14 52 54	65	15 18 54	65	15 43 55	65	16 08 55	65	16 33 56	66	253
14 29 55	64	14 56 54	64	15 22 55	64	15 48 55	65	16 13 56	65	252
14 07 54	63	14 34 55	63	15 01 55	63	15 27 56	64	15 54 56	64	251
13 44+55	62	14 12+55	62	14 40+55	63	15 07+56	63	15 35+56	63	250
13 22 55	61	13 51 55	61	14 19 56	62	14 48 55	62	15 16 56	62	249
13 00 55	60	13 30 55	61	13 59 55	61	14 28 56	61	14 57 56	61	248
12 38 55	60	13 09 55	60	13 39 55	60	14 08 56	60	14 38 56	60	247
12 17 55	59	12 48 55	59	13 19 55	59	13 49 56	59	14 20 56	59	246
11 55+55	58	12 27+55	58	12 59+55	58	13 30+56	58	14 01+57	59	245
11 34 55	57	12 07 55	57	12 39 56	57	13 11 56	57	13 43 56	58	244
11 13 55	56	11 46 56	56	12 19 56	56	12 52 56	57	13 25 57	57	243
10 52 55	55	11 26 56	55	12 00 56	56	12 34 56	56	13 07 57	56	242
10 32 55	54	11 06 56	54	11 41 56	55	12 15 57	55	12 50 56	55	241
10 11+56	53	10 47+55	54	11 22+56	54	11 57+56	54	12 32+57	54	240
...		10 27 56	53	11 03 56	53	11 39 57	53	12 15 57	53	239
...		10 08+56	52	10 45 56	52	11 21 57	52	11 58 57	52	238
...		...		10 27 56	51	11 04 56	51	11 41 57	51	237
...		...		10 09+56	50	10 47 56	50	11 25 56	51	236
...		...		...		10 29+57	50	11 08+57	50	235
...		...		...		10 13+56	49	10 52 57	49	234
...		...		...		...		10 36 57	48	233
...		...		...		...		10 20 57	47	232
...		...		...		...		10 05+57	46	231
...		...		...		...		...		230

For argument H.A. on the left, True Azimuth = $360^\circ - \text{Tabulated Azimuth}$. } See
 For argument H.A. on the right, True Azimuth = Tabulated Azimuth. } p. 90.

24°

24°

In South { For argument H.A. on the left, True Azimuth = $180^\circ + \text{Tabulated Azimuth}$. } See
Latitudes { For argument H.A. on the right, True Azimuth = $180^\circ - \text{Tabulated Azimuth}$. } p. 91.

25°

DECLINATION SAME NAME AS LATITUDE

25°

LAT.	65°		66°		67°		68°		69°		LAT.
H.A.	Alt.	Az.	Alt.	Az.	Alt.	Az.	Alt.	Az.	Alt.	Az.	H.A.
0	50 01+60	180	49 01+60	180	48 01+60	180	47 01+60	180	46 01+60	180	360
1	50 00 60	179	49 00 60	179	48 00 60	179	47 00 60	179	46 01 60	179	359
2	49 59 60	177	49 00 59	177	48 00 60	177	47 00 60	177	46 00 60	177	358
3	49 58 60	176	48 58 60	176	47 58 60	176	46 58 60	176	45 59 60	176	357
4	49 56 60	174	48 56 60	174	47 56 60	175	46 57 60	175	45 57 60	175	356
5	49 53+60	173	48 53+60	173	47 54+60	173	46 54+60	173	45 55+60	173	355
6	49 49 60	172	48 50 60	172	47 51 60	172	46 51 60	172	45 52 60	172	354
7	49 45 60	170	48 46 60	170	47 47 60	171	46 48 60	171	45 49 60	171	353
8	49 41 60	169	48 42 60	169	47 43 60	169	46 44 60	169	45 45 60	170	352
9	49 36 59	167	48 37 60	168	47 38 60	168	46 40 60	168	45 41 60	168	351
10	49 30+59	166	48 32+59	166	47 33+60	167	46 35+60	167	45 36+60	167	350
11	49 23 60	165	48 25 60	165	47 27 60	165	46 29 60	165	45 31 60	166	349
12	49 16 60	163	48 19 59	164	47 21 60	164	46 24 59	164	45 26 59	164	348
13	49 09 59	162	48 12 59	162	47 14 60	163	46 17 60	163	45 20 59	163	347
14	49 00 60	160	48 04 59	161	47 07 60	161	46 10 60	162	45 13 60	162	346
15	48 52+59	159	47 56+59	160	46 59+60	160	46 03+59	160	45 06+60	161	345
16	48 42 59	158	47 47 59	158	46 51 59	159	45 55 59	159	44 59 59	159	344
17	48 33 58	156	47 37 60	157	46 42 59	157	45 47 59	158	44 51 60	158	343
18	48 22 59	155	47 28 59	156	46 33 59	156	45 38 59	156	44 43 59	157	342
19	48 11 59	154	47 17 59	154	46 23 59	155	45 29 59	155	44 34 60	156	341
20	48 00+58	152	47 06+59	153	46 13+59	153	45 19+59	154	44 25+59	154	340
21	47 48 58	151	46 55 59	152	46 02 59	152	45 09 59	153	44 16 59	153	339
22	47 35 58	150	46 43 59	150	45 51 59	151	44 59 58	151	44 06 59	152	338
23	47 22 58	148	46 31 58	149	45 39 59	150	44 48 58	150	43 55 59	151	337
24	47 09 58	147	46 18 58	148	45 27 59	148	44 36 59	149	43 45 58	149	336
25	46 55+58	146	46 05+58	146	45 15+58	147	44 24+59	148	43 33+59	148	335
26	46 40 58	145	45 51 58	145	45 02 58	146	44 12 58	146	43 22 58	147	334
27	46 25 58	143	45 37 58	144	44 48 58	145	43 59 59	145	43 10 58	146	333
28	46 10 57	142	45 23 57	143	44 35 58	143	43 46 58	144	42 58 58	144	332
29	45 54 58	141	45 08 57	141	44 20 58	142	43 33 58	143	42 45 58	143	331
30	45 38+57	140	44 52+58	140	44 06+58	141	43 19+58	141	42 32+58	142	330
31	45 21 57	138	44 36 58	139	43 51 57	140	43 05 58	140	42 19 58	141	329
32	45 04 57	137	44 20 57	138	43 36 57	138	42 50 58	139	42 05 58	140	328
33	44 47 57	136	44 04 57	137	43 20 57	137	42 36 57	138	41 51 58	139	327
34	44 29 57	135	43 47 57	135	43 04 57	136	42 20 58	137	41 36 58	137	326
35	44 11+56	134	43 29+57	134	42 47+57	135	42 05+57	136	41 22+57	136	325
36	43 52 57	132	43 12 56	133	42 31 56	134	41 49 57	134	41 07 57	135	324
37	43 34 56	131	42 54 56	132	42 13 57	133	41 33 57	133	40 51 58	134	323
38	43 14 56	130	42 35 57	131	41 56 57	131	41 16 57	132	40 36 57	133	322
39	42 55 56	129	42 17 56	130	41 38 57	130	40 59 57	131	40 20 57	132	321
40	42 35+55	128	41 58+56	128	41 20+57	129	40 42+57	130	40 04+57	130	320
41	42 15 55	127	41 39 56	127	41 02 56	128	40 25 56	129	39 47 57	129	319
42	41 54 56	125	41 19 56	126	40 43 57	127	40 07 57	128	39 30 57	128	318
43	41 33 56	124	40 59 56	125	40 24 57	126	39 49 57	126	39 13 57	127	317
44	41 12 55	123	40 39 56	124	40 05 56	125	39 31 56	125	38 56 57	126	316
45	40 51+55	122	40 19+55	123	39 46+56	124	39 12+57	124	38 38+57	125	315

In North { For argument H.A. on the left, True Azimuth = $360^\circ - \text{Tabulated Azimuth}$. } See
 Latitudes { For argument H.A. on the right, True Azimuth = Tabulated Azimuth. } p. 90.

25°

DECLINATION SAME NAME AS LATITUDE

25°

LAT.	65°		66°		67°		68°		69°		LAT.
H.A.	Alt.	Az.	Alt.	Az.	Alt.	Az.	Alt.	Az.	Alt.	Az.	H.A.
45	40 51+55	122	40 19+55	123	39 46+56	124	39 12+57	124	38 38+57	125	315
46	40 29 55	121	39 58 55	122	39 26 56	122	38 54 56	123	38 21 56	124	314
47	40 08 54	120	39 37 56	121	39 06 56	121	38 35 56	122	38 03 56	123	313
48	39 45 55	119	39 16 55	120	38 46 56	120	38 16 56	121	37 45 56	122	312
49	39 23 55	118	38 55 55	118	38 26 55	119	37 56 56	120	37 26 56	121	311
50	39 01+54	117	38 33+55	117	38 05+56	118	37 37+56	119	37 08+56	119	310
51	38 38 54	116	38 12 54	116	37 45 55	117	37 17 56	118	36 49 56	118	309
52	38 15 54	115	37 50 54	115	37 24 55	116	36 57 56	117	36 30 56	117	308
53	37 52 54	114	37 27 55	114	37 02 56	115	36 37 55	116	36 11 56	116	307
54	37 28 54	113	37 05 55	113	36 41 55	114	36 17 55	115	35 51 56	115	306
55	37 05+54	112	36 43+54	112	36 20+55	113	35 56+55	114	35 32+56	114	305
56	36 41 54	110	36 20 54	111	35 58 55	112	35 35 56	113	35 12 56	113	304
57	36 17 54	109	35 57 54	110	35 36 55	111	35 15 55	112	34 52 56	112	303
58	35 54 53	108	35 34 54	109	35 14 55	110	34 54 55	110	34 32 56	111	302
59	35 29 54	107	35 11 54	108	34 52 55	109	34 32 56	109	34 12 56	110	301
60	35 05+54	106	34 48+54	107	34 30+54	108	34 11+55	108	33 52+55	109	300
61	34 41 53	105	34 24 55	106	34 07 55	107	33 50 55	107	33 32 55	108	299
62	34 16 54	104	34 01 54	105	33 45 54	106	33 28 55	106	33 11 56	107	298
63	33 52 53	104	33 37 54	104	33 22 55	105	33 07 55	105	32 50 56	106	297
64	33 27 53	103	33 14 54	103	33 00 54	104	32 45 55	104	32 30 55	105	296
65	33 02+54	102	32 50+54	102	32 37+54	103	32 23+55	103	32 09+55	104	295
66	32 37 54	101	32 26 54	101	32 14 54	102	32 01 55	102	31 48 55	103	294
67	32 12 54	100	32 02 54	100	31 51 54	101	31 39 55	102	31 27 55	102	293
68	31 47 54	99	31 38 54	99	31 28 54	100	31 17 55	101	31 06 55	101	292
69	31 22 54	98	31 14 54	98	31 05 54	99	30 55 55	100	30 45 55	100	291
70	30 57+53	97	30 50+53	97	30 42+54	98	30 33+55	99	30 24+55	99	290
71	30 32 53	96	30 26 53	96	30 19 54	97	30 11 54	98	30 03 55	98	289
72	30 07 53	95	30 01 54	96	29 55 54	96	29 49 54	97	29 41 55	97	288
73	29 42 53	94	29 37 54	95	29 32 54	95	29 26 55	96	29 20 55	96	287
74	29 16 53	93	29 13 53	94	29 09 54	94	29 04 54	95	28 59 55	95	286
75	28 51+53	92	28 48+54	93	28 45+54	93	28 41+55	94	28 37+55	94	285
76	28 26 53	91	28 24 54	92	28 22 54	92	28 19 55	93	28 16 55	93	284
77	28 00 53	90	28 00 53	91	27 58 54	91	27 57 54	92	27 54 55	93	283
78	27 35 53	89	27 35 54	90	27 35 54	91	27 34 55	91	27 33 55	92	282
79	27 10 53	89	27 11 53	89	27 12 54	90	27 12 54	90	27 11 55	91	281
80	26 44+53	88	26 47+53	88	26 48+54	89	26 49+55	89	26 50+55	90	280
81	26 19 53	87	26 22 54	87	26 25 54	88	26 27 54	88	26 28 55	89	279
82	25 54 53	86	25 58 53	86	26 01 54	87	26 04 55	87	26 07 55	88	278
83	25 29 53	85	25 34 53	85	25 38 54	86	25 42 55	86	25 45 56	87	277
84	25 03 53	84	25 09 54	85	25 15 54	85	25 20 54	86	25 24 55	86	276
85	24 38+53	83	24 45+54	84	24 51+54	84	24 57+55	85	25 03+55	85	275
86	24 13 53	82	24 21 53	83	24 28 54	83	24 35 55	84	24 41 55	84	274
87	23 48 53	81	23 57 53	82	24 05 54	82	24 13 54	83	24 20 55	83	273
88	23 23 53	81	23 33 53	81	23 42 54	81	23 50 55	82	23 59 55	82	272
89	22 58 53	80	23 09 53	80	23 19 54	81	23 28 55	81	23 37 55	81	271
90	22 33+53	79	22 45+53	79	22 56+54	80	23 06+55	80	23 16+55	81	270

In South { For argument H.A. on the left, True Azimuth = $180^\circ + \text{Tabulated Azimuth}$. } See
 Latitudes { For argument H.A. on the right, True Azimuth = $180^\circ - \text{Tabulated Azimuth}$. } p. 91.

25°

DECLINATION **SAME** NAME AS LATITUDE

25°

LAT.	65°		66°		67°		68°		69°		LAT.
H.A.	Alt.	Az.	Alt.	Az.	Alt.	Az.	Alt.	Az.	Alt.	Az.	H.A.
°	°	d	°	d	°	d	°	d	°	d	°
90	22 33+53	79	22 45+53	79	22 56+54	80	23 06+55	80	23 16+55	81	270
91	22 08 54	78	22 21 53	78	22 33 54	79	22 44 55	79	22 55 55	80	269
92	21 44 53	77	21 57 54	78	22 10 54	78	22 22 55	78	22 34 55	79	268
93	21 19 53	76	21 33 54	77	21 47 54	77	22 00 55	77	22 13 55	78	267
94	20 55 53	75	21 09 54	76	21 24 54	76	21 38 55	77	21 52 55	77	266
95	20 30+54	75	20 46+54	75	21 01+55	75	21 16+55	76	21 31+55	76	265
96	20 06 53	74	20 22 54	74	20 39 54	74	20 55 55	75	21 10 56	75	264
97	19 42 53	73	19 59 54	73	20 16 55	73	20 33 55	74	20 50 55	74	263
98	19 17 54	72	19 36 54	72	19 54 54	73	20 12 55	73	20 29 55	73	262
99	18 53 54	71	19 13 54	71	19 32 54	72	19 50 55	72	20 09 55	72	261
100	18 30+53	70	18 50+54	71	19 09+55	71	19 29+55	71	19 48+56	72	260
101	18 06 54	69	18 27 54	70	18 47 55	70	19 08 55	70	19 28 55	71	259
102	17 42 54	68	18 04 54	69	18 26 54	69	18 47 55	69	19 08 55	70	258
103	17 19 54	68	17 41 55	68	18 04 55	68	18 26 55	69	18 48 55	69	257
104	16 55 54	67	17 19 54	67	17 42 55	67	18 05 55	68	18 28 55	68	256
105	16 32+54	66	16 57+54	66	17 21+55	66	17 44+56	67	18 08+56	67	255
106	16 09 54	65	16 34 55	65	16 59 55	66	17 24 55	66	17 48 56	66	254
107	15 46 55	64	16 12 55	64	16 38 55	65	17 03 56	65	17 29 55	65	253
108	15 24 54	63	15 50 55	64	16 17 55	64	16 43 56	64	17 09 56	64	252
109	15 01 55	62	15 29 55	63	15 56 55	63	16 23 56	63	16 50 56	64	251
110	14 39+54	62	15 07+55	62	15 35+56	62	16 03+56	62	16 31+56	63	250
111	14 17 54	61	14 46 55	61	15 15 55	61	15 43 56	61	16 12 56	62	249
112	13 55 55	60	14 25 55	60	14 54 56	60	15 24 56	61	15 53 56	61	248
113	13 33 55	59	14 04 55	59	14 34 56	60	15 04 56	60	15 34 57	60	247
114	13 12 54	58	13 43 55	58	14 14 56	59	14 45 56	59	15 16 56	59	246
115	12 50+55	57	13 22+56	58	13 54+56	58	14 26+56	58	14 58+56	58	245
116	12 29 55	57	13 02 55	57	13 35 55	57	14 07 56	57	14 39 57	57	244
117	12 08 55	56	12 42 55	56	13 15 56	56	13 48 57	56	14 22 56	56	243
118	11 47 56	55	12 22 55	55	12 56 56	55	13 30 56	55	14 04 56	56	242
119	11 27 55	54	12 02 55	54	12 37 56	54	13 12 56	54	13 46 57	55	241
120	11 07+55	53	11 42+56	53	12 18+56	53	12 53+57	54	13 29+56	54	240
121	10 47 55	52	11 23 56	52	11 59 56	53	12 36 56	53	13 12 56	53	239
122	10 27 55	51	11 04 56	52	11 41 56	52	12 18 56	52	12 55 56	52	238
123	10 07+56	51	10 45 56	51	11 23 56	51	12 00 57	51	12 38 57	51	237
124	...		10 26 56	50	11 05 56	50	11 43 57	50	12 21 57	50	236
125	...		10 08+56	49	10 47+56	49	11 26+57	49	12 05+57	49	235
126	...		...		10 30 56	48	11 09 57	48	11 49 57	48	234
127	...		...		10 12+57	47	10 53 57	47	11 33 57	48	233
128	...		...		...		10 36 57	47	11 17 57	47	232
129	...		...		...		10 20 57	46	11 02 57	46	231
130	...		...		...		10 04+57	45	10 47+57	45	230
131	...		...		...		...		10 32 57	44	229
132	...		...		...		...		10 17 57	43	228
133	...		...		...		...		10 02+58	42	227
134	...		...		...		...		...		226
135	...		...		...		...		...		225

In North { For argument H.A. on the left, True Azimuth = 360° - Tabulated Azimuth. } See
 Latitudes { For argument H.A. on the right, True Azimuth = Tabulated Azimuth. } p. 90.

25°

25°

In South { For argument H.A. on the left, True Azimuth = $180^\circ + \text{Tabulated Azimuth}$. } See
Latitudes { For argument H.A. on the right, True Azimuth = $180^\circ - \text{Tabulated Azimuth}$. } p. 91.

LAT.	65°		66°		67°		68°		69°		LAT.
H.A.	Alt.	Az.	Alt.	Az.	Alt.	Az.	Alt.	Az.	Alt.	Az.	H.A.
0	51 01+60	180	50 01+60	180	49 01+60	180	48 01+60	180	47 01+60	180	360
1	51 00 60	179	50 00 60	179	49 00 60	179	48 00 60	179	47 01 59	179	359
2	50 59 60	177	49 59 60	177	49 00 60	177	48 00 60	177	47 00 60	177	358
3	50 58 60	176	49 58 60	176	48 58 60	176	47 58 60	176	46 59 59	176	357
4	50 56 60	174	49 56 60	174	48 56 60	175	47 57 59	175	46 57 60	175	356
5	50 53+60	173	49 53+60	173	48 54+60	173	47 54+60	173	46 55+59	173	355
6	50 49 60	171	49 50 60	172	48 51 60	172	47 51 60	172	46 52 60	172	354
7	50 45 60	170	49 46 60	170	48 47 60	170	47 48 60	171	46 49 60	171	353
8	50 41 59	169	49 42 59	169	48 43 60	169	47 44 60	169	46 45 60	169	352
9	50 35 60	167	49 37 59	167	48 38 60	168	47 40 59	168	46 41 60	168	351
10	50 29+60	166	49 31+60	166	48 33+60	166	47 35+59	167	46 36+60	167	350
11	50 23 59	164	49 25 60	165	48 27 60	165	47 29 60	165	46 31 60	166	349
12	50 18 59	163	49 18 60	163	48 21 59	164	47 23 60	164	46 25 60	164	348
13	50 08 59	162	49 11 59	162	48 14 59	162	47 17 59	163	46 19 60	163	347
14	50 00 59	160	49 03 59	161	48 07 59	161	47 10 59	161	46 13 59	162	346
15	49 51+59	159	48 55+59	159	47 59+59	160	47 02+60	160	46 06+59	160	345
16	49 41 59	157	48 46 59	158	47 50 59	158	46 54 60	159	45 58 60	159	344
17	49 31 59	156	48 37 58	157	47 41 59	157	46 46 59	157	45 51 59	158	343
18	49 21 59	155	48 27 58	155	47 32 59	156	46 37 59	156	45 42 59	157	342
19	49 10 58	153	48 16 59	154	47 22 59	154	46 28 59	155	45 34 59	155	341
20	48 58+59	152	48 05+59	153	47 12+59	153	46 18+59	154	45 24+59	154	340
21	48 46 58	151	47 54 58	151	47 01 59	152	46 08 59	152	45 15 59	153	339
22	48 33 59	149	47 42 58	150	46 50 58	151	45 57 59	151	45 05 59	152	338
23	48 20 58	148	47 29 59	149	46 38 58	149	45 46 59	150	44 54 59	150	337
24	48 07 58	147	47 16 58	147	46 26 58	148	45 35 58	149	44 43 59	149	336
25	47 53+57	146	47 03+58	146	46 13+58	147	45 23+58	147	44 32+59	148	335
26	47 38 58	144	46 49 58	145	46 00 58	145	45 10 59	146	44 20 59	147	334
27	47 23 57	143	46 35 58	144	45 46 58	144	44 58 58	145	44 08 59	145	333
28	47 07 58	142	46 20 58	142	45 33 57	143	44 44 59	144	43 56 58	144	332
29	46 52 57	140	46 05 58	141	45 18 58	142	44 31 58	142	43 43 58	143	331
30	46 35+57	139	45 50+57	140	45 04+57	140	44 17+58	141	43 30+58	142	330
31	46 18 57	138	45 34 57	139	44 48 58	139	44 03 57	140	43 17 58	141	329
32	46 01 57	137	45 17 57	137	44 33 57	138	43 48 58	139	43 03 58	139	328
33	45 44 56	135	45 01 57	136	44 17 57	137	43 33 58	138	42 49 57	138	327
34	45 26 56	134	44 44 56	135	44 01 57	136	43 18 57	136	42 34 58	137	326
35	45 07+57	133	44 26+57	134	43 44+57	134	43 02+57	135	42 19+58	136	325
36	44 49 56	132	44 08 57	133	43 27 57	133	42 46 57	134	42 04 58	135	324
37	44 30 56	131	43 50 57	131	43 10 57	132	42 30 57	133	41 49 57	133	323
38	44 10 56	130	43 32 56	130	42 53 56	131	42 13 57	132	41 33 57	132	322
39	43 51 55	128	43 13 56	129	42 35 56	130	41 56 57	131	41 17 57	131	321
40	43 30+56	127	42 54+56	128	42 17+56	129	41 39+57	129	41 01+57	130	320
41	43 10 56	126	42 35 55	127	41 58 57	128	41 21 57	128	40 44 57	129	319
42	42 50 55	125	42 15 56	126	41 40 56	126	41 04 56	127	40 27 57	128	318
43	42 29 55	124	41 55 55	125	41 21 56	125	40 46 56	126	40 10 57	127	317
44	42 07 55	123	41 35 55	123	41 01 56	124	40 27 57	125	39 53 56	126	316
45	41 46+55	122	41 14+56	122	40 42+56	123	40 09+56	124	39 35+57	124	315

In North { For argument H.A. on the left, True Azimuth = $360^\circ - \text{Tabulated Azimuth}$. } See
 Latitudes { For argument H.A. on the right, True Azimuth = Tabulated Azimuth. } p. 90.

26°

DECLINATION SAME NAME AS LATITUDE

26°

LAT.	65°		66°		67°		68°		69°		LAT.
H.A.	Alt.	Az.	Alt.	Az.	Alt.	Az.	Alt.	Az.	Alt.	Az.	H.A.
45	41 46+55	122	41 14+56	122	40 42+56	123	40 09+56	124	39 35+57	124	315
46	41 24 55	120	40 53 56	121	40 22 56	122	39 50 56	123	39 17 57	123	314
47	41 02 55	119	40 33 55	120	40 02 56	121	39 31 56	122	38 59 57	122	313
48	40 40 55	118	40 11 55	119	39 42 55	120	39 12 56	120	38 41 56	121	312
49	40 18 54	117	39 50 55	118	39 21 56	119	38 52 56	119	38 22 57	120	311
50	39 55+54	116	39 28+55	117	39 01+55	118	38 33+55	118	38 04+56	119	310
51	39 32 54	115	39 06 55	116	38 40 55	117	38 13 55	117	37 45 56	118	309
52	39 09 54	114	38 44 55	115	38 19 55	116	37 53 55	116	37 26 56	117	308
53	38 46 54	113	38 22 55	114	37 58 55	114	37 32 56	115	37 07 56	116	307
54	38 22 54	112	38 00 54	113	37 36 55	113	37 12 55	114	36 47 56	115	306
55	37 59+54	111	37 37+54	112	37 15+54	112	36 51+56	113	36 28+55	114	305
56	37 35 54	110	37 14 55	111	36 53 55	111	36 31 55	112	36 08 56	113	304
57	37 11 54	109	36 51 55	110	36 31 55	110	36 10 55	111	35 48 56	112	303
58	36 47 54	108	36 28 55	109	36 09 55	109	35 49 55	110	35 28 56	111	302
59	36 23 54	107	36 05 54	108	35 47 54	108	35 28 55	109	35 08 55	110	301
60	35 59+53	106	35 42+54	107	35 24+55	107	35 06+55	108	34 47+56	109	300
61	35 34 54	105	35 19 53	106	35 02 54	106	34 45 55	107	34 27 55	108	299
62	35 10 53	104	34 55 54	105	34 39 55	105	34 23 55	106	34 07 55	107	298
63	34 45 53	103	34 31 54	104	34 17 54	104	34 02 54	105	33 46 55	106	297
64	34 20 54	102	34 08 53	103	33 54 54	103	33 40 55	104	33 25 55	105	296
65	33 56+53	101	33 44+53	102	33 31+54	102	33 18+55	103	33 04+56	104	295
66	33 31 53	100	33 20 53	101	33 08 54	101	32 56 55	102	32 43 56	103	294
67	33 06 53	99	32 56 53	100	32 45 54	100	32 34 55	101	32 22 56	102	293
68	32 41 53	98	32 32 53	99	32 22 54	99	32 12 55	100	32 01 55	101	292
69	32 16 52	97	32 08 53	98	31 59 54	98	31 50 55	99	31 40 55	100	291
70	31 50+53	96	31 43+54	97	31 36+54	98	31 28+54	98	31 19+55	99	290
71	31 25 53	95	31 19 54	96	31 13 54	97	31 05 55	97	30 58 55	98	289
72	31 00 53	94	30 55 53	95	30 49 54	96	30 43 55	96	30 36 55	97	288
73	30 35 53	94	30 31 53	94	30 26 54	95	30 21 54	95	30 15 55	96	287
74	30 09 53	93	30 06 54	93	30 03 54	94	29 58 55	94	29 54 55	95	286
75	29 44+53	92	29 42+53	92	29 39+54	93	29 36+55	93	29 32+55	94	285
76	29 19 53	91	29 18 53	91	29 16 54	92	29 14 54	92	29 11 55	93	284
77	28 53 53	90	28 53 54	90	28 52 54	91	28 51 55	92	28 49 55	92	283
78	28 28 53	89	28 29 53	90	28 29 54	90	28 29 54	91	28 28 55	91	282
79	28 03 53	88	28 04 54	89	28 06 54	89	28 06 55	90	28 06 55	90	281
80	27 37+53	87	27 40+54	88	27 42+54	88	27 44+54	89	27 45+55	89	280
81	27 12 53	86	27 16 53	87	27 19 54	87	27 21 55	88	27 23 55	88	279
82	26 47 53	85	26 51 54	86	26 55 54	86	26 59 54	87	27 02 55	87	278
83	26 22 53	84	26 27 54	85	26 32 54	85	26 37 54	86	26 41 54	86	277
84	25 56 53	84	26 03 53	84	26 09 54	85	26 14 55	85	26 19 55	86	276
85	25 31+53	83	25 39+53	83	25 45+54	84	25 52+54	84	25 58+55	85	275
86	25 06 53	82	25 14 54	82	25 22 54	83	25 30 54	83	25 36 55	84	274
87	24 41 53	81	24 50 54	81	24 59 54	82	25 07 55	82	25 15 55	83	273
88	24 16 53	80	24 26 54	81	24 36 54	81	24 45 55	81	24 54 55	82	272
89	23 51 53	79	24 02 54	80	24 13 54	80	24 23 54	81	24 32 56	81	271
90	23 26+54	78	23 38+54	79	23 50+54	79	24 01+54	80	24 11+55	80	270

In South { For argument H.A. on the left, True Azimuth = $180^\circ + \text{Tabulated Azimuth}$. } See
 Latitudes { For argument H.A. on the right, True Azimuth = $180^\circ - \text{Tabulated Azimuth}$. } p. 91.

LAT.	65°		66°		67°		68°		69°		LAT.
H.A.	Alt.	Az.	Alt.	Az.	Alt.	Az.	Alt.	Az.	Alt.	Az.	H.A.
90	23 26+54	78	23 38+54	79	23 50+54	79	24 01+54	80	24 11+55	80	270
91	23 02 53	77	23 14 54	78	23 27 54	78	23 39 54	79	23 50 55	79	269
92	22 37 53	77	22 51 53	77	23 04 54	77	23 17 54	78	23 29 55	78	268
93	22 12 54	76	22 27 54	76	22 41 54	77	22 55 55	77	23 08 55	77	267
94	21 48 53	75	22 03 54	75	22 18 55	76	22 33 55	76	22 47 55	76	266
95	21 24+53	74	21 40+54	74	21 56+54	75	22 11+55	75	22 26+56	76	265
96	20 59 54	73	21 16 54	74	21 33 55	74	21 50 54	74	22 06 55	75	264
97	20 35 54	72	20 53 54	73	21 11 54	73	21 28 55	73	21 45 55	74	263
98	20 11 54	71	20 30 54	72	20 48 55	72	21 07 55	73	21 24 56	73	262
99	19 47 54	71	20 07 54	71	20 26 55	71	20 45 55	72	21 04 55	72	261
100	19 23+54	70	19 44+54	70	20 04+55	70	20 24+55	71	20 44+55	71	260
101	19 00 53	69	19 21 54	69	19 42 55	70	20 03 55	70	20 23 56	70	259
102	18 36 54	68	18 58 55	68	19 20 55	69	19 42 55	69	20 03 56	69	258
103	18 13 54	67	18 36 54	67	18 59 54	68	19 21 55	68	19 43 56	68	257
104	17 49 54	66	18 13 55	67	18 37 55	67	19 00 56	67	19 23 56	68	256
105	17 26+54	65	17 51+55	66	18 16+54	66	18 40+55	66	19 04+55	67	255
106	17 03 55	65	17 29 55	65	17 54 55	65	18 19 56	65	18 44 56	66	254
107	16 41 54	64	17 07 55	64	17 33 55	64	17 59 55	65	18 24 56	65	253
108	16 18 54	63	16 45 55	63	17 12 55	63	17 39 55	64	18 05 56	64	252
109	15 56 54	62	16 24 54	62	16 51 55	63	17 19 55	63	17 46 56	63	251
110	15 33+55	61	16 02+55	61	16 31+55	62	16 59+55	62	17 27+56	62	250
111	15 11 55	60	15 41 55	61	16 10 55	61	16 39 56	61	17 08 56	61	249
112	14 50 54	60	15 20 55	60	15 50 55	60	16 20 55	60	16 49 56	60	248
113	14 28 55	59	14 59 55	59	15 30 55	59	16 00 56	59	16 31 56	60	247
114	14 06 55	58	14 38 55	58	15 10 55	58	15 41 56	58	16 12 56	59	246
115	13 45+55	57	14 18+55	57	14 50+55	57	15 22+56	58	15 54+56	58	245
116	13 24 55	56	13 57 56	56	14 30 56	57	15 03 56	57	15 36 56	57	244
117	13 03 55	55	13 37 56	55	14 11 56	56	14 45 56	56	15 18 56	56	243
118	12 43 55	54	13 17 56	55	13 52 56	55	14 26 56	55	15 00 57	55	242
119	12 22 55	54	12 57 56	54	13 33 56	54	14 08 56	54	14 43 56	54	241
120	12 02+55	53	12 38+56	53	13 14+56	53	13 50+56	53	14 25+57	53	240
121	11 42 55	52	12 19 56	52	12 55 57	52	13 32 56	52	14 08 57	53	239
122	11 22 56	51	12 00 56	51	12 37 56	51	13 14 57	52	13 51 57	52	238
123	11 03 55	50	11 41 56	50	12 19 56	50	12 57 56	51	13 35 57	51	237
124	10 44 55	49	11 22 56	49	12 01 56	50	12 40 56	50	13 18 57	50	236
125	10 25+55	48	11 04+56	49	11 43+57	49	12 23+56	49	13 02+57	49	235
126	10 06+56	48	10 46 56	48	11 26 57	48	12 06 57	48	12 46 57	48	234
127	...	...	10 28 56	47	11 09 56	47	11 50 56	47	12 30 57	47	233
128	...	...	10 11+56	46	10 52 57	46	11 33 57	46	12 14 58	46	232
129	...	...	...	...	10 35 57	45	11 17 57	45	11 59 57	46	231
130	...	...	...	...	10 19+57	44	11 01+57	45	11 44+57	45	230
131	...	...	...	...	10 03+57	44	10 46 57	44	11 29 57	44	229
132	...	...	...	...	...	...	10 31 57	43	11 14 58	43	228
133	...	...	...	...	...	...	10 16 57	42	11 00 57	42	227
134	...	...	...	...	...	...	10 01+57	41	10 46 57	41	226
135	...	...	...	...	...	...	...	...	10 32+57	40	225

In North { For argument H.A. on the left, True Azimuth = 360° - Tabulated Azimuth. } See
 Latitudes { For argument H.A. on the right, True Azimuth = Tabulated Azimuth. } p. 90.

26°

DECLINATION **SAME** NAME AS LATITUDE

26°

LAT.	65°	66°	67°	68°	69°		LAT.
H.A.					Alt.	Az.	H.A.
					° ' "	° ' "	°
135	...	...	...	...	10 32+57	40	225
136	...	...	...	...	10 18 58	39	224
137	...	...	...	...	10 05+57	38	223
138	...	...	...	...	...	...	222
139	...	...	...	...	...	...	221
140	...	...	...	...	...	...	220

In South { For argument H.A. on the left, True Azimuth = 180° + Tabulated Azimuth. } See
 Latitudes { For argument H.A. on the right, True Azimuth = 180° - Tabulated Azimuth. } p. 91.

LAT.	65°		66°		67°		68°		69°		LAT.
H.A.	Alt.	Az.	Alt.	Az.	Alt.	Az.	Alt.	Az.	Alt.	Az.	H.A.
0	52 01+60	180	51 01+60	180	50 01+60	180	49 01+60	180	48 01+60	180	360
1	52 00 60	179	51 00 60	179	50 00 60	179	49 00 60	179	48 00 60	179	359
2	51 59 60	177	50 59 60	177	50 00 60	177	49 00 60	177	48 00 60	177	358
3	51 58 60	176	50 58 60	176	49 58 60	176	48 58 60	176	47 58 60	176	357
4	51 56 59	174	50 56 60	174	49 56 60	174	48 56 60	175	47 57 60	175	356
5	51 53+60	173	50 53+60	173	49 54+59	173	48 54+60	173	47 54+60	173	355
6	51 49 60	171	50 50 60	172	49 51 59	172	48 51 60	172	47 52 60	172	354
7	51 45 60	170	50 46 60	170	49 47 60	170	48 48 60	171	47 49 59	171	353
8	51 40 60	168	50 41 60	169	49 43 59	169	48 44 60	169	47 45 60	169	352
9	51 35 60	167	50 36 60	167	49 38 60	168	48 39 60	168	47 41 59	168	351
10	51 29+59	166	50 31+59	166	49 33+59	166	48 34+60	166	47 36+60	167	350
11	51 22 60	164	50 25 59	165	49 27 59	165	48 29 59	165	47 31 59	165	349
12	51 15 59	163	50 18 59	163	49 20 60	163	48 23 59	164	47 25 60	164	348
13	51 07 60	161	50 10 60	162	49 13 60	162	48 16 60	162	47 19 60	163	347
14	50 59 59	160	50 02 60	160	49 06 59	161	48 09 60	161	47 12 60	162	346
15	50 50+59	159	49 54+59	159	48 58+59	159	48 02+59	160	47 05+60	160	345
16	50 40 59	157	49 45 59	158	48 49 60	158	47 54 59	159	46 58 59	159	344
17	50 30 59	156	49 35 59	156	48 40 60	157	47 45 59	157	46 50 59	158	343
18	50 20 58	154	49 25 59	155	48 31 59	155	47 36 59	156	46 41 60	156	342
19	50 08 59	153	49 15 59	154	48 21 59	154	47 27 59	155	46 33 59	155	341
20	49 57+58	152	49 04+58	152	48 11+58	153	47 17+59	153	46 23+59	154	340
21	49 44 59	150	48 52 59	151	48 00 58	152	47 07 59	152	46 14 59	153	339
22	49 32 58	149	48 40 58	150	47 48 59	150	46 56 59	151	46 04 58	151	338
23	49 18 58	148	48 28 58	148	47 36 59	149	46 45 58	149	45 53 59	150	337
24	49 05 57	146	48 14 59	147	47 24 58	148	46 33 59	148	45 42 59	149	336
25	48 50+58	145	48 01+58	146	47 11+58	146	46 21+58	147	45 31+58	148	335
26	48 36 57	144	47 47 58	144	46 58 58	145	46 09 58	146	45 19 58	146	334
27	48 20 58	143	47 33 57	143	46 44 58	144	45 56 58	144	45 07 58	145	333
28	48 05 57	141	47 18 57	142	46 30 58	143	45 43 58	143	44 54 59	144	332
29	47 49 57	140	47 03 57	141	46 16 58	141	45 29 58	142	44 41 59	143	331
30	47 32+57	139	46 47+57	139	46 01+58	140	45 15+58	141	44 28+58	141	330
31	47 15 57	137	46 31 57	138	45 46 57	139	45 00 58	140	44 15 58	140	329
32	46 58 57	136	46 14 57	137	45 30 58	138	44 46 57	138	44 01 57	139	328
33	46 40 57	135	45 58 56	136	45 14 57	136	44 31 57	137	43 46 58	138	327
34	46 22 56	134	45 40 57	135	44 58 57	135	44 15 57	136	43 32 57	137	326
35	46 04+56	133	45 23+56	133	44 41+57	134	43 59+58	135	43 17+57	135	325
36	45 45 56	131	45 05 56	132	44 24 57	133	43 43 57	134	43 02 57	134	324
37	45 26 55	130	44 47 56	131	44 07 57	132	43 27 57	132	42 46 57	133	323
38	45 06 56	129	44 28 56	130	43 49 57	131	43 10 57	131	42 30 57	132	322
39	44 46 56	128	44 09 56	129	43 31 57	129	42 53 57	130	42 14 57	131	321
40	44 26+55	127	43 50+56	127	43 13+56	128	42 36+56	129	41 58+57	130	320
41	44 06 55	126	43 30 56	126	42 55 56	127	42 18 57	128	41 41 57	128	319
42	43 45 55	124	43 11 55	125	42 36 56	126	42 00 57	127	41 24 57	127	318
43	43 24 55	123	42 50 56	124	42 17 55	125	41 42 56	126	41 07 57	126	317
44	43 02 55	122	42 30 55	123	41 57 56	124	41 24 56	124	40 49 57	125	316
45	42 41+55	121	42 10+55	122	41 38+55	123	41 05+56	123	40 32+56	124	315

In North { For argument H.A. on the left, True Azimuth = $360^\circ - \text{Tabulated Azimuth}$. } See
 Latitudes { For argument H.A. on the right, True Azimuth = Tabulated Azimuth. } p. 90.

LAT.	65°		66°		67°		68°		69°		LAT.
H.A.	Alt.	Az.	Alt.	Az.	Alt.	Az.	Alt.	Az.	Alt.	Az.	H.A.
45	42 41+55	121	42 10+55	122	41 38+55	123	41 05+56	123	40 32+56	124	315
46	42 19 55	120	41 49 55	121	41 18 55	121	40 46 56	122	40 14 56	123	314
47	41 57 54	119	41 28 55	120	40 58 55	120	40 27 56	121	39 56 56	122	313
48	41 35 54	118	41 06 55	119	40 37 56	119	40 08 55	120	39 37 57	121	312
49	41 12 54	117	40 45 55	117	40 17 55	118	39 48 56	119	39 19 56	120	311
50	40 49+54	116	40 23+55	116	39 56+55	117	39 28+56	118	39 00+56	119	310
51	40 26 54	115	40 01 55	115	39 35 55	116	39 08 56	117	38 41 56	118	309
52	40 03 54	114	39 39 54	114	39 14 55	115	38 48 56	116	38 22 56	116	308
53	39 40 54	112	39 17 54	113	38 53 54	114	38 28 55	115	38 03 55	115	307
54	39 16 54	111	38 54 54	112	38 31 55	113	38 07 56	114	37 43 56	114	306
55	38 53+53	110	38 31+55	111	38 09+55	112	37 47+55	113	37 23+56	113	305
56	38 29 53	109	38 09 54	110	37 48 54	111	37 26 55	112	37 04 55	112	304
57	38 05 53	108	37 46 54	109	37 26 54	110	37 05 55	111	36 44 55	111	303
58	37 41 53	107	37 23 53	108	37 04 54	109	36 44 55	110	36 24 55	110	302
59	37 17 53	106	36 59 54	107	36 41 55	108	36 23 55	108	36 03 56	109	301
60	36 52+53	105	36 36+54	106	36 19+54	107	36 01+55	107	35 43+55	108	300
61	36 28 53	104	36 12 54	105	35 56 55	106	35 40 55	106	35 22 56	107	299
62	36 03 53	103	35 49 53	104	35 34 54	105	35 18 55	105	35 02 55	106	298
63	35 38 53	102	35 25 54	103	35 11 54	104	34 56 55	104	34 41 55	105	297
64	35 14 53	101	35 01 54	102	34 48 54	103	34 35 54	103	34 20 56	104	296
65	34 49+53	100	34 37+54	101	34 25+55	102	34 13+54	102	34 00+55	103	295
66	34 24 53	100	34 13 54	100	34 02 55	101	33 51 54	102	33 39 55	102	294
67	33 59 53	99	33 49 54	99	33 39 54	100	33 29 54	101	33 18 55	101	293
68	33 34 52	98	33 25 54	98	33 16 54	99	33 07 54	100	32 56 55	100	292
69	33 08 53	97	33 01 54	97	32 53 54	98	32 45 54	99	32 35 55	99	291
70	32 43+53	96	32 37+53	96	32 30+54	97	32 22+55	98	32 14+55	98	290
71	32 18 53	95	32 13 53	95	32 07 54	96	32 00 54	97	31 53 55	97	289
72	31 53 53	94	31 48 54	95	31 43 54	95	31 38 54	96	31 31 55	96	288
73	31 28 52	93	31 24 53	94	31 20 54	94	31 15 55	95	31 10 55	95	287
74	31 02 53	92	31 00 53	93	30 57 53	93	30 53 54	94	30 49 54	94	286
75	30 37+53	91	30 35+54	92	30 33+54	92	30 31+54	93	30 27+55	94	285
76	30 12 52	90	30 11 53	91	30 10 54	91	30 08 54	92	30 06 55	93	284
77	29 46 53	89	29 47 53	90	29 46 54	90	29 46 54	91	29 44 55	92	283
78	29 21 53	88	29 22 54	89	29 23 54	90	29 23 55	90	29 23 55	91	282
79	28 56 52	88	28 58 53	88	29 00 53	89	29 01 54	89	29 01 55	90	281
80	28 30+53	87	28 34+53	87	28 36+54	88	28 38+55	88	28 40+55	89	280
81	28 05 53	86	28 09 53	86	28 13 54	87	28 16 54	87	28 18 55	88	279
82	27 40 53	85	27 45 53	85	27 49 54	86	27 53 55	86	27 57 55	87	278
83	27 15 52	84	27 21 53	84	27 26 54	85	27 31 54	86	27 35 55	86	277
84	26 49 53	83	26 56 54	84	27 03 54	84	27 09 54	85	27 14 55	85	276
85	26 24+53	82	26 32+54	83	26 39+54	83	26 46+55	84	26 53+55	84	275
86	25 59 53	81	26 08 53	82	26 16 54	82	26 24 54	83	26 31 55	83	274
87	25 34 53	80	25 44 53	81	25 53 54	81	26 02 54	82	26 10 55	82	273
88	25 09 53	80	25 20 53	80	25 30 54	81	25 40 54	81	25 49 55	81	272
89	24 44 53	79	24 56 53	79	25 07 54	80	25 17 55	80	25 28 54	81	271
90	24 20+53	78	24 32+54	78	24 44+54	79	24 55+55	79	25 06+55	80	270

In South { For argument H.A. on the left, True Azimuth = $180^\circ +$ Tabulated Azimuth. } See
 Latitudes { For argument H.A. on the right, True Azimuth = $180^\circ -$ Tabulated Azimuth. } p. 91.

LAT.	65°		66°		67°		68°		69°		LAT.
H.A.	Alt.	Az.	Alt.	Az.	Alt.	Az.	Alt.	Az.	Alt.	Az.	H.A.
90	24 20+53	78	24 32+54	78	24 44+54	79	24 55+55	79	25 06+55	80	270
91	23 55 53	77	24 08 54	77	24 21 54	78	24 33 55	78	24 45 55	79	269
92	23 30 53	76	23 44 54	77	23 58 54	77	24 11 55	77	24 24 55	78	268
93	23 06 53	75	23 21 53	76	23 35 55	76	23 50 54	77	24 03 55	77	267
94	22 41 54	74	22 57 54	75	23 13 54	75	23 28 54	76	23 42 56	76	266
95	22 17+53	74	22 34+54	74	22 50+54	74	23 06+55	75	23 22+55	75	265
96	21 53 53	73	22 10 54	73	22 28 54	73	22 44 55	74	23 01 55	74	264
97	21 29 53	72	21 47 54	72	22 05 55	73	22 23 55	73	22 40 56	73	263
98	21 05 53	71	21 24 54	71	21 43 54	72	22 02 54	72	22 20 55	72	262
99	20 41 53	70	21 01 54	70	21 21 54	71	21 40 55	71	21 59 56	72	261
100	20 17+54	69	20 38+54	70	20 59+54	70	21 19+55	70	21 39+55	71	260
101	19 53 54	68	20 15 54	69	20 37 54	69	20 58 55	69	21 19 55	70	259
102	19 30 54	68	19 53 54	68	20 15 55	68	20 37 55	69	20 59 55	69	258
103	19 07 53	67	19 30 54	67	19 53 55	67	20 16 55	68	20 39 55	68	257
104	18 43 54	66	19 08 54	66	19 32 55	66	19 56 55	67	20 19 56	67	256
105	18 20+54	65	18 46+54	65	19 10+55	66	19 35+55	66	19 59+56	66	255
106	17 58 54	64	18 24 54	64	18 49 55	65	19 15 55	65	19 40 55	65	254
107	17 35 54	63	18 02 54	64	18 28 55	64	18 54 56	64	19 20 56	65	253
108	17 12 55	62	17 40 55	63	18 07 55	63	18 34 56	63	19 01 56	64	252
109	16 50 54	62	17 18 55	62	17 46 56	62	18 14 56	62	18 42 56	63	251
110	16 28+54	61	16 57+55	61	17 26+55	61	17 54+56	62	18 23+56	62	250
111	16 06 54	60	16 36 55	60	17 05 56	60	17 35 55	61	18 04 56	61	249
112	15 44 55	59	16 15 55	59	16 45 56	60	17 15 56	60	17 45 56	60	248
113	15 23 54	58	15 54 55	58	16 25 56	59	16 56 56	59	17 27 56	59	247
114	15 01 55	57	15 33 55	58	16 05 56	58	16 37 56	58	17 08 57	58	246
115	14 40+55	57	15 13+55	57	15 45+56	57	16 18+56	57	16 50+56	58	245
116	14 19 55	56	14 53 55	56	15 26 56	56	15 59 56	56	16 32 57	57	244
117	13 58 55	55	14 33 55	55	15 07 55	55	15 41 56	56	16 14 57	56	243
118	13 38 55	54	14 13 55	54	14 48 55	54	15 22 56	55	15 57 56	55	242
119	13 17 56	53	13 53 56	53	14 29 56	54	15 04 56	54	15 39 57	54	241
120	12 57+56	52	13 34+55	53	14 10+56	53	14 46+56	53	15 22+57	53	240
121	12 37 56	51	13 15 55	52	13 52 56	52	14 28 57	52	15 05 57	52	239
122	12 18 55	51	12 56 55	51	13 33 56	51	14 11 56	51	14 48 57	51	238
123	11 58 56	50	12 37 56	50	13 15 56	50	13 53 57	50	14 32 56	51	237
124	11 39 56	49	12 18 56	49	12 57 57	49	13 36 57	49	14 15 57	50	236
125	11 20+56	48	12 00+56	48	12 40+56	48	13 19+57	49	13 59+57	49	235
126	11 02 56	47	11 42 56	47	12 23 56	48	13 03 57	48	13 43 57	48	234
127	10 43 56	46	11 24 57	47	12 05 57	47	12 46 57	47	13 27 57	47	233
128	10 25 56	46	11 07 56	46	11 49 56	46	12 30 57	46	13 12 57	46	232
129	10 07+57	45	10 50 56	45	11 32 57	45	12 14 57	45	12 56 58	45	231
130	...		10 33+56	44	11 16+56	44	11 58+58	44	12 41+57	44	230
131	...		10 16 57	43	11 00 56	43	11 43 57	43	12 26 58	44	229
132	...		10 00+56	42	10 44 57	42	11 28 57	42	12 12 57	43	228
133	...		...		10 28 57	41	11 13 57	42	11 57 58	42	227
134	...		...		10 13+57	41	10 58 57	41	11 43 58	41	226
135	...		...		...		10 44+57	40	11 29+58	40	225

In North { For argument H.A. on the left, True Azimuth = 360° - Tabulated Azimuth. } See
 Latitudes { For argument H.A. on the right, True Azimuth = Tabulated Azimuth. } p. 90.

27°

DECLINATION **SAME** NAME AS LATITUDE

27°

LAT.	65°	66°	67°	68°	69°	LAT.
H.A.				Alt. Az.	Alt. Az.	H.A.
°				° ° ° °		°
135	...	...	...	10 44+57 40	11 29+58 40	225
136	...	...	...	10 29 58 39	11 16 57 39	224
137	...	...	...	10 16 57 38	11 02 58 38	223
138	...	...	...	10 02+58 37	10 49 58 37	222
139	...	...	...	...	10 36 58 36	221
140	...	...	...	...	10 24+58 36	220
141	...	...	...	...	10 12 58 35	219
142	...	...	...	...	10 00+58 34	218
143	...	...	...	...	...	217
144	...	...	...	...	...	216
145	...	...	...	...	...	215

In South { For argument H.A. on the left, True Azimuth = $180^\circ + \text{Tabulated Azimuth}$. } See
 Latitudes { For argument H.A. on the right, True Azimuth = $180^\circ - \text{Tabulated Azimuth}$. } p. 91.

LAT.	65°			66°			67°			68°			69°			LAT.
H.A.	Alt.	Az.		Alt.	Az.		Alt.	Az.		Alt.	Az.		Alt.	Az.		H.A.
	°	°	d	°	°	d	°	°	d	°	°	d	°	°	d	°
0	53 01	+60	180	52 01	+60	180	51 01	+60	180	50 01	+60	180	49 01	+60	180	360
1	53 00	60	179	52 00	60	179	51 00	60	179	50 00	60	179	49 00	60	179	359
2	52 59	60	177	51 59	60	177	51 00	59	177	50 00	60	177	49 00	60	177	358
3	52 58	60	176	51 58	60	176	50 58	60	176	49 58	60	176	48 58	60	176	357
4	52 55	60	174	51 56	60	174	50 56	60	174	49 56	60	175	48 57	60	175	356
5	52 53	+59	173	51 53	+60	173	50 53	+60	173	49 54	+60	173	48 54	+60	173	355
6	52 49	60	171	51 50	60	171	50 50	60	172	49 51	60	172	48 52	60	172	354
7	52 45	60	170	51 46	60	170	50 47	59	170	49 48	59	170	48 48	60	171	353
8	52 40	60	168	51 41	60	169	50 42	60	169	49 44	59	169	48 45	59	169	352
9	52 35	59	167	51 36	60	167	50 38	59	167	49 39	60	168	48 40	60	168	351
10	52 28	+60	165	51 30	+60	166	50 32	+60	166	49 34	+60	166	48 36	+59	167	350
11	52 22	59	164	51 24	60	164	50 26	60	165	49 28	60	165	48 30	60	165	349
12	52 14	60	163	51 17	60	163	50 20	59	163	49 22	60	164	48 25	59	164	348
13	52 07	59	161	51 10	59	162	50 13	59	162	49 16	59	162	48 19	59	163	347
14	51 58	59	160	51 02	59	160	50 05	60	161	49 09	59	161	48 12	59	161	346
15	51 49	+59	158	50 53	+59	159	49 57	+59	159	49 01	+59	160	48 05	+59	160	345
16	51 39	59	157	50 44	59	157	49 49	59	158	48 53	59	158	47 57	59	159	344
17	51 29	59	156	50 34	59	156	49 40	59	156	48 44	60	157	47 49	59	157	343
18	51 18	59	154	50 24	59	155	49 30	59	155	48 35	59	156	47 41	59	156	342
19	51 07	58	153	50 14	58	153	49 20	59	154	48 26	59	154	47 32	59	155	341
20	50 55	+58	151	50 02	+59	152	49 09	+59	153	48 16	+59	153	47 22	+59	154	340
21	50 43	58	150	49 51	58	151	48 58	59	151	48 06	58	152	47 13	58	152	339
22	50 30	58	149	49 38	59	149	48 47	58	150	47 55	58	150	47 02	59	151	338
23	50 16	58	147	49 26	58	148	48 35	58	149	47 43	59	149	46 52	58	150	337
24	50 02	58	146	49 13	58	147	48 22	58	147	47 32	58	148	46 41	58	148	336
25	49 48	+58	145	48 59	+58	145	48 09	+58	146	47 19	+59	147	46 29	+59	147	335
26	49 33	58	143	48 45	58	144	47 56	58	145	47 07	58	145	46 17	59	146	334
27	49 18	57	142	48 30	58	143	47 42	58	143	46 54	58	144	46 05	58	145	333
28	49 02	57	141	48 15	58	142	47 28	58	142	46 41	57	143	45 53	58	143	332
29	48 46	57	140	48 00	57	140	47 14	57	141	46 27	58	142	45 40	58	142	331
30	48 29	+57	138	47 44	+57	139	46 59	+57	140	46 13	+57	140	45 26	+58	141	330
31	48 12	57	137	47 28	57	138	46 43	58	138	45 58	58	139	45 13	57	140	329
32	47 55	56	136	47 11	57	137	46 28	57	137	45 43	58	138	44 58	58	139	328
33	47 37	56	135	46 54	57	135	46 11	57	136	45 28	57	137	44 44	58	137	327
34	47 18	57	133	46 37	56	134	45 55	57	135	45 12	58	136	44 29	58	136	326
35	47 00	+56	132	46 19	+57	133	45 38	+57	134	44 57	+57	134	44 14	+58	135	325
36	46 41	56	131	46 01	56	132	45 21	57	132	44 40	57	133	43 59	57	134	324
37	46 21	56	130	45 43	56	130	45 04	56	131	44 24	57	132	43 43	58	133	323
38	46 02	55	128	45 24	56	129	44 46	56	130	44 07	57	131	43 27	58	132	322
39	45 42	55	127	45 05	56	128	44 28	56	129	43 50	56	130	43 11	57	130	321
40	45 21	+56	126	44 46	+55	127	44 09	+56	128	43 32	+57	128	42 55	+57	129	320
41	45 01	55	125	44 26	56	126	43 51	56	127	43 15	56	127	42 38	57	128	319
42	44 40	55	124	44 06	56	125	43 32	56	125	42 57	56	126	42 21	57	127	318
43	44 19	55	123	43 46	55	124	43 12	56	124	42 38	57	125	42 04	56	126	317
44	43 57	55	122	43 25	56	122	42 53	56	123	42 20	56	124	41 46	56	125	316
45	43 36	+54	120	43 05	+55	121	42 33	+56	122	42 01	+56	123	41 28	+57	124	315

In North { For argument H.A. on the left, True Azimuth = 360° - Tabulated Azimuth. } See
 Latitudes { For argument H.A. on the right, True Azimuth = Tabulated Azimuth. } p. 90.

28°

DECLINATION **SAME** NAME AS LATITUDE

28°

LAT.	65°		66°		67°		68°		69°		LAT.
H.A.	Alt.	Az.	Alt.	Az.	Alt.	Az.	Alt.	Az.	Alt.	Az.	H.A.
45	43 36+54	120	43 05+55	121	42 33+56	122	42 01+56	123	41 28+57	124	315
46	43 14 54	119	42 44 55	120	42 13 56	121	41 42 56	122	41 10 56	122	314
47	42 51 55	118	42 23 54	119	41 53 55	120	41 23 56	121	40 52 56	121	313
48	42 29 54	117	42 01 55	118	41 33 55	119	41 03 56	120	40 34 56	120	312
49	42 06 54	116	41 40 54	117	41 12 55	118	40 44 55	118	40 15 56	119	311
50	41 43+54	115	41 18+54	116	40 51+55	117	40 24+55	117	39 56+56	118	310
51	41 20 54	114	40 56 54	115	40 30 55	116	40 04 55	116	39 37 56	117	309
52	40 57 54	113	40 33 55	114	40 09 55	114	39 44 55	115	39 18 56	116	308
53	40 34 53	112	40 11 54	113	39 47 55	113	39 23 55	114	38 58 56	115	307
54	40 10 54	111	39 48 54	112	39 26 55	112	39 03 55	113	38 39 55	114	306
55	39 46+54	110	39 26+54	111	39 04+55	111	38 42+55	112	38 19+56	113	305
56	39 22 54	109	39 03 54	110	38 42 55	110	38 21 55	111	37 59 56	112	304
57	38 58 54	108	38 40 54	109	38 20 55	109	38 00 55	110	37 39 56	111	303
58	38 34 53	107	38 16 54	108	37 58 54	108	37 39 55	109	37 19 55	110	302
59	38 10 53	106	37 53 54	107	37 36 54	107	37 18 54	108	36 59 55	109	301
60	37 45+53	105	37 30+53	106	37 13+54	106	36 56+55	107	36 38+56	108	300
61	37 21 53	104	37 06 54	105	36 51 54	105	36 35 54	106	36 18 55	107	299
62	36 56 53	103	36 42 54	104	36 28 54	104	36 13 55	105	35 57 55	106	298
63	36 31 53	102	36 19 53	103	36 05 54	103	35 51 55	104	35 36 55	105	297
64	36 07 52	101	35 55 53	102	35 42 54	102	35 29 55	103	35 16 55	104	296
65	35 42+52	100	35 31+53	101	35 20+53	101	35 07+55	102	34 55+55	103	295
66	35 17 52	99	35 07 53	100	34 57 53	100	34 45 55	101	34 34 55	102	294
67	34 52 52	98	34 43 53	99	34 33 54	99	34 23 55	100	34 13 54	101	293
68	34 26 53	97	34 19 53	98	34 10 54	98	34 01 55	99	33 51 55	100	292
69	34 01 53	96	33 55 53	97	33 47 54	97	33 39 54	98	33 30 55	99	291
70	33 36+53	95	33 30+54	96	33 24+54	96	33 17+54	97	33 09+55	98	290
71	33 11 52	94	33 06 53	95	33 01 53	96	32 54 55	96	32 48 54	97	289
72	32 46 52	93	32 42 53	94	32 37 54	95	32 32 54	95	32 26 55	96	288
73	32 20 53	92	32 17 54	93	32 14 54	94	32 10 54	94	32 05 55	95	287
74	31 55 52	91	31 53 53	92	31 50 54	93	31 47 55	93	31 43 55	94	286
75	31 30+52	91	31 29+53	91	31 27+54	92	31 25+54	92	31 22+55	93	285
76	31 04 53	90	31 04 53	90	31 04 53	91	31 02 55	91	31 01 54	92	284
77	30 39 52	89	30 40 53	89	30 40 54	90	30 40 54	91	30 39 55	91	283
78	30 14 52	88	30 16 53	88	30 17 54	89	30 18 54	90	30 18 54	90	282
79	29 48 53	87	29 51 53	88	29 53 54	88	29 55 54	89	29 56 55	89	281
80	29 23+53	86	29 27+53	87	29 30+54	87	29 33+54	88	29 35+54	88	280
81	28 58 52	85	29 02 54	86	29 07 53	86	29 10 54	87	29 13 55	87	279
82	28 33 52	84	28 38 53	85	28 43 54	85	28 48 54	86	28 52 54	86	278
83	28 07 53	83	28 14 53	84	28 20 54	84	28 25 55	85	28 30 55	86	277
84	27 42 53	83	27 50 53	83	27 57 53	84	28 03 54	84	28 09 55	85	276
85	27 17+53	82	27 26+53	82	27 33+54	83	27 41+54	83	27 48+54	84	275
86	26 52 53	81	27 01 54	81	27 10 54	82	27 18 55	82	27 26 55	83	274
87	26 27 53	80	26 37 54	80	26 47 54	81	26 56 55	81	27 05 55	82	273
88	26 02 53	79	26 13 54	80	26 24 54	80	26 34 54	81	26 44 55	81	272
89	25 37 53	78	25 49 54	79	26 01 54	79	26 12 54	80	26 22 55	80	271
90	25 13+53	77	25 26+53	78	25 38+54	78	25 50+54	79	26 01+55	79	270

In South { For argument H.A. on the left, True Azimuth = $180^\circ + \text{Tabulated Azimuth.}$ } See
 Latitudes { For argument H.A. on the right, True Azimuth = $180^\circ - \text{Tabulated Azimuth.}$ } p. 91.

28°

DECLINATION **SAME** NAME AS LATITUDE

28°

LAT.	65°		66°		67°		68°		69°		LAT.
H.A.	Alt.	Az.	Alt.	Az.	Alt.	Az.	Alt.	Az.	Alt.	Az.	H.A.
90	25 13+53	77	25 26+53	78	25 38+54	78	25 50+54	79	26 01+55	79	270
91	24 48 53	76	25 02 53	77	25 15 54	77	25 28 54	78	25 40 55	78	269
92	24 23 53	76	24 38 54	76	24 52 54	76	25 06 55	77	25 19 55	77	268
93	23 59 53	75	24 14 54	75	24 30 54	76	24 44 55	76	24 58 55	77	267
94	23 35 53	74	23 51 54	74	24 07 54	75	24 22 55	75	24 38 55	76	266
95	23 10+53	73	23 28+53	73	23 44+55	74	24 01+54	74	24 17+55	75	265
96	22 46 53	72	23 04 54	73	23 22 54	73	23 39 55	73	23 56 55	74	264
97	22 22 53	71	22 41 54	72	23 00 54	72	23 18 55	73	23 36 55	73	263
98	21 58 54	70	22 18 54	71	22 37 55	71	22 56 55	72	23 15 55	72	262
99	21 34 54	70	21 55 54	70	22 15 55	70	22 35 55	71	22 55 55	71	261
100	21 11+53	69	21 32+54	69	21 53+55	70	22 14+55	70	22 34+56	70	260
101	20 47 54	68	21 09 55	68	21 31 55	69	21 53 55	69	22 14 56	69	259
102	20 24 53	67	20 47 54	67	21 10 54	68	21 32 55	68	21 54 56	69	258
103	20 00 54	66	20 24 55	67	20 48 55	67	21 11 55	67	21 34 56	68	257
104	19 37 54	65	20 02 54	66	20 27 54	66	20 51 55	66	21 15 55	67	256
105	19 14+54	65	19 40+54	65	20 05+55	65	20 30+55	66	20 55+55	66	255
106	18 52 54	64	19 18 55	64	19 44 55	64	20 10 55	65	20 35 56	65	254
107	18 29 54	63	18 56 55	63	19 23 55	63	19 50 55	64	20 16 56	64	253
108	18 07 54	62	18 35 54	62	19 02 55	63	19 30 55	63	19 57 56	63	252
109	17 44 55	61	18 13 55	61	18 42 55	62	19 10 55	62	19 38 55	62	251
110	17 22+55	60	17 52+55	61	18 21+55	61	18 50+56	61	19 19+56	62	250
111	17 00 55	60	17 31 55	60	18 01 55	60	18 30 56	60	19 00 56	61	249
112	16 39 54	59	17 10 55	59	17 41 55	59	18 11 56	59	18 41 56	60	248
113	16 17 55	58	16 49 55	58	17 21 55	58	17 52 56	59	18 23 56	59	247
114	15 56 55	57	16 28 56	57	17 01 55	57	17 33 56	58	18 05 56	58	246
115	15 35+55	56	16 08+55	56	16 41+56	57	17 14+56	57	17 46+57	57	245
116	15 14 55	55	15 48 55	56	16 22 55	56	16 55 56	56	17 29 56	56	244
117	14 53 55	54	15 28 55	55	16 02 56	55	16 37 56	55	17 11 56	55	243
118	14 33 55	54	15 08 56	54	15 43 56	54	16 18 57	54	16 53 57	55	242
119	14 13 55	53	14 49 55	53	15 25 56	53	16 00 57	53	16 36 56	54	241
120	13 53+55	52	14 29+56	52	15 06+56	52	15 42+57	53	16 19+56	53	240
121	13 33 55	51	14 10 56	51	14 48 56	52	15 25 56	52	16 02 56	52	239
122	13 13 56	50	13 51 56	50	14 29 57	51	15 07 57	51	15 45 57	51	238
123	12 54 56	49	13 33 56	50	14 11 57	50	14 50 57	50	15 28 57	50	237
124	12 35 56	49	13 14 56	49	13 54 56	49	14 33 57	49	15 12 57	49	236
125	12 16+56	48	12 56+56	48	13 36+57	48	14 16+57	48	14 56+57	48	235
126	11 58 56	47	12 38 57	47	13 19 57	47	14 00 56	47	14 40 57	48	234
127	11 39 56	46	12 21 56	46	13 02 57	46	13 43 57	47	14 24 57	47	233
128	11 21 56	45	12 03 57	45	12 45 57	46	13 27 57	46	14 09 57	46	232
129	11 04 56	44	11 46 57	44	12 29 56	45	13 11 57	45	13 54 57	45	231
130	10 46+56	44	11 29+57	44	12 12+57	44	12 56+57	44	13 38+58	44	230
131	10 29 56	43	11 13 56	43	11 56 57	43	12 40 57	43	13 24 57	43	229
132	10 12+56	42	10 56 57	42	11 41 57	42	12 25 57	42	13 09 58	42	228
133	...		10 40 57	41	11 25 57	41	12 10 57	41	12 55 57	41	227
134	...		10 25 56	40	11 10 57	40	11 55 58	40	12 41 57	41	226
135	...		10 09+57	39	10 55+57	39	11 41+58	40	12 27+58	40	225

In North { For argument H.A. on the left, True Azimuth = 360° - Tabulated Azimuth. } See
 Latitudes { For argument H.A. on the right, True Azimuth = Tabulated Azimuth. } p. 90.

28°

DECLINATION SAME NAME AS LATITUDE

28°

LAT.	65°	66°	67°	68°	69°	LAT.
H.A.		Alt. Az.	Alt. Az.	Alt. Az.	Alt. Az.	H.A.
135	...	10 09+57 39	10 55+57 39	11 41+58 40	12 27+58 40	225
136	...	...	10 40 58 39	11 27 57 39	12 13 58 39	224
137	...	...	10 26 57 38	11 13 58 38	12 00 58 38	223
138	...	...	10 12+57 37	11 00 57 37	11 47 58 37	222
139	...	...	...	10 46 58 36	11 34 58 36	221
140	...	...	...	10 33+58 35	11 22+58 35	220
141	...	...	...	10 20 58 34	11 10 58 34	219
142	...	...	...	10 08+58 34	10 58 58 34	218
143	...	...	...	...	10 46 58 33	217
144	...	...	...	...	10 35 58 32	216
145	...	...	...	...	10 23+59 31	215
146	...	...	...	...	10 13 58 30	214
147	...	...	...	...	10 02+58 29	213
148	...	...	...	...	...	212
149	...	...	...	...	...	211
150	...	...	...	...	...	210

In South { For argument H.A. on the left, True Azimuth = $180^\circ + \text{Tabulated Azimuth}$. } See
 Latitudes { For argument H.A. on the right, True Azimuth = $180^\circ - \text{Tabulated Azimuth}$. } p. 91.

EXPLANATION

By agreement with the Admiralty, the *Astronomical Navigation Tables* are produced by H.M. Nautical Almanac Office to the general requirements of the Air Ministry.

These tables are designed to give, in a simple and direct manner, the solution of the astronomical spherical triangle that occurs in navigational practice. They have been planned for use with the *Air Almanac* (Air Publication 1602) and are consequently designed primarily to meet the requirements of modern air navigation: their use can however be extended to surface navigation, as in the case of the *Air Almanac*, within the limitations of the precision of the tabulated altitude and azimuth.

The general object of the *Astronomical Navigation Tables* is to facilitate the calculation of the Altitude and Azimuth of an observed heavenly body, as seen from some position close to that of the observer. This information, together with the observed altitude, allows to be plotted on the chart a position line upon which the observer must lie; two such position lines serve in general to determine the position of the observer. The tables have been arranged with special relation to the determination of the altitude and azimuth when an assumed position is adopted such that the latitude and hour angle are both integral degrees; interpolation in this case is consequently restricted to interpolation to the declination of the body observed, and provision has been made for this to be done in a simple manner. The precision of the tabulated data is consistent with that adopted for the *Air Almanac*, namely that the altitudes are given to the nearest minute of arc, and so are correct to within 0'.5; this standard of precision is sufficient for all purposes of air navigation and, in fact, is at present (1938) considerably greater than the precision obtainable in an altitude observed with a bubble sextant. Although these tables have been prepared in conjunction with the *Air Almanac*, they are equally applicable for use with any other almanac from which the Greenwich Hour Angle and Declination of the body observed can be found for the time of observation; it is intended, however, that the two publications should provide, in the most convenient form, all the material for a rapid solution of the navigator's problem, for all practical observations.

The *Astronomical Navigation Tables* consist of main tables and auxiliary tables. The main tables give the Tabulated Altitude, to the nearest minute of arc, and the Tabulated Azimuth, to the nearest degree, with the three arguments:—

Latitude —each integral degree from S.69° to N.69°.

Declination—for 22 selected stars for the epoch 1940 and each integral degree from S.28° to N.28°.

Hour Angle—each integral degree for which the altitude is greater than 10°* and less than 80°.

Thus for every combination of an integral degree of latitude, declination and hour angle in the above ranges, the tables give immediately the quantities required.

* The limit is decreased for declinations appropriate to the Sun (0°–23°) in latitudes above 55°, where the Sun may be at low altitudes for long periods of each day, and in latitudes below 30°, where the Sun rises rapidly, and the azimuth at low altitudes is required for checking compasses.

EXPLANATION

In the case of the separate tabulations for the 22 stars, the values of the declinations used in the tables are those of the stars themselves at the middle of 1940; the declinations of the stars change slowly owing to precession and to other causes, but the effect of these changes can be allowed for by means of a simple correcting term, which although smaller, is catered for in a similar way to the interpolation for the declination of other bodies. The stars have been selected for their brightness and their distribution in the sky, and are the same in both name and number as stars Nos. 1-22 in the *Air Almanac*. The tables for integral degrees of declination are applicable to observations of the Sun, Moon and planets, as well as for all stars with declinations between $S.29^{\circ}$ and $N.29^{\circ}$; a list of 13 such stars is given in the *Air Almanac* (Nos. 23-35). It is only for stars outside these limits of declination, in particular stars Nos. 36-50 in the *Air Almanac*, that these tables are not applicable, some other method of obtaining the altitude and azimuth must then be employed. The 22 stars catered for separately may however be regarded as generally sufficient for all practical purposes of air navigation; with the 13 additional stars to be used in exceptional circumstances, reference to other methods should be unnecessary.

The interpolation of tables with three arguments is both laborious and difficult, and should be avoided wherever possible; no provision has therefore been made for interpolation other than for declination, and the navigator should not interpolate for latitude and hour angle, but should use an assumed position so that this may be avoided. The arrangement of the tables, however, allows for interpolation for latitude and hour angle without, in general, the necessity for the comparison of figures on different pages, and the tables may therefore be interpolated for these arguments for the solution of special problems.

The tabulated altitude includes the effect of atmospheric refraction, and is thus directly comparable with the corrected sextant reading; it is in fact the altitude of the body as would be measured by an observer. The refraction included is based on the mean value of the refraction at a height of 5,000 feet in normal conditions, and it is unlikely that at heights in that neighbourhood the refraction will differ by more than 0.5 from that used. Table VI on page 222 gives the adjustment necessary at heights that differ materially from the basic height adopted; the values in this table should only be applied in extreme cases, and where great accuracy is necessary.

The tabulated azimuth is measured from the elevated pole either to the east or to the west. This can be converted to true azimuth, measured always from the north through east, either by the rules given at the foot of each page, or by the use of Table III on pages 90 and 91.

For the greater convenience of the user, the tables are issued in fourteen volumes, each of which caters for a belt of latitude, 5° in width, in both the northern and southern hemispheres. In each volume tabulations are given for five integral degrees of latitude; working from an assumed position, whose latitude is taken to be the nearest integral degree to that of the D.R. (or estimated) position of the observer, each tabular latitude suffices to cover observations from positions within $0^{\circ} 30'$ of the integral degree used. The Explanation and auxiliary tables are reprinted in each volume.

Each volume consists of two main parts, pages 2-89 giving the tabulations for the selected 22 stars and pages 94-209 those for declinations 0° - 28° . Each part is

EXPLANATION

divided into sections of four pages, covering one star or one whole degree of declination; separate indexes on the margin enable immediate reference to be made to the first opening of each section. Throughout, the arrangement of the tabulations in each section is generally the same; the five values of latitude (LAT.) are given across the page and the values of the hour angle (H.A.) down the page. For the stars, the tabulations for NORTH latitudes precede those for SOUTH latitudes, and for the integral degrees of declination, those for the SAME name as the latitude precede those for CONTRARY name. The amount of tabulation varies in each case with different stars and declinations, and in some cases there are no tabulations either in north or in south latitudes, as the star or a body of the given declination does not reach an altitude which makes it suitable for observation in those latitudes; occasionally it has been necessary to continue the tabulation from one page on to the previous page, and for one or two stars, in south latitudes, on to two pages before.

For the stars, each column refers to a given latitude, and contains for all applicable values of the hour angle, the altitude (Alt.), its variation with time (t) and the azimuth (Az.). For the degrees of declination, the variation t is replaced by the difference (d) between the altitude given and that for the following degree. The procedure of entering and interpolating the tables is not appreciably different in the two cases.

An assumed position is taken close to the D.R. position so that the latitude is an integral degree, while the longitude is chosen so that the hour angle, formed by the combination of longitude (*added if east, subtracted if west*) with the G.H.A., taken from the *Air Almanac*, is also an integral degree. The appropriate part (star or degree of declination) is chosen, and the correct section obtained by the marginal index, using the star number, or the integral degree numerically *less* than the declination of the observed body as found from the *Air Almanac*. In this section, the column is chosen corresponding to the assumed latitude, care being taken to select the correct hemisphere. In this column, the values of Alt., t , and Az. can be read off for the stars, corresponding to the particular integral hour angle; for a degree of declination, the values of Alt., d and Az. are similarly found.

The tabulated altitude must now be corrected, in the case of the 22 stars, for the effect of precession, and for other bodies, interpolated to the true declination. Table I on the inside front cover gives the correction to be applied to the altitude of the stars for all years to 2000 for values of t ; this correction must be added or subtracted according to the sign prefixed to t . For each star a limiting year is given before which this correction cannot exceed $1'$, and there is therefore no need to apply it until after that date. Similarly, the inside back cover and its facing page contain Table XV, with arguments d and the minutes of the declination of the body, giving the correction to be applied to the tabulated altitude taken out for an integral degree; this correction is to be applied to the tabulated altitude with the same sign as that of d .

It is unnecessary to correct the tabulated azimuth in any way, but it must of course be converted to true azimuth before being used to plot a position line.

Having thus obtained the corrected tabulated altitude and the true azimuth, the position line is drawn in the usual manner. The intercept is obtained from the difference between the corrected sextant reading and the corrected tabulated altitude, and is set off from the assumed position either *towards* the direction given

EXPLANATION

by the true azimuth or in the opposite direction (*away* from), according to the following rules:

Corr. Tab. Alt. *less* than Corr. Sext. Rdg., intercept *towards*;

Corr. Tab. Alt. *greater* than Corr. Sext. Rdg., intercept *away*.

The position line is then drawn at right angles to the intercept through the point so obtained. The expression corrected sextant reading is used conveniently for the observed altitude to emphasize that this quantity is the altitude as measured by the sextant, corrected only for sextant errors and for dome refraction if applicable. As the atmospheric refraction is catered for in the tabulated altitude, no correction for this should be applied to the sextant reading.

If the assumed position is close to the true position, a slight inaccuracy in plotting the tabulated azimuth is unimportant; when the tabulated azimuth is near 0° or 180° advantage may be taken of this to draw the position line simply as part of a parallel of latitude. A double border rule, given when the azimuth is within a few degrees of the meridian, indicates the portions of the tables where this can be done without great error; the limit of azimuth has been varied slightly in different volumes, according to the latitude, so as to reduce the error due to this simplified procedure. The accuracy of this method depends upon the error in the assumed longitude; for an error of 20 miles in the D.R. longitude, the maximum error introduced into the deduced latitude is about 2 miles, while the remaining error (due to the use of an assumed position) may reach a maximum of 2 miles in the worst case. This method should therefore only be adopted either when errors up to about 4 miles can be tolerated, or when the D.R. longitude is known to be fairly accurate; if the D.R. position is liable to much greater error than 20 miles, this method should not be used. An assumed position is taken and the tables entered in exactly the same way (whether for stars or other bodies) as for an ordinary observation, but there is now no necessity to take out the azimuth or to convert to true azimuth. The tabulated altitude is corrected by Table I or Table XV as necessary, and the intercept formed by the usual rules. The intercept is then set off from the assumed position *towards* or *away* from the direction of the object observed, this direction being taken as true north or true south; the position line is thus drawn in as a parallel of latitude. Although the procedure of entering the tables is exactly the same, this method saves a considerable amount of work in the plotting of the position line.

A list of the auxiliary tables is given in the list of contents; in general the titles of these tables are self-explanatory and their use either self-evident or explained on the page concerned.

Tables VII, VIII, IX, X, XI and XIII are arranged as critical tables, so that the result is obtained immediately without interpolation. The argument is divided into intervals, successive intervals corresponding to successive values of the result; for any values of the argument, inside one of these intervals, the corresponding result is the quantity opposite that interval and has in general a maximum error of less than half a unit in the last figure given; when successive values of the result are not consecutive integers, this error can rise to half the difference between successive values. The tabulated values of the argument correspond to half-way values of the result, and these are always chosen so that when the argument is exactly equal to one of the tabulated values, the nearest value of the result is the one corresponding to the previous interval. Thus the rule to be followed is:

When the argument is an exact tabulated value, the *upper* of the two possible values of the result should be taken.

ILLUSTRATIONS

Example 1.—On 1941 March 31, local date, about two hours after sunset, in dead reckoning position latitude $68^{\circ} 17' N.$, longitude $125^{\circ} 20' W.$, star number 16 (Procyon) was observed to obtain a position line. Corrected sextant reading $24^{\circ} 23'$: G.M.T. of observation $05^h 08^m 14^s$.

From Table IV, page 92:

Long. $120^{\circ} W.$ (approx.)		
Approx.	Hrs.	Date
L.M.T.	2100	Mar. 31
G.M.T.	0500	Apr. 1

From *Air Almanac*, 1941 Apr. 1:

G.H.A. γ ($05^h 00^m$)	. 264	10
Increment ($8^m 14^s$)	. 2	04
S.H.A. (No. 16)	. 245	57
G.H.A. of star	. 512	11
Long. of ass. position	. -125	11
		387 00
		-360

From page 62:

Lat. of ass. position $68^{\circ} NORTH$

Tab. Alt.	. . .	24	49
Correction	. . .		—

Corr. Tab. Alt. . . . 24 49

Corr. Sext. Rdg. . . . 24 23

Intercept 26' away

Star No. 16

H.A. 27°

No correction for
date is necessary
in 1941.

Tab. Az. 150°

Assumed position : From Table III,
Lat. $68^{\circ} N.$ page 90:
Long. $125^{\circ} 11' W.$ True Az. $210^{\circ} T.$

Example 2.—On 1950 August 17, Greenwich date, in dead reckoning position latitude $65^{\circ} 52' S.$, longitude $26^{\circ} 29' E.$, star number 13 (Fomalhaut) was observed to obtain a position line. From the *Almanac* of that date it was found that the G.H.A. of the star corresponding to the G.M.T. of observation was $355^{\circ} 14'$. Corrected sextant reading $51^{\circ} 39'$.

G.H.A. of star	. . .	355	14
Long. of ass. position	. +	26	46
			382 00
			-360

From page 50:

Lat. of ass. position $66^{\circ} SOUTH$

Tab. Alt.	. . .	51	31
Correction (Table I)	. -		3

Corr. Tab. Alt. . . . 51 28

Corr. Sext. Rdg. . . . 51 39

Intercept 11' towards

Star No. 13

H.A. 22°

. . . -19
Year . 1950

Tab. Az. 149°

Assumed position: From Table III,
Lat. $66^{\circ} S.$ page 91:
Long. $26^{\circ} 46' E.$ True Az. $329^{\circ} T.$

ILLUSTRATIONS

Example 3.—On 1941 April 1, local date, at approximate local noon, in dead reckoning position latitude $68^{\circ} 40' N.$, longitude $49^{\circ} 47' W.$, the Sun was observed to obtain a position line. Corrected sextant reading $25^{\circ} 51'$; G.M.T. of observation $15^h 11^m 27^s$.

From Table IV, page 92:

Long. $45^{\circ} W.$ (approx.)		
Approx.	Hrs.	Date
L.M.T.	1200	Apr. 1
G.M.T.	1500	Apr. 1

From *Air Almanac*, 1941 Apr. 1:

G.H.A.	($15^h 10^m$)	.	46	31
Increment	($1^m 27^s$)	.	0	22
G.H.A. of Sun	.	.	46	53
Long. of ass. position	.	-	49	53
			-	3 00
			+360	

From page 110:

Lat. of ass. position	$69^{\circ} N.$	Dec.	$4^{\circ} 33' N.$	SAME name	H.A.	357°
Tab. Alt.	.	.	25 00	d	.	+60
Correction (Table XV)	+		33	Minutes of dec.	33	
Corr. Tab. Alt.	.	.	25 33	Assumed position:	From Table III,	
Corr. Sext. Rdg.	.	.	25 51	Lat.	$69^{\circ} N.$	page 90:
Intercept	.	.	18' towards	Long.	$49^{\circ} 53' W.$	True Az. $177^{\circ} T.$

Since there is a double border rule opposite the entry on page 110, this observation may be reduced by the method described on page 213. In this case the intercept is set off from the assumed position *towards* the Sun (i.e. southwards), and the position line drawn as a parallel of latitude. There is then no necessity to take out the tabulated azimuth.

Example 4.—On 1941 April 2, local date, shortly before sunrise, in dead reckoning position latitude $64^{\circ} 38' S.$, longitude $147^{\circ} 58' E.$, Mars was observed to obtain a position line. Corrected sextant reading $44^{\circ} 31'$; G.M.T. of observation $20^h 28^m 17^s$.

From Table IV, page 93:

Long. $150^{\circ} E.$ (approx.)		
Approx.	Hrs.	Date
L.M.T.	0600	Apr. 2
G.M.T.	2000	Apr. 1

From *Air Almanac*, 1941 Apr. 1:

G.H.A.	(20^h)	.	187	51
Increment	($28^m 17^s$)	.	7	05
G.H.A. of Mars	.	.	194	56
Long. of ass. position	.	+	148	04

From page 178:

Lat. of ass. position	$65^{\circ} S.$	Dec.	$21^{\circ} 11' S.$	SAME name	H.A.	343°
Tab. Alt.	.	.	44 37	d	.	+59
Correction (Table XV)	+		11	Minutes of dec.	11	
Corr. Tab. Alt.	.	.	44 48	Assumed position:	From Table III,	
Corr. Sext. Rdg.	.	.	44 31	Lat.	$65^{\circ} S.$	page 91:
Intercept	.	.	17' away	Long.	$148^{\circ} 04' E.$	True Az. $023^{\circ} T.$

IVa.—CHANGE OF SEXTANT READING WITH TIME

Due to motion of
body observed

Due to motion of observer

True Azi- muth of body	Latitude			True Azi- muth of body	Difference between True Az. of body and Track	Ground speed in m.p.h.									Difference between True Az. of body and Track
	65°	67°	69°			100	130	160	190	220	250	280	310	340	
090	+19	+18	+16	090	000	+4	+6	+7	+8	+10	+11	+12	+13	+15	360
095	19	18	16	085	005	4	6	7	8	10	11	12	13	15	355
100	19	17	16	080	010	4	6	7	8	9	11	12	13	15	350
105	18	17	16	075	015	4	5	7	8	9	10	12	13	14	345
110	18	17	15	070	020	4	5	7	8	9	10	11	13	14	340
115	17	16	15	065	025	4	5	6	7	9	10	11	12	13	335
120	+16	+15	+14	060	030	+4	+5	+6	+7	+8	+9	+11	+12	+13	330
125	16	14	13	055	035	4	5	6	7	8	9	10	11	12	325
130	15	13	12	050	040	3	4	5	6	7	8	9	10	11	320
135	13	12	11	045	045	3	4	5	6	7	8	9	10	10	315
140	12	11	10	040	050	3	4	4	5	6	7	8	9	9	310
145	11	10	9	035	055	2	3	4	5	5	6	7	8	8	305
150	+10	+9	+8	030	060	+2	+3	+3	+4	+5	+5	+6	+7	+7	300
155	8	7	7	025	065	2	2	3	3	4	5	5	6	6	295
160	7	6	6	020	070	1	2	2	3	3	4	4	5	5	290
165	5	5	4	015	075	1	1	2	2	2	3	3	3	4	285
170	3	3	3	010	080	+1	+1	1	1	2	2	2	2	3	280
175	+2	+2	+1	005	085	0	0	+1	+1	+1	+1	+1	+1	+1	275
180	0	0	0	000	090	0	0	0	0	0	0	0	0	0	270
185	-2	-2	-1	355	095	0	0	-1	-1	-1	-1	-1	-1	-1	265
190	3	3	3	350	100	-1	-1	1	1	2	2	2	2	3	260
195	5	5	4	345	105	1	1	2	2	2	3	3	3	4	255
200	7	6	6	340	110	1	2	2	3	3	4	4	5	5	250
205	8	7	7	335	115	2	2	3	3	4	5	5	6	6	245
210	-10	-9	-8	330	120	-2	-3	-3	-4	-5	-5	-6	-7	-7	240
215	11	10	9	325	125	2	3	4	5	5	6	7	8	8	235
220	12	11	10	320	130	3	4	4	5	6	7	8	9	9	230
225	13	12	11	315	135	3	4	5	6	7	8	9	10	10	225
230	15	13	12	310	140	3	4	5	6	7	8	9	10	11	220
235	16	14	13	305	145	4	5	6	7	8	9	10	11	12	215
240	-16	-15	-14	300	150	-4	-5	-6	-7	-8	-9	-11	-12	-13	210
245	17	16	15	295	155	4	5	6	7	9	10	11	12	13	205
250	18	17	15	290	160	4	5	7	8	9	10	11	13	14	200
255	18	17	16	285	165	4	5	7	8	9	10	12	13	14	195
260	19	17	16	280	170	4	6	7	8	9	11	12	13	15	190
265	19	18	16	275	175	4	6	7	8	10	11	12	13	15	185
270	-19	-18	-16	270	180	-4	-6	-7	-8	-10	-11	-12	-13	-15	180

The theoretical change of sextant reading in any interval of time depends partly on the motion of the body observed across the sky and partly on the motion of the observer over the Earth's surface.

The two tables above give this change, in an interval of three minutes of time, due to each of these causes; a + sign denotes that the sextant reading is increasing, and a - sign that it is decreasing. The theoretical change of sextant reading in three minutes of time is obtained by combining the appropriate entries from each table.

IVb.—CHANGE OF SEXTANT READING WITH TIME

Interval of time	Change in 3 ^m (from Table IVa)								Interval of time
	0' 3' 6'	9' 12' 15'	18' 21' 24'	27' 30' 33'	36' 39' 42'	45' 48' 51'	54' 57' 60'		
0 00	0 0 0	0 0 0	0 0 0	0 0 0	0 0 0	0 0 0	0 0 0	0 00	
05	0 0 0	0 0 0	0 1 1	1 1 1	1 1 1	1 1 1	2 2 2	05	
10	0 0 0	0 1 1	1 1 1	2 2 2	2 2 2	2 3 3	3 3 3	10	
15	0 0 0	1 1 1	2 2 2	2 2 3	3 3 4	4 4 4	4 5 5	15	
20	0 0 1	1 1 2	2 2 3	3 3 4	4 4 5	5 5 6	6 6 7	20	
25	0 0 1	1 2 2	2 3 3	4 4 5	5 5 6	6 7 7	8 8 8	25	
0 30	0 0 1	2 2 2	3 4 4	4 5 6	6 6 7	8 8 8	9 10 10	0 30	
35	0 1 1	2 2 3	4 4 5	5 6 6	7 8 8	9 9 10	10 11 12	35	
40	0 1 1	2 3 3	4 5 5	6 7 7	8 9 9	10 11 11	12 13 13	40	
45	0 1 2	2 3 4	4 5 6	7 8 8	9 10 10	11 12 13	14 14 15	45	
50	0 1 2	2 3 4	5 6 7	8 8 9	10 11 12	12 13 14	15 16 17	50	
0 55	0 1 2	3 4 5	6 6 7	8 9 10	11 12 13	14 15 16	16 17 18	0 55	
1 00	0 1 2	3 4 5	6 7 8	9 10 11	12 13 14	15 16 17	18 19 20	1 00	
05	0 1 2	3 4 5	6 8 9	10 11 12	13 14 15	16 17 18	20 21 22	05	
10	0 1 2	4 5 6	7 8 9	10 12 13	14 15 16	18 19 20	21 22 23	10	
15	0 1 2	4 5 6	8 9 10	11 12 14	15 16 18	19 20 21	22 24 25	15	
20	0 1 3	4 5 7	8 9 11	12 13 15	16 17 19	20 21 23	24 25 27	20	
25	0 1 3	4 6 7	8 10 11	13 14 16	17 18 20	21 23 24	26 27 28	25	
1 30	0 2 3	4 6 8	9 10 12	14 15 16	18 20 21	22 24 26	27 28 30	1 30	
35	0 2 3	5 6 8	10 11 13	14 16 17	19 21 22	24 25 27	28 30 32	35	
40	0 2 3	5 7 8	10 12 13	15 17 18	20 22 23	25 27 28	30 32 33	40	
45	0 2 4	5 7 9	10 12 14	16 18 19	21 23 24	26 28 30	32 33 35	45	
50	0 2 4	6 7 9	11 13 15	16 18 20	22 24 26	28 29 31	33 35 37	50	
1 55	0 2 4	6 8 10	12 13 15	17 19 21	23 25 27	29 31 33	34 36 38	1 55	
2 00	0 2 4	6 8 10	12 14 16	18 20 22	24 26 28	30 32 34	36 38 40	2 00	
05	0 2 4	6 8 10	12 15 17	19 21 23	25 27 29	31 33 35	38 40 42	05	
10	0 2 4	6 9 11	13 15 17	20 22 24	26 28 30	32 35 37	39 41 43	10	
15	0 2 4	7 9 11	14 16 18	20 22 25	27 29 32	34 36 38	40 43 45	15	
20	0 2 5	7 9 12	14 16 19	21 23 26	28 30 33	35 37 40	42 44 47	20	
25	0 2 5	7 10 12	14 17 19	22 24 27	29 31 34	36 39 41	44 46 48	25	
2 30	0 2 5	8 10 12	15 18 20	22 25 28	30 32 35	38 40 42	45 48 50	2 30	
35	0 3 5	8 10 13	16 18 21	23 26 28	31 34 36	39 41 44	46 49 52	35	
40	0 3 5	8 11 13	16 19 21	24 27 29	32 35 37	40 43 45	48 51 53	40	
45	0 3 6	8 11 14	16 19 22	25 28 30	33 36 38	41 44 47	50 52 55	45	
50	0 3 6	8 11 14	17 20 23	26 28 31	34 37 40	42 45 48	51 54 57	50	
2 55	0 3 6	9 12 15	18 20 23	26 29 32	35 38 41	44 47 50	52 55 58	2 55	
3 00	0 3 6	9 12 15	18 21 24	27 30 33	36 39 42	45 48 51	54 57 60	3 00	

This table gives the theoretical change of sextant reading in any interval of time up to 3^m, in terms of the change in 3^m obtained from the tables on the opposite page. If the interval is greater than 3^m, it may be split into multiples of 3^m and a residue, and the corresponding entries from the table added together.

A knowledge of this change enables sights on different objects taken at slightly different times to be adjusted to a specified exact time, which may be either the exact time of one of them or a moment when a fix is required for a particular reason.

NOTES

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V.—DIFFERENCE BETWEEN RHUMB LINE AND GREAT CIRCLE DISTANCES

N. 65°-69°

S. 65°-69°

Latitude of Destination	Change of Longitude						Latitude of Destination
	5° 10° 15°	20° 25° 30°	35° 40° 45°	50° 55° 60°	65° 70° 75°	80° 85° 90°	
N. 60°	0 1 1	3 5 8	13 19 26	36 47 61	77 96 118	143 172 204	S. 60°
55	0 1 2	4 6 10	15 21 29	39 51 66	83 103 126	153 183 217	55
50	0 1 2	4 7 11	17 24 32	43 56 71	89 110 134	162 193 228	50
45	0 1 3	5 9 13	19 26 35	47 60 76	94 116 141	169 202 238	45
40	0 1 3	6 10 14	21 28 38	50 64 80	99 121 147	176 209 246	40
N. 35	0 2 4	6 10 16	22 30 40	52 67 84	103 126 152	181 215 253	S. 35
30	0 2 4	7 11 17	24 32 42	55 69 86	106 129 156	185 219 257	30
25	0 2 4	7 12 17	25 33 44	56 71 88	109 132 158	188 222 260	25
20	0 2 4	8 12 18	25 34 45	58 72 90	110 133 159	189 223 261	20
15	0 2 4	8 13 18	26 35 46	58 73 90	110 133 159	189 223 261	15
N. 10	0 2 4	8 13 19	26 35 46	58 73 90	110 132 158	188 221 258	S. 10
N. 5	0 2 4	8 13 19	26 35 45	58 72 89	108 131 156	184 217 253	S. 5
0	0 2 4	8 13 18	26 34 45	57 71 87	106 128 152	180 211 247	0
S. 5	0 2 4	8 12 18	25 34 44	55 69 85	103 124 147	174 204 239	N. 5
10	0 2 4	8 12 18	24 32 42	53 67 82	99 119 141	167 196 229	10
S. 15	0 2 4	7 11 17	23 31 40	51 64 78	94 113 134	159 186 217	N. 15
20	0 2 4	7 11 16	22 29 38	48 60 73	89 107 127	149 175 204	20
25	0 2 4	6 10 15	21 28 36	45 56 69	83 99 118	139 162 189	25
30	0 1 3	6 10 14	19 26 33	42 52 63	76 91 108	127 149 173	30
35	0 1 3	6 9 13	18 23 30	38 47 58	70 83 98	116 135 157	35
S. 40	0 1 3	5 8 12	16 21 27	34 43 52	63 75 88	104 121 140	N. 40
45	0 1 3	5 7 10	14 19 25	31 38 47	56 66 78	92 107 124	45
50	0 1 2	4 7 9	13 17 22	28 34 42	50 59 70	81 94 109	50
55	0 1 2	4 6 9	12 16 20	25 31 38	45 53 62	72 84 96	55
S. 60	0 1 2	4 6 8	11 15 19	24 29 35	42 50 58	67 77 88	N. 60

This table gives the difference, in nautical miles, between the distance from one place to another by the Rhumb Line track and the distance by the Great Circle track. It is based on a *Latitude of Departure* of 67°, but may be used for any place of departure between latitudes 65° and 69°. Of the two argument columns headed *Latitude of Destination*, the one on the left is to be used when the place of departure lies between N. 65° and N. 69°, and the one on the right when the place of departure lies between S. 65° and S. 69°.

The table is intended to give only the approximate difference of distance between the two tracks. For intermediate values of the arguments *Latitude of Destination* and *Change of Longitude*, the figures in the table should be interpolated by inspection. If the *Latitude of Departure* differs by the maximum of 2½ from that on which the table is based, the error in the result will not exceed 6 miles up to a *Change of Longitude* of 50°, but may reach 12 miles for a change of 70°, and 20 miles for a change of 90°.

Example.—Required the difference in distance between the Rhumb Line track and the Great Circle track from Obdorsk (Lat. 66° 30' N., Long. 67° 20' E.) to Lerwick (Lat. 60° 10' N., Long. 1° 10' W.).

Entering the argument column on the left with the *Latitude of Destination* of 60° 10' N., and interpolating by inspection for the *Change of Longitude* of 68° 30', it will be seen that the difference in distance is about 90 nautical miles.

VI.—ADJUSTMENT TO REFRACTION IN SPECIAL CONDITIONS

Height in feet	Observed Altitude									Height in metres
	4°	6°	8°	10°	15°	20°	30°	45°	60°	
0	-2	-1	-1	-1	0	0	0	0	0	0
5000	0	0	0	0	0	0	0	0	0	1500
10000	+1	+1	+1	+1	0	0	0	0	0	3000
15000	2	2	2	1	+1	+1	0	0	0	4600
20000	3	2	2	2	1	1	+1	0	0	6100
25000	4	3	2	2	1	1	1	0	0	7600
30000	4	3	3	3	2	1	1	0	0	9100
35000	5	4	3	3	2	1	1	+1	0	10700
40000	+5	+4	+3	+3	+2	+2	+1	+1	0	12200

This table gives the additional correction for refraction to be applied to the *observed* altitude beyond that already included in the altitude tabulated in the main tables. It is only intended for use by an observer at great heights, and when special accuracy is required.

VII.—TRUE AZIMUTH OF THE POLE STAR

1940-1960		1960-1980		1980-2000	
L.H.A. °	True Azi- muth	L.H.A. °	True Azi- muth	L.H.A. °	True Azi- muth
0	0	0	0	0	0
15	001	17	001	20	001
38	000	43	000	49	000
64	359	72	359	83	359
170	358	168	358	166	358
195	359	197	359	200	359
218	000	223	000	229	000
244	001	252	001	263	001
350	002	348	002	346	002
360	001	360	001	360	001

These tables give the True Azimuth of the Pole Star, over various periods of time, for an observer between latitudes N. 65° and N. 69°. The argument L.H.A.° is obtained from G.H.A.° by *subtracting west* longitude or *adding east* longitude.

VIII.—DIP OF THE SEA HORIZON

Height in feet	Height in metres	Height in feet	Height in metres	Height in feet	Height in metres	Height in feet	Height in metres	Height in feet	Height in metres	Height in feet	Height in metres
0	0	437	133	1700	520	3810	1160	6740	2050		
2	1	481	146	1790	546	3930	1200	6910	2100		
6	1	527	160	1880	573	4060	1230	7080	2160		
12	3	575	175	1970	600	4190	1270	7250	2210		
21	4	625	190	2060	628	4330	1320	7430	2260		
31	5	677	206	2150	657	4460	1360	7610	2320		
43	6	731	222	2250	686	4600	1400	7790	2370		
58	7	787	240	2340	716	4740	1440	7970	2420		
75	8	845	257	2440	746	4880	1480	8150	2480		
93	9	906	276	2550	777	5020	1530	8340	2540		
114	10	968	295	2650	809	5170	1570	8520	2590		
137	11	1030	314	2760	841	5320	1620	8710	2650		
162	12	1090	335	2860	874	5470	1660	8900	2710		
189	13	1160	356	2980	908	5620	1710	9100	2770		
218	14	1230	377	3090	942	5770	1760	9290	2830		
250	15	1310	399	3200	977	5930	1800	9490	2890		
283	16	1380	422	3320	1010	6090	1850	9690	2950		
318	17	1460	446	3440	1040	6250	1900	9890	3010		
356	18	1540	470	3560	1080	6410	1950	10100	3070		
395	19	1620	495	3680	1120	6580	2000	10300	3140		
437	20	1700	520	3810	1160	6740	2050	10500	3200		

This table gives the dip of the sea horizon, in minutes of arc, with argument height of eye of the observer in feet or in metres. It is only required when the altitude is measured from the sea horizon. The dip is to be *subtracted* from the observed altitude.

IX.—DISTANCE TO THE SEA HORIZON IN NAUTICAL MILES

Height in feet	Dist.	Height in metres	Height in feet	Dist.	Height in metres	Height in feet	Dist.	Height in metres	Height in feet	Dist.	Height in metres	Height in feet	Dist.	Height in metres	Height in feet	Dist.	Height in metres
0		0	287	20	87	1120	39	341	2500	58	762	4420	77	1340	6890	96	2100
1	1		317	21	96	1170	39	359	2580	59	788	4540	78	1380	7040	97	2140
4	2	1	349	22	106	1240	40	378	2670	60	815	4650	79	1420	7180	97	2190
9	3	2	382	22	116	1300	41	396	2760	61	843	4770	80	1450	7330	98	2230
15	4	4	417	24	127	1360	42	416	2850	62	871	4900	81	1490	7480	99	2280
22	5	6	453	25	138	1430	43	436	2950	63	900	5020	82	1530	7630	100	2320
31	6	9	491	26	149	1490	44	456	3040	64	929	5140	83	1560	7780	101	2370
42	7	12	531	27	161	1560	45	477	3140	65	958	5270	84	1600	7940	102	2420
54	8	16	571	28	174	1630	46	498	3240	66	988	5390	85	1640	8100	103	2460
68	9	20	614	28	187	1700	47	520	3340	66	1010	5520	86	1680	8250	104	2510
83	10	25	658	29	200	1770	48	542	3440	67	1050	5650	87	1720	8410	105	2560
100	11	30	703	30	214	1850	49	564	3540	68	1080	5780	88	1760	8570	106	2610
118	12	36	750	31	228	1920	50	587	3650	69	1110	5920	88	1800	8730	107	2660
137	13	42	798	32	243	2000	51	611	3750	70	1140	6050	89	1840	8900	108	2710
158	14	48	848	33	258	2080	52	635	3860	71	1170	6190	90	1880	9060	109	2760
181	15	55	900	34	274	2160	53	659	3970	72	1210	6330	91	1920	9230	110	2810
205	16	62	953	35	290	2240	54	684	4080	73	1240	6460	92	1970	9400	111	2860
231	17	70	1000	36	307	2320	55	709	4190	74	1270	6610	93	2010	9560	112	2910
258	18	78	1060	37	324	2410	56	735	4310	75	1310	6750	94	2050	9740	113	2960
287	19	87	1120	38	341	2500	57	762	4420	76	1340	6890	95	2100	9910	114	3020

IX.—DISTANCE TO THE SEA HORIZON IN STATUTE MILES

Height in feet	Dist.	Height in metres	Height in feet	Dist.	Height in metres	Height in feet	Dist.	Height in metres	Height in feet	Dist.	Height in metres	Height in feet	Dist.	Height in metres	Height in feet	Dist.	Height in metres
0		0	288	23	87	1120	45	344	2520	67	768	4460	89	1360	6960	111	2120
1	1		314	23	95	1180	46	359	2590	68	791	4560	90	1390	7080	112	2160
3	2	1	342	24	104	1230	46	375	2670	68	815	4670	91	1420	7210	112	2190
6	3	2	370	25	113	1280	47	392	2750	69	839	4770	91	1450	7340	113	2230
11	4	3	400	26	122	1340	48	408	2830	70	863	4870	92	1480	7470	114	2270
17	5	5	431	27	131	1390	49	425	2910	71	888	4980	93	1510	7600	115	2310
24	6	7	463	28	141	1450	50	443	2990	72	913	5090	94	1550	7730	116	2350
32	7	9	496	29	151	1510	51	460	3080	73	938	5200	95	1580	7870	117	2390
41	8	12	530	30	161	1570	52	479	3160	74	964	5310	96	1610	8000	118	2440
51	9	15	565	31	172	1630	53	497	3250	75	990	5420	97	1650	8140	119	2480
62	10	19	602	32	183	1690	54	516	3330	76	1010	5530	98	1680	8280	120	2520
75	11	22	639	33	195	1750	55	535	3420	77	1040	5640	99	1720	8410	121	2560
89	12	27	678	34	206	1820	56	554	3510	78	1070	5750	100	1750	8550	122	2600
103	13	31	718	35	219	1880	57	574	3600	79	1090	5870	101	1790	8690	123	2650
119	14	36	759	36	231	1950	58	594	3690	80	1120	5990	102	1820	8830	124	2690
137	15	41	801	37	244	2010	59	615	3780	81	1150	6100	103	1860	8980	125	2730
155	16	47	845	38	257	2080	60	636	3880	82	1180	6220	104	1890	9120	126	2780
174	17	53	889	39	271	2150	61	657	3970	83	1210	6340	105	1930	9270	127	2820
195	18	59	935	40	285	2220	62	678	4070	84	1240	6460	106	1970	9410	128	2870
216	19	66	982	41	299	2290	63	700	4160	85	1270	6580	107	2000	9560	129	2910
239	20	73	1030	42	313	2370	64	723	4260	86	1300	6710	108	2040	9710	130	2960
263	21	80	1070	43	328	2440	65	745	4360	87	1330	6830	109	2080	9860	131	3000
288	22	87	1120	44	344	2520	66	768	4460	88	1360	6960	110	2120	10000	132	3050

These tables give the distance to the sea horizon, in nautical miles and in statute miles, with argument height of eye of the observer in feet or in metres.

At the moment when an object of known height is just appearing or disappearing over the sea horizon, its distance may be found by adding the distance corresponding to its height to the distance corresponding to the height of eye of the observer.

X.—TABLE OF RANGES IN NAUTICAL MILES

The tables below and on the opposite page give the distance, to the nearest 5 nautical miles, of an object, whose height is known and is *greater* than the height of the observer. The arguments of the table are the observed *angle of elevation* to the object, and the *difference in height* between the object and the observer, expressed in feet or in metres.

Example.—An observer, whose height is 1,500 feet, finds that the angle of elevation to the summit of a mountain, whose height is known to be 7,000 feet, is $0^{\circ} 48'$. Required the distance away of the mountain.

The difference in height between the mountain and the observer is $7,000 - 1,500 = 5,500$ feet. Entering on the opposite page the column headed $0^{\circ} 50'$ (the nearest tabulated value to $0^{\circ} 48'$), and choosing the left-hand of the two argument columns since the height is measured in feet, it is seen that 5,500 lies in the interval between 5,130 and 5,910, so that the distance of the mountain, to the nearest 5 miles, is 45 nautical miles.

The tables on pages 226 to 228 give the distance of an object, whose height is known, and is *less* than the height of the observer. The arguments of the table are the observed *angle of depression* to the object, and the *difference in height* between the observer and the object, expressed in feet or in metres. The distance is given to the nearest mile up to 10 nautical miles, and to the nearest 5 miles from 10 to 60 nautical miles.

Example.—An observer, whose height is 1,500 metres, finds that the angle of depression to a ship is $5^{\circ} 37'$. Required the distance away of the ship.

Entering on page 228 the column headed $5^{\circ} 30'$, and choosing the right-hand of the two argument columns, it is seen that 1,500 is an exact tabulated value, so that the distance away of the ship is 8 nautical miles.

On page 226, figures in *italics* represent the difference in height, *when the object observed is beyond the sea horizon*. If it is uncertain whether the object is beyond the horizon or not, and the two parts of the table give widely different results, there should be no doubt which is the correct one, while in doubtful cases the error will not be serious.

These tables are intended to give only the approximate range. They should prove a more reliable guide for large angles of elevation and depression than for small ones.

Height of object *greater* than height of observer

Angle of elevation																	
$4^{\circ} 00'$			$3^{\circ} 40'$			$3^{\circ} 20'$			$3^{\circ} 00'$			$2^{\circ} 40'$			$2^{\circ} 20'$		
Height in feet	Range	Height in metres	Height in feet	Range	Height in metres	Height in feet	Range	Height in metres	Height in feet	Range	Height in metres	Height in feet	Range	Height in metres	Height in feet	Range	Height in metres
0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
1060	5	325	978	5	298	890	5	271	801	5	244	712	5	217	624	5	190
3230	10	985	2960	10	904	2690	10	822	2430	10	741	2160	10	660	1900	10	579
5430	15	1650	4990	15	1520	4540	15	1380	4100	15	1250	3650	15	1110	3210	15	980
7670	20	2330	7050	20	2140	6430	20	1960	5810	20	1770	5190	20	1580	4570	20	1390
9950	25	3030	9150	25	2790	8350	25	2540	7550	25	2300	6750	25	2050	5960	25	1810
12200	30	3740	11200	30	3440	10300	30	3140	9340	30	2840	8360	30	2540	7390	30	2250
14600	35	4450	13400	35	4100	12300	35	3750	11100	35	3400	10000	35	3050	8850	35	2690
17000	40	5180	15600	40	4780	14300	40	4370	13000	40	3960	11600	40	3560	10300	40	3150
19400	45	5920	17900	45	5460	16400	45	5000	14900	45	4540	13400	45	4080	11900	45	3620
21900	50	6680	20200	50	6160	18500	50	5650	16800	50	5130	15100	50	4620	13400	50	4110
24400	55	7440	22500	55	6870	20600	55	6300	18800	55	5730	16900	55	5170	15100	55	4600
26900	60	8210	24900	60	7590	22800	60	6970	20800	60	6350	18800	60	5730	16700	60	5100
29500		9000	27300		8320	25100		7650	22800		6970	20600		6300	18400		5620

X.—TABLE OF RANGES IN NAUTICAL MILES
Height of object *greater* than height of observer

Angle of elevation																	
2° 00'			1° 50'			1° 40'			1° 30'			1° 20'			1° 10'		
Height in feet	Range	Height in metres	Height in feet	Range	Height in metres	Height in feet	Range	Height in metres	Height in feet	Range	Height in metres	Height in feet	Range	Height in metres	Height in feet	Range	Height in metres
0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
535	5	163	491	5	149	447	5	136	402	5	122	358	5	109	314	5	95
1630	10	498	1500	10	458	1370	10	417	1230	10	377	1100	10	336	971	10	296
2770	15	845	2550	15	777	2330	15	710	2100	15	643	1880	15	575	1660	15	508
3940	20	1200	3630	20	1100	3320	20	1010	3020	20	920	2710	20	826	2400	20	731
5160	25	1570	4760	25	1450	4360	25	1330	3960	25	1200	3570	25	1080	3170	25	966
6410	30	1950	5920	30	1800	5440	30	1650	4950	30	1510	4460	30	1360	3980	30	1210
7700	35	2340	7130	35	2170	6550	35	1990	5970	35	1820	5400	35	1640	4820	35	1470
9030	40	2750	8360	40	2550	7700	40	2340	7040	40	2140	6370	40	1940	5710	40	1740
10400	45	3160	9640	45	2940	8890	45	2710	8140	45	2480	7390	45	2250	6630	45	2020
11800	50	3590	10900	50	3340	10100	50	3080	9280	50	2820	8440	50	2570	7590	50	2310
13200	55	4030	12300	55	3750	11300	55	3470	10400	55	3180	9520	55	2900	8590	55	2620
14700	60	4480	13700	60	4170	12600	60	3860	11600	60	3550	10600	60	3240	9630	60	2930
16200		4950	15100		4610	14000		4270	12900		3930	11800		3600	10700		3260

Angle of elevation																	
1° 00'			0° 55'			0° 50'			0° 45'			0° 40'			0° 35'		
Height in feet	Range	Height in metres	Height in feet	Range	Height in metres	Height in feet	Range	Height in metres	Height in feet	Range	Height in metres	Height in feet	Range	Height in metres	Height in feet	Range	Height in metres
0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
270	5	82	247	5	75	225	5	68	203	5	62	181	5	55	159	5	48
839	10	255	772	10	235	706	10	215	640	10	195	573	10	174	507	10	154
1440	15	440	1330	15	406	1220	15	373	1110	15	339	1000	15	305	893	15	272
2090	20	637	1930	20	590	1780	20	542	1620	20	495	1470	20	448	1310	20	401
2770	25	845	2570	25	784	2370	25	724	2170	25	663	1970	25	602	1770	25	542
3490	30	1060	3250	30	991	3000	30	916	2760	30	842	2520	30	768	2270	30	694
4250	35	1290	3960	35	1200	3670	35	1120	3390	35	1030	3100	35	945	2810	35	858
5050	40	1530	4710	40	1430	4380	40	1330	4050	40	1230	3720	40	1130	3390	40	1030
5880	45	1790	5500	45	1670	5130	45	1560	4750	45	1450	4380	45	1330	4000	45	1220
6750	50	2060	6330	50	1930	5910	50	1800	5490	50	1670	5070	50	1540	4650	50	1410
7670	55	2330	7200	55	2190	6740	55	2050	6270	55	1910	5810	55	1770	5340	55	1620
8610	60	2620	8100	60	2470	7600	60	2310	7090	60	2160	6580	60	2000	6070	60	1850
9600		2920	9050		2750	8500		2590	7940		2420	7390		2250	6840		2080

Angle of elevation																	
0° 30'			0° 25'			0° 20'			0° 15'			0° 10'			0° 05'		
Height in feet	Range	Height in metres	Height in feet	Range	Height in metres	Height in feet	Range	Height in metres	Height in feet	Range	Height in metres	Height in feet	Range	Height in metres	Height in feet	Range	Height in metres
0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
137	5	41	115	5	35	93	5	28	71	5	21	48	5	14	26	5	8
440	10	134	374	10	114	308	10	93	241	10	73	175	10	53	109	10	33
782	15	238	671	15	204	561	15	171	450	15	137	339	15	103	229	15	69
1160	20	354	1000	20	306	852	20	259	697	20	212	542	20	165	387	20	118
1570	25	481	1380	25	420	1180	25	360	982	25	299	783	25	238	584	25	178
2030	30	620	1790	30	546	1540	30	471	1300	30	397	1060	30	323	818	30	249
2520	35	770	2240	35	683	1950	35	595	1660	35	507	1370	35	420	1090	35	332
3060	40	932	2720	40	831	2390	40	730	2060	40	629	1730	40	528	1400	40	427
3620	45	1100	3250	45	991	2870	45	877	2500	45	762	2120	45	648	1750	45	533
4230	50	1290	3810	50	1160	3390	50	1030	2970	50	907	2550	50	799	2130	50	651
4880	55	1480	4410	55	1340	3950	55	1200	3480	55	1060	3020	55	922	2560	55	780
5560	60	1690	5050	60	1540	4540	60	1380	4040	60	1230	3530	60	1070	3020	60	921
6280		1910	5730		1740	5180		1570	4620		1410	4070		1240	3520		1070

X.—TABLE OF RANGES IN NAUTICAL MILES

Height of object *less* than height of observer

Angle of depression																	
0° 05'			0° 10'			0° 15'			0° 20'			0° 25'			0° 30'		
Height in feet	Range	Height in metres	Height in feet	Range	Height in metres	Height in feet	Range	Height in metres	Height in feet	Range	Height in metres	Height in feet	Range	Height in metres	Height in feet	Range	Height in metres
0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
4	1	1	9	1	2	13	1	4	17	1	5	21	1	6	26	1	8
11	2	3	24	2	7	38	2	11	51	2	15	64	2	19	77	2	23
17	3	5	39	3	12	61	3	18	83	3	25	106	3	32	127	3	39
21	4	6	52	4	15	83	4	25	114	4	34	145	4	44	176	4	53
24	5	7	64	5	19	103	5	31	143	5	43	183	5	55	223	5	68
25	6	8	74	6	22	122	6	37	171	6	52	220	6	67	268	6	81
26	7	8	82	7	25	140	7	42	197	7	60	255	7	77	312	7	95
24	8		89	8	27	156	8	47	222	8	67	288	8	88	355	8	108
21	9	7	95	9	29	170	9	52	245	9	74	320	9	97	396	9	120
16	10	5	99	10	30	183	10	55	267	10	81	351	10	107	435	10	132
0		0	103	15	32	212	15	64	323	15	98	434	15	132	544	15	166
			77	20	24	231	20	70	386	20	117	541	20	164	695	20	212
			13	25	0	213	25	65	411	25	125	609	25	185	808	25	246
			0			155	30	18	398	30	122	640	30	195	884	30	269
						59	35	0	346	35	106	634	35	194	921	35	280
						0			258	40	79	590	40	180	921	35	281
									130	45	40	506	45	155	882	40	269
									0		0	385	45	118	805	45	246
												226	50	69	690	50	211
												28	55	9	537	55	164
												0	60	0	346	60	106

Angle of depression																	
0° 35'			0° 40'			0° 45'			0° 50'			0° 55'			1° 00'		
Height in feet	Range	Height in metres	Height in feet	Range	Height in metres	Height in feet	Range	Height in metres	Height in feet	Range	Height in metres	Height in feet	Range	Height in metres	Height in feet	Range	Height in metres
0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
30	1	9	35	1	10	39	1	12	44	1	13	48	1	14	52	1	16
91	2	27	104	2	31	117	2	35	130	2	39	144	2	43	157	2	47
150	3	45	172	3	52	194	3	59	216	3	65	238	3	72	260	3	79
207	4	63	238	4	72	269	4	82	300	4	91	331	4	100	362	4	110
263	5	80	302	5	92	342	5	104	382	5	116	422	5	128	462	5	140
317	6	96	366	6	111	414	6	126	463	6	141	512	6	156	560	6	170
370	7	112	427	7	130	485	7	147	542	7	165	600	7	182	657	7	200
421	8	128	488	8	148	554	8	168	620	8	189	687	8	209	753	8	229
471	9	143	546	9	166	621	9	189	696	9	212	772	9	235	847	9	258
519	10	158	603	10	183	687	10	209	771	10	235	855	10	260	939	10	286
655	15	199	765	15	233	876	15	267	986	15	300	1090	15	334	1200	15	368
850	20	259	1000	20	306	1160	20	353	1310	20	400	1470	20	448	1620	20	495
1000	25	307	1200	25	367	1400	25	428	1600	25	489	1800	25	549	2000	25	610
1120	30	343	1370	30	417	1610	30	491	1850	30	566	2100	30	640	2340	30	714
1200	35	368	1490	35	456	1780	35	543	2070	35	631	2350	35	719	2640	35	806
1250	40	384	1630	40	497	1910	40	612	2240	40	727	2570	40	841	2910	40	887
1260	45	374	1650	45	502	2060	45	629	2480	45	757	2760	45	885	3130	45	956
1230	50	352	1620	50	494	2080	50	634	2540	50	776	2900	50	918	3320	50	1010
1050	55	319	1560	55	474	2070	55	629	2570	55	783	3010	55	918	3470	55	1050
899	60	274	1460	60	443	2010	60	611	2560	60	780	3110	60	947	3660	60	1110

For explanation, see page 224.

X.—TABLE OF RANGES IN NAUTICAL MILES

Height of object *less* than height of observer

Angle of depression																	
1° 10'			1° 20'			1° 30'			1° 40'			1° 50'			2° 00'		
Height in feet	Range in metres	Height in metres	Height in feet	Range in metres	Height in metres	Height in feet	Range in metres	Height in metres	Height in feet	Range in metres	Height in metres	Height in feet	Range in metres	Height in metres	Height in feet	Range in metres	Height in metres
0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
61	1	18	70	1	21	79	1	24	88	1	26	97	1	29	106	1	32
183	2	56	210	2	64	237	2	72	263	2	80	290	2	88	316	2	96
305	3	92	349	3	106	393	3	119	437	3	133	481	3	146	526	3	160
424	4	129	486	4	148	548	4	167	610	4	185	672	4	204	734	4	223
541	5	165	621	5	189	701	5	213	780	5	238	860	5	262	940	5	286
658	6	200	755	6	230	852	6	259	950	6	289	1040	6	319	1140	6	349
772	7	235	887	7	270	1000	7	305	1110	7	340	1230	7	375	1340	7	410
886	8	270	1010	8	310	1150	8	351	1280	8	391	1410	8	432	1550	8	472
997	9	304	1140	9	350	1290	9	395	1440	9	441	1590	9	487	1750	9	533
1100	10	337	1270	10	388	1440	10	440	1610	10	491	1780	10	542	1940	10	594
1430	15	435	1650	15	503	1870	15	570	2090	15	638	2310	15	705	2530	15	772
1930	20	589	2240	20	684	2550	20	778	2860	20	872	3170	20	967	3480	20	1060
2400	25	732	2790	25	853	3190	25	974	3590	25	1090	3990	25	1210	4390	25	1330
2830	30	862	3310	30	1015	3800	30	1150	4290	30	1300	4770	30	1450	5260	30	1600
3220	35	982	3790	35	1150	4370	35	1330	4940	35	1500	5520	35	1680	6090	35	1850
3570	40	1080	4230	40	1290	4900	40	1490	5560	40	1690	6230	40	1890	6890	40	2100
3880	45	1180	4640	45	1410	5390	45	1640	6140	45	1870	6890	45	2100	7650	45	2330
4160	50	1270	5000	50	1520	5840	50	1780	6680	50	2030	7530	50	2290	8370	50	2550
4400	55	1340	5330	55	1620	6260	55	1900	7190	55	2190	8120	55	2470	9050	55	2750
4600	60	1400	5620	60	1710	6640	60	2020	7660	60	2330	8670	60	2640	9690	60	2950
4760		1450	5870		1790	6980		2120	8080		2460	9190		2800	10300		3140

Angle of depression																	
2° 20'			2° 40'			3° 00'			3° 20'			3° 40'			4° 00'		
Height in feet	Range in metres	Height in metres	Height in feet	Range in metres	Height in metres	Height in feet	Range in metres	Height in metres	Height in feet	Range in metres	Height in metres	Height in feet	Range in metres	Height in metres	Height in feet	Range in metres	Height in metres
0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
123	1	37	141	1	43	159	1	48	176	1	53	194	1	59	212	1	64
369	2	112	422	2	128	476	2	145	529	2	161	582	2	177	636	2	193
614	3	187	703	3	214	792	3	241	880	3	268	969	3	295	1050	3	322
858	4	261	982	4	299	1100	4	337	1230	4	375	1350	4	412	1470	4	450
1090	5	335	1250	5	383	1410	5	432	1570	5	481	1730	5	529	1890	5	578
1340	6	408	1530	6	467	1730	6	527	1920	6	586	2120	6	646	2310	6	706
1570	7	481	1800	7	551	2040	7	621	2270	7	692	2500	7	762	2730	7	832
1810	8	553	2080	8	634	2340	8	715	2610	8	796	2880	8	877	3140	8	959
2050	9	625	2350	9	719	2650	9	809	2950	9	901	3250	9	993	3560	9	1080
2280	10	698	2620	10	797	2950	10	902	3290	10	1000	3630	10	1100	3970	10	1210
2970	15	908	3420	15	1040	3860	15	1170	4300	15	1310	4750	15	1440	5190	15	1580
4100	20	1250	4720	20	1430	5340	20	1620	5960	20	1810	6580	20	2000	7200	20	2190
5190	25	1580	5980	25	2190	6780	25	2060	7580	25	2310	8380	25	2550	9180	25	2790
6230	30	1900	7210	30	2560	8180	30	2490	9160	30	2790	10100	30	3090	11100	30	3380
7250	35	2210	8400	35	2910	9550	35	2910	10700	35	3260	11800	35	3610	13000	35	3960
8220	40	2500	9550	40	3250	10800	40	3310	12200	40	3720	13500	40	4120	14800	40	4530
9150	45	2790	10600	45	3570	12100	45	3710	13600	45	4170	15100	45	4620	16700	45	5090
10000	50	3060	11700	50	3890	13400	50	4090	15100	50	4600	16700	50	5120	18400	50	5630
10900	55	3320	12700	55	4190	14600	55	4460	16400	55	5020	18300	55	5590	20200	55	6160
11700	60	3570	13700	60	4490	15800	60	4810	17800	60	5440	19900	60	6060	21900	60	6680
12500		3810	14700			16900		5160	19100		5840	21300		6510	23600		7190

For explanation, see page 224.

X.—TABLE OF RANGES IN NAUTICAL MILES

Height of object *less* than height of observer

Angle of depression																	
4° 30'			5° 00'			5° 30'			6° 00'			6° 30'			7° 00'		
Height in feet	Range	Height in metres	Height in feet	Range	Height in metres	Height in feet	Range	Height in metres	Height in feet	Range	Height in metres	Height in feet	Range	Height in metres	Height in feet	Range	Height in metres
0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
238	1	72	265	1	81	292	1	89	319	1	97	346	1	105	373	1	113
716	2	218	796	2	242	876	2	267	956	2	291	1030	2	316	1110	2	340
1190	3	363	1320	3	404	1450	3	444	1590	3	485	1720	3	526	1860	3	567
1660	4	507	1850	4	564	2040	4	621	2220	4	679	2410	4	736	2600	4	793
2130	5	651	2370	5	725	2610	5	798	2860	5	872	3100	5	945	3340	5	1010
2600	6	795	2900	6	885	3190	6	974	3490	6	1060	3780	6	1150	4080	6	1240
3070	7	938	3420	7	1040	3770	7	1150	4120	7	1250	4470	7	1360	4820	7	1460
3540	8	1080	3940	8	1200	4340	8	1320	4750	8	1440	5150	8	1570	5550	8	1690
4010	9	1220	4460	9	1360	4920	9	1500	5370	9	1630	5830	9	1770	6290	9	1910
4470	10	1360	4980	10	1510	5490	10	1670	6000	10	1830	6510	10	1980	7020	10	2140
5860	15	1780	6530	15	1990	7200	15	2190	7870	15	2390	8540	15	2600	9210	15	2800
8140	20	2480	9070	20	2760	10000	20	3050	10900	20	3330	11800	20	3620	12800	20	3910
10300	25	3160	11500	25	3530	12700	25	3890	14000	25	4260	15200	25	4630	16400	25	5000
12500	30	3830	14000	30	4280	15500	30	4730	16900	30	5180	18400	30	5630	19900	30	6080
14700	35	4490	16400	35	5020	18200	35	5550	19900	35	6080	21700	35	6620	23400	35	7150
16800	40	5140	18800	40	5750	20800	40	6360	22800	40	6880	24900	40	7590	26900	40	8210
18900	45	5780	21200	45	6470	23500	45	7160	25800	45	7860	28000	45	8550	30300	45	9250
21000	50	6400	23500	50	7180	26000	50	7950	28600	50	8730	31100	50	9510	33700	50	10200
23000	55	7020	25800	55	7870	28600	55	8730	31400	55	9590	34200	55	10400	37100	55	11300
25000	60	7620	28000	60	8550	31100	60	9490	34200	60	10400	37300	60	11300	40400	60	12300
26900		8210	30200		9230	33600		10200	36900		11200	40300		12200	43600		13300

Angle of depression																	
7° 30'			8° 00'			8° 30'			9° 00'			9° 30'			10° 00'		
Height in feet	Range	Height in metres	Height in feet	Range	Height in metres	Height in feet	Range	Height in metres	Height in feet	Range	Height in metres	Height in feet	Range	Height in metres	Height in feet	Range	Height in metres
0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
399	1	121	427	1	130	454	1	138	481	1	146	508	1	154	535	1	163
1190	2	365	1270	2	390	1360	2	415	1440	2	439	1520	2	464	1600	2	489
1990	3	608	2130	3	649	2260	3	691	2400	3	732	2540	3	774	2670	3	815
2790	4	851	2980	4	909	3170	4	966	3360	4	1020	3550	4	1080	3740	4	1140
3580	5	1090	3830	5	1160	4070	5	1240	4310	5	1310	4560	5	1390	4810	5	1460
4380	6	1330	4670	6	1420	4970	6	1510	5270	6	1600	5570	6	1690	5870	6	1790
5170	7	1570	5520	7	1680	5870	7	1790	6220	7	1890	6580	7	2000	6930	7	2110
5960	8	1810	6360	8	1940	6770	8	2060	7180	8	2180	7580	8	2310	8000	8	2430
6750	9	2050	7210	9	2190	7670	9	2330	8130	9	2470	8590	9	2610	9060	9	2760
7530	10	2290	8050	10	2450	8560	10	2610	9080	10	2760	9600	10	2920	10100	10	3080
9880	15	3010	10500	15	3220	11200	15	3420	11900	15	3630	12600	15	3840	13200	15	4050
13700	20	4200	14700	20	4480	15600	20	4770	16600	20	5060	17500	20	5350	18500	20	5640
17600	25	5370	18800	25	5740	20000	25	6110	21200	25	6480	22500	25	6860	23700	25	7230
21400	30	6530	22900	30	6980	24400	30	7440	25900	30	7890	27400	30	8350	28900	30	8810
25200	35	7680	26900	35	8220	28700	35	8760	30500	35	9290	32200	35	9830	34000	35	10300
28900	40	8820	30900	40	9440	33000	40	10000	35000	40	10600	37000	40	11300	39100	40	11900
32600	45	9950	34900	45	10600	37200	45	11300	39500	45	12000	41800	45	12700	44200	45	13400
36300	50	11000	38800	50	11800	41400	50	12600	44000	50	13400	46600	50	14200	49200	50	15000
39900	55	12100	42700	55	13000	45600	55	13900	48400	55	14700	51300	55	15600	54200	55	16500
43500	60	13200	46600	60	14200	49700	60	15100	52800	60	16100	56000	60	17000	59100	60	18000
47000		14300	50400		15300	53800		16400	57200		17400	60600		18400	64000		19500

For explanation, see page 224.

XI.—TEMPERATURE CONVERSION **FAHRENHEIT AND CENTIGRADE**

°F	°C	°F	°C	°F	°C	°F	°C	°F	°C	°F	°C	°F	°C
-52	-46	-14	-25	+23	-4	+61	+17	+99	+38	+137	+59	+175	+80
50	45	13	24	25	3	63	18	101	39	139	60	176	81
49	44	11	23	27	3	65	18	103	39	140	60	178	81
47	44	9	23	29	2	67	19	104	40	142	61	180	82
45	43	7	22	31	-1	68	20	106	41	144	62	182	83
43	42	5	21	32	0	70	21	108	42	146	63	184	84
41	41	3	20	34	+1	72	22	110	43	148	64	185	85
40	40	2	19	36	2	74	23	112	44	149	65	187	86
38	39	0	18	38	3	76	24	113	45	151	66	189	87
36	38	-2	17	40	4	77	25	115	46	153	67	191	88
34	37	-4	16	42	5	79	26	117	47	155	68	193	89
32	36	-6	15	44	6	81	27	119	48	157	69	195	90
31	35	-7	14	45	7	83	28	121	49	158	70	196	91
29	34	-9	13	47	8	85	29	122	50	160	71	198	92
27	33	-11	12	49	9	86	30	124	51	162	72	200	93
25	32	-13	11	50	10	88	31	126	52	164	73	202	94
23	31	-15	10	52	11	90	32	128	53	166	74	203	95
22	30	-16	9	54	12	92	33	130	54	167	75	205	96
20	29	-18	8	56	13	94	34	131	55	169	76	207	97
18	28	-20	7	58	14	95	35	133	56	171	77	209	98
16	27	-22	6	59	15	97	36	135	57	173	78	211	99
-14	-26	-24	-5	+61	+16	+99	+37	+137	+58	+175	+79	+212	+100

XII.—CONVERSION FACTORS

Conversion	Ratio	Factor	Reciprocal
DISTANCE			
Statute Miles to Nautical Miles	66 to 76	0.8684	1.1515
Statute Miles „ Kilometres	66 „ 41	1.6093	0.6214
Nautical Miles „ Kilometres	76 „ 41	1.8531	0.5396
Feet „ Metres	25 „ 82	0.3048	3.2808
Yards „ Metres	32 „ 35	0.9144	1.0936
Fathoms „ Feet	6 „ 1	6.0	0.1667
SPEED			
Miles per hour to Knots	66 to 76	0.8684	1.1515
Miles per hour „ Metres per second	38 „ 85	0.4470	2.2369
Knots „ Metres per second	35 „ 68	0.5148	1.9426
Miles per hour „ Feet per second	22 „ 15	1.4667	0.6818
LIQUID MEASURE			
Gallons to Litres	50 to 11	4.5460	0.2200
WEIGHT			
Pounds to Kilograms	44 to 97	0.4536	2.2046
PRESSURE			
Inches of Mercury to Millibars	2100 to 62	33.87	0.02953

XIII.—CONVERSION OF TIME TO ARC

For Intervals of 10 ^m						Interpolation Table											
h m	° ' "	h m	° ' "	h m	° ' "	h m	° ' "	h m	° ' "	h m	° ' "	h m	° ' "	h m	° ' "	h m	° ' "
00 00	0 00	08 00	120 00	16 00	240 00	00 00	0 00	03 17	0 50	06 37	1 40	00 02	0 01	22 0 51	42 1 41	00 05	0 02
10	2 30	10	122 30	10	242 30	02	0 03	22 0 52	45 1 42	00 10	0 04	33 0 53	50 1 43	06 58	1 44	00 13	0 05
20	5 00	20	125 00	20	245 00	18	0 05	38 0 55	06 58	07 01	1 45	21 0 06	46 0 56	07 06	1 46	00 26	0 06
30	7 30	30	127 30	30	247 30	26	0 07	46 0 57	09 06	09 01	1 47	29 0 08	49 0 58	09 09	1 48	00 29	0 07
40	10 00	40	130 00	40	250 00	34	0 09	54 0 59	14 1 49	14 1 49	1 49	37 0 10	57 1 00	17 1 50	00 34	0 09	0 10
50	12 30	50	132 30	50	252 30	42	0 11	05 1 01	22 1 51	22 1 51	1 51	45 0 12	05 1 02	25 1 52	00 42	0 11	0 12
01 00	15 00	09 00	135 00	17 00	255 00	50	0 12	10 1 03	30 1 53	30 1 53	1 53	53 0 13	13 1 04	33 1 54	00 53	0 12	0 13
10	17 30	10	137 30	10	257 30	00 58	0 14	18 1 05	38 1 55	38 1 55	1 55	01 01	0 15	21 1 06	41 1 56	00 58	0 14
20	20 00	20	140 00	20	260 00	01 01	0 16	26 1 07	46 1 57	46 1 57	1 57	06 0 17	29 1 08	49 1 58	00 06	0 16	0 15
30	22 30	30	142 30	30	262 30	14	0 18	34 1 09	54 1 59	54 1 59	1 59	09 0 18	37 1 10	57 2 00	00 14	0 18	0 16
40	25 00	40	145 00	40	265 00	17	0 19	42 1 11	05 2 02	05 2 02	2 02	17 0 19	42 1 11	57 2 00	00 17	0 19	0 17
50	27 30	50	147 30	50	267 30	22	0 21	45 1 12	10 2 03	10 2 03	2 03	25 0 21	45 1 12	05 2 02	00 22	0 21	0 18
02 00	30 00	10 00	150 00	18 00	270 00	30	0 23	50 1 13	13 2 04	13 2 04	2 04	30 0 22	50 1 13	10 2 03	00 30	0 23	0 19
10	32 30	10	152 30	10	272 30	33	0 24	53 1 14	18 2 05	18 2 05	2 05	33 0 23	53 1 14	13 2 04	00 33	0 24	0 20
20	35 00	20	155 00	20	275 00	38	0 25	58 1 15	21 2 06	21 2 06	2 06	38 0 24	58 1 15	18 2 05	00 38	0 25	0 21
30	37 30	30	157 30	30	277 30	41	0 26	01 1 16	26 2 07	26 2 07	2 07	41 0 25	01 1 16	21 2 05	00 41	0 26	0 22
40	40 00	40	160 00	40	280 00	46	0 27	06 1 17	29 2 08	29 2 08	2 08	46 0 26	06 1 17	26 2 07	00 46	0 27	0 23
50	42 30	50	162 30	50	282 30	49	0 28	09 1 18	34 2 09	34 2 09	2 09	49 0 27	09 1 18	29 2 08	00 49	0 28	0 24
03 00	45 00	11 00	165 00	19 00	285 00	54	0 29	14 1 19	37 2 10	37 2 10	2 10	54 0 28	14 1 19	34 2 09	00 54	0 29	0 25
10	47 30	10	167 30	10	287 30	57	0 30	17 1 20	42 2 11	42 2 11	2 11	01 57	17 1 20	37 2 09	00 57	0 30	0 26
20	50 00	20	170 00	20	290 00	02 02	0 31	22 1 21	45 2 12	45 2 12	2 12	02 02	22 1 21	42 2 10	00 02	0 31	0 27
30	52 30	30	172 30	30	292 30	05	0 32	25 1 22	50 2 13	50 2 13	2 13	05 0 31	25 1 22	45 2 11	00 05	0 32	0 28
40	55 00	40	175 00	40	295 00	10	0 33	30 1 23	53 2 14	53 2 14	2 14	10 0 32	30 1 23	50 2 12	00 10	0 33	0 29
50	57 30	50	177 30	50	297 30	13	0 34	33 1 24	58 2 15	58 2 15	2 15	13 0 33	33 1 24	53 2 13	00 13	0 34	0 30
04 00	60 00	12 00	180 00	20 00	300 00	18	0 35	38 1 25	01 2 16	01 2 16	2 16	18 0 34	38 1 25	58 2 14	00 18	0 35	0 31
10	62 30	10	182 30	10	302 30	21	0 36	41 1 26	06 2 17	06 2 17	2 17	21 0 35	41 1 26	01 2 15	00 21	0 36	0 32
20	65 00	20	185 00	20	305 00	26	0 37	46 1 27	09 2 18	09 2 18	2 18	26 0 36	46 1 27	06 2 16	00 26	0 37	0 33
30	67 30	30	187 30	30	307 30	29	0 38	49 1 28	14 2 19	14 2 19	2 19	29 0 37	49 1 28	09 2 17	00 29	0 38	0 34
40	70 00	40	190 00	40	310 00	34	0 39	54 1 29	17 2 20	17 2 20	2 20	34 0 38	54 1 29	14 2 19	00 34	0 39	0 35
50	72 30	50	192 30	50	312 30	37	0 40	57 1 30	22 2 21	22 2 21	2 21	37 0 39	57 1 30	17 2 19	00 37	0 40	0 36
05 00	75 00	13 00	195 00	21 00	315 00	42	0 41	05 1 31	25 2 22	25 2 22	2 22	42 0 40	05 1 31	14 2 19	00 42	0 41	0 37
10	77 30	10	197 30	10	317 30	45	0 42	10 1 32	30 2 23	30 2 23	2 23	45 0 41	10 1 32	17 2 20	00 45	0 42	0 38
20	80 00	20	200 00	20	320 00	50	0 43	13 1 33	33 2 24	33 2 24	2 24	50 0 42	13 1 33	22 2 21	00 50	0 43	0 39
30	82 30	30	202 30	30	322 30	53	0 44	18 1 34	38 2 25	38 2 25	2 25	53 0 43	18 1 34	25 2 22	00 53	0 44	0 40
40	85 00	40	205 00	40	325 00	58	0 45	21 1 35	41 2 26	41 2 26	2 26	02 58	21 1 35	30 2 23	00 58	0 45	0 41
50	87 30	50	207 30	50	327 30	01	0 46	26 1 36	46 2 27	46 2 27	2 27	01 01	26 1 36	33 2 24	00 01	0 46	0 42
06 00	90 00	14 00	210 00	22 00	330 00	06	0 47	29 1 37	49 2 28	49 2 28	2 28	06 0 46	29 1 37	38 2 25	00 06	0 47	0 43
10	92 30	10	212 30	10	332 30	09	0 48	34 1 38	54 2 29	54 2 29	2 29	09 0 47	34 1 38	41 2 26	00 09	0 48	0 44
20	95 00	20	215 00	20	335 00	14	0 49	37 1 39	57 2 30	57 2 30	2 30	14 0 48	37 1 39	49 2 27	00 14	0 49	0 45
30	97 30	30	217 30	30	337 30	17	0 50	40 1 40	09 00	09 00	2 30	17 0 49	40 1 40	54 2 28	00 17	0 50	0 46
40	100 00	40	220 00	40	340 00	03 22	0 50	42 1 40	10 00	10 00	2 30	03 22	42 1 40	57 2 29	00 03	0 50	0 47
50	102 30	50	222 30	50	342 30	When the argument is an exact tabulated value, the upper of the two possible values of the result should be taken.											
07 00	105 00	15 00	225 00	23 00	345 00												
10	107 30	10	227 30	10	347 30												
20	110 00	20	230 00	20	350 00												
30	112 30	30	232 30	30	352 30												
40	115 00	40	235 00	40	355 00												
50	117 30	50	237 30	50	357 30												

XIV.—CONVERSION OF ARC TO TIME

DEGREES												MINUTES	
°	'	°	'	°	'	°	'	°	'	°	'	°	'
0	00	60	4 00	120	8 00	180	12 00	240	16 00	300	20 00	0	00
1	04	61	4 04	121	8 04	181	12 04	241	16 04	301	20 04	1	04
2	08	62	4 08	122	8 08	182	12 08	242	16 08	302	20 08	2	08
3	12	63	4 12	123	8 12	183	12 12	243	16 12	303	20 12	3	12
4	16	64	4 16	124	8 16	184	12 16	244	16 16	304	20 16	4	16
5	20	65	4 20	125	8 20	185	12 20	245	16 20	305	20 20	5	20
6	24	66	4 24	126	8 24	186	12 24	246	16 24	306	20 24	6	24
7	28	67	4 28	127	8 28	187	12 28	247	16 28	307	20 28	7	28
8	32	68	4 32	128	8 32	188	12 32	248	16 32	308	20 32	8	32
9	36	69	4 36	129	8 36	189	12 36	249	16 36	309	20 36	9	36
10	40	70	4 40	130	8 40	190	12 40	250	16 40	310	20 40	10	40
11	44	71	4 44	131	8 44	191	12 44	251	16 44	311	20 44	11	44
12	48	72	4 48	132	8 48	192	12 48	252	16 48	312	20 48	12	48
13	52	73	4 52	133	8 52	193	12 52	253	16 52	313	20 52	13	52
14	56	74	4 56	134	8 56	194	12 56	254	16 56	314	20 56	14	56
15	00	75	5 00	135	9 00	195	13 00	255	17 00	315	21 00	15	00
16	04	76	5 04	136	9 04	196	13 04	256	17 04	316	21 04	16	04
17	08	77	5 08	137	9 08	197	13 08	257	17 08	317	21 08	17	08
18	12	78	5 12	138	9 12	198	13 12	258	17 12	318	21 12	18	12
19	16	79	5 16	139	9 16	199	13 16	259	17 16	319	21 16	19	16
20	20	80	5 20	140	9 20	200	13 20	260	17 20	320	21 20	20	20
21	24	81	5 24	141	9 24	201	13 24	261	17 24	321	21 24	21	24
22	28	82	5 28	142	9 28	202	13 28	262	17 28	322	21 28	22	28
23	32	83	5 32	143	9 32	203	13 32	263	17 32	323	21 32	23	32
24	36	84	5 36	144	9 36	204	13 36	264	17 36	324	21 36	24	36
25	40	85	5 40	145	9 40	205	13 40	265	17 40	325	21 40	25	40
26	44	86	5 44	146	9 44	206	13 44	266	17 44	326	21 44	26	44
27	48	87	5 48	147	9 48	207	13 48	267	17 48	327	21 48	27	48
28	52	88	5 52	148	9 52	208	13 52	268	17 52	328	21 52	28	52
29	56	89	5 56	149	9 56	209	13 56	269	17 56	329	21 56	29	56
30	00	90	6 00	150	10 00	210	14 00	270	18 00	330	22 00	30	00
31	04	91	6 04	151	10 04	211	14 04	271	18 04	331	22 04	31	04
32	08	92	6 08	152	10 08	212	14 08	272	18 08	332	22 08	32	08
33	12	93	6 12	153	10 12	213	14 12	273	18 12	333	22 12	33	12
34	16	94	6 16	154	10 16	214	14 16	274	18 16	334	22 16	34	16
35	20	95	6 20	155	10 20	215	14 20	275	18 20	335	22 20	35	20
36	24	96	6 24	156	10 24	216	14 24	276	18 24	336	22 24	36	24
37	28	97	6 28	157	10 28	217	14 28	277	18 28	337	22 28	37	28
38	32	98	6 32	158	10 32	218	14 32	278	18 32	338	22 32	38	32
39	36	99	6 36	159	10 36	219	14 36	279	18 36	339	22 36	39	36
40	40	100	6 40	160	10 40	220	14 40	280	18 40	340	22 40	40	40
41	44	101	6 44	161	10 44	221	14 44	281	18 44	341	22 44	41	44
42	48	102	6 48	162	10 48	222	14 48	282	18 48	342	22 48	42	48
43	52	103	6 52	163	10 52	223	14 52	283	18 52	343	22 52	43	52
44	56	104	6 56	164	10 56	224	14 56	284	18 56	344	22 56	44	56
45	00	105	7 00	165	11 00	225	15 00	285	19 00	345	23 00	45	00
46	04	106	7 04	166	11 04	226	15 04	286	19 04	346	23 04	46	04
47	08	107	7 08	167	11 08	227	15 08	287	19 08	347	23 08	47	08
48	12	108	7 12	168	11 12	228	15 12	288	19 12	348	23 12	48	12
49	16	109	7 16	169	11 16	229	15 16	289	19 16	349	23 16	49	16
50	20	110	7 20	170	11 20	230	15 20	290	19 20	350	23 20	50	20
51	24	111	7 24	171	11 24	231	15 24	291	19 24	351	23 24	51	24
52	28	112	7 28	172	11 28	232	15 28	292	19 28	352	23 28	52	28
53	32	113	7 32	173	11 32	233	15 32	293	19 32	353	23 32	53	32
54	36	114	7 36	174	11 36	234	15 36	294	19 36	354	23 36	54	36
55	40	115	7 40	175	11 40	235	15 40	295	19 40	355	23 40	55	40
56	44	116	7 44	176	11 44	236	15 44	296	19 44	356	23 44	56	44
57	48	117	7 48	177	11 48	237	15 48	297	19 48	357	23 48	57	48
58	52	118	7 52	178	11 52	238	15 52	298	19 52	358	23 52	58	52
59	56	119	7 56	179	11 56	239	15 56	299	19 56	359	23 56	59	56

XV.—CORRECTION TO TABULATED ALTITUDE FOR MINUTES OF DECLINATION

d	1	2	3	4	5	6	7	8	9	10	11	12	13	14	15	16	17	18	19	20	21	22	23	24	25	26	27	28	29	30	d	
00	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	00	
01	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	01	
02	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	1	1	1	1	1	1	1	1	1	1	1	1	1	1	1	02	
03	0	0	0	0	0	0	0	0	0	0	1	1	1	1	1	1	1	1	1	1	1	1	1	1	1	1	1	1	1	1	03	
04	0	0	0	0	0	0	0	1	1	1	1	1	1	1	1	1	1	1	1	1	1	1	2	2	2	2	2	2	2	2	04	
05	0	0	0	0	0	0	1	1	1	1	1	1	1	1	1	1	2	2	2	2	2	2	2	2	2	2	2	2	2	2	05	
06	0	0	0	0	0	1	1	1	1	1	1	1	1	2	2	2	2	2	2	2	2	2	2	2	2	2	3	3	3	3	06	
07	0	0	0	0	1	1	1	1	1	1	1	2	2	2	2	2	2	2	2	2	2	3	3	3	3	3	3	3	3	3	07	
08	0	0	0	1	1	1	1	1	1	1	2	2	2	2	2	2	2	2	3	3	3	3	3	3	3	3	3	4	4	4	08	
09	0	0	0	1	1	1	1	1	1	2	2	2	2	2	2	2	3	3	3	3	3	3	3	3	4	4	4	4	4	4	09	
10	0	0	0	1	1	1	1	1	2	2	2	2	2	2	2	3	3	3	3	3	3	4	4	4	4	4	4	4	4	4	10	
11	0	0	1	1	1	1	1	1	2	2	2	2	2	3	3	3	3	3	3	4	4	4	4	4	4	4	5	5	5	5	11	
12	0	0	1	1	1	1	1	2	2	2	2	2	3	3	3	3	3	4	4	4	4	4	4	4	4	5	5	5	5	6	12	
13	0	0	1	1	1	1	2	2	2	2	2	3	3	3	3	3	4	4	4	4	4	4	5	5	5	5	6	6	6	6	13	
14	0	0	1	1	1	1	2	2	2	2	3	3	3	3	4	4	4	4	4	4	5	5	5	5	6	6	6	6	6	7	14	
15	0	0	1	1	1	2	2	2	2	2	3	3	3	4	4	4	4	4	4	5	5	5	6	6	6	6	6	6	7	7	15	
16	0	1	1	1	1	2	2	2	2	3	3	3	3	4	4	4	5	5	5	5	6	6	6	6	6	6	7	7	7	8	16	
17	0	1	1	1	1	2	2	2	2	3	3	3	3	4	4	4	5	5	5	5	6	6	6	6	7	7	7	8	8	8	17	
18	0	1	1	1	2	2	2	2	2	3	3	3	4	4	4	4	5	5	5	6	6	6	6	7	7	7	8	8	8	9	18	
19	0	1	1	1	2	2	2	3	3	3	3	4	4	4	5	5	5	6	6	6	6	7	7	7	8	8	8	9	9	9	19	
20	0	1	1	1	2	2	2	3	3	3	4	4	4	4	5	5	6	6	6	6	7	7	7	8	8	8	8	9	9	10	20	
21	0	1	1	1	2	2	2	3	3	3	4	4	4	5	5	6	6	6	6	7	7	7	8	8	8	9	9	9	9	10	21	
22	0	1	1	1	2	2	2	3	3	3	4	4	4	5	5	6	6	6	7	7	7	8	8	8	9	9	10	10	10	11	22	
23	0	1	1	2	2	2	2	3	3	3	4	4	4	5	5	6	6	7	7	7	8	8	8	9	9	10	10	10	11	11	23	
24	0	1	1	2	2	2	3	3	3	4	4	4	5	5	6	6	6	7	7	8	8	8	9	9	10	10	10	11	11	12	24	
25	0	1	1	2	2	2	3	3	4	4	4	5	5	6	6	6	7	7	8	8	8	9	9	10	10	10	11	11	12	12	25	
26	0	1	1	2	2	3	3	3	4	4	5	5	6	6	6	6	7	7	8	8	9	9	9	10	10	10	11	11	12	13	26	
27	0	1	1	2	2	3	3	4	4	4	5	5	6	6	6	7	7	8	8	9	9	9	10	10	11	11	12	12	13	14	27	
28	0	1	1	2	2	3	3	4	4	5	5	6	6	7	7	7	8	8	9	9	10	10	11	11	12	12	13	13	14	14	28	
29	0	1	1	2	2	3	3	4	4	5	5	6	6	7	7	8	8	8	9	9	10	10	11	11	12	12	13	13	14	14	29	
30	0	1	2	2	2	3	4	4	4	5	6	6	6	7	8	8	8	9	9	10	10	10	11	11	12	12	13	13	14	15	30	
31	1	1	2	2	3	3	4	4	5	5	6	6	7	7	8	8	9	9	9	10	10	11	11	12	12	13	13	14	15	16	31	
32	1	1	2	2	3	3	4	4	5	5	6	6	7	7	8	8	9	9	10	10	11	11	12	12	13	13	14	15	15	16	32	
33	1	1	2	2	3	3	4	4	5	6	6	7	7	8	8	8	9	9	10	10	11	11	12	12	13	13	14	15	16	16	33	
34	1	1	2	2	3	3	4	4	5	6	6	7	7	8	8	9	10	10	11	11	12	12	13	13	14	14	15	15	16	17	34	
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XV.—CORRECTION TO TABULATED ALTITUDE FOR MINUTES OF DECLINATION

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